CS 184: Foundations of Computer Graphics Kinematics of Articulated Bodies

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Kinematics vs. dynamics

- Kinematics = motion but no forces
 - Keyframing, motion capture, etc.
- Dynamics = motion from forces
 - Simulation

If you want to know more about dynamics and simulation...

- Particles and rigid bodies:
 - Baraff and Witkin, "Physically Based Modeling", 2001
- Deformable bodies:
 - James O'Brien's CS 283 slides and readings on elastic simulation
- Fluids:
 - Bridson and Müller-Fischer, "Fluid Simulation for Computer Animation", 2007

- Rigid bodies connected with joints
 - Topology (what's connected to what)
 - Geometric relations from joints
- Not necessarily what's displayed in the end





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- Root body
 - Position and orientation set by "global" transformation
 - Other bodies move relative to root

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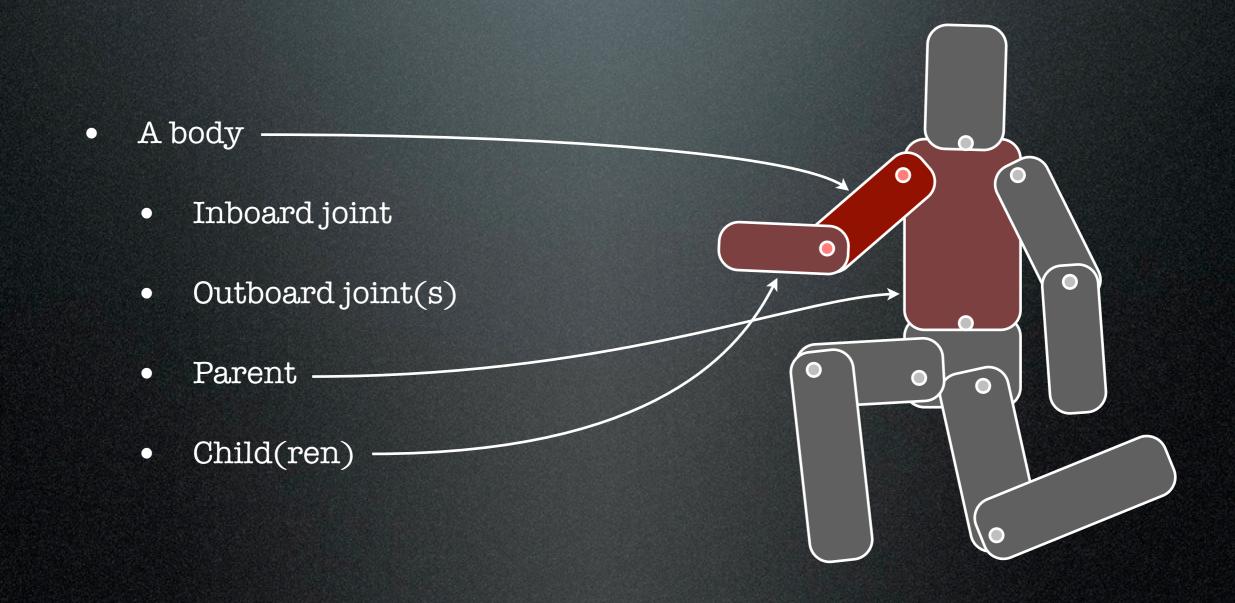
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- A joint
 - Inboard body (towards root)
 - Outboard body (away from root)

A body · • 0 Inboard joint • \mathbf{O} Outboard joint(s) • Parent • lacksquare \mathbf{O} Child(ren)

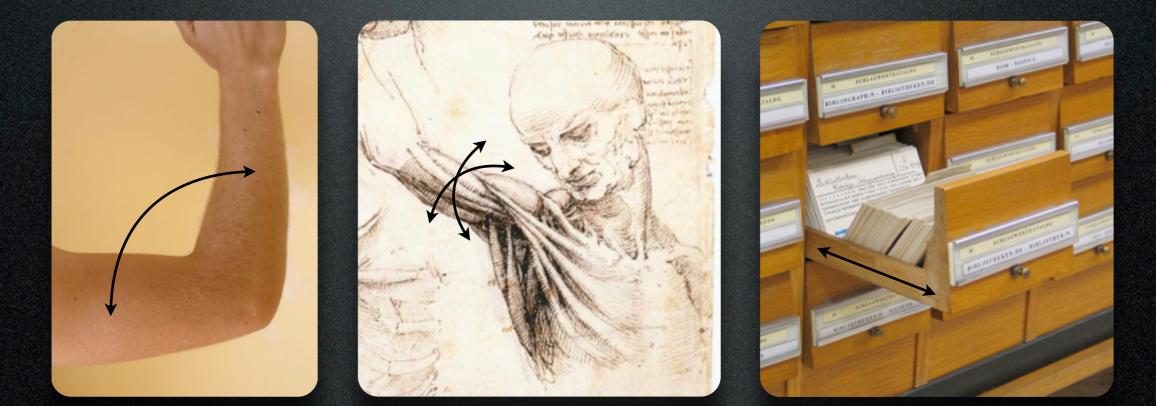
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• Interior joints are typically not 6 DOF

Pin joint: rotation about one axis Ball: arbitrary rotation Prism joint: translation along one axis

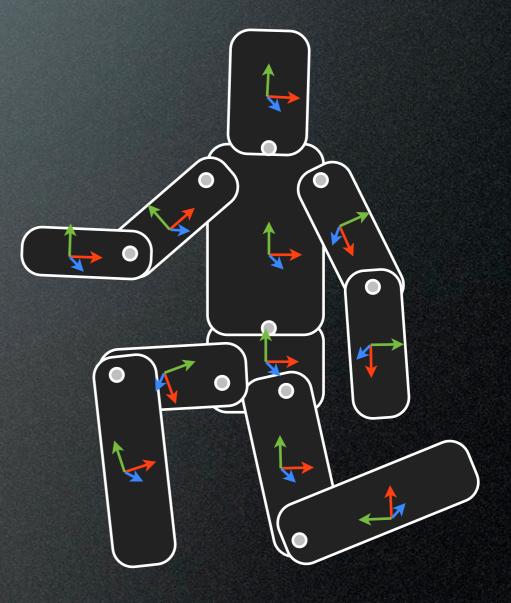


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Forward and inverse kinematics

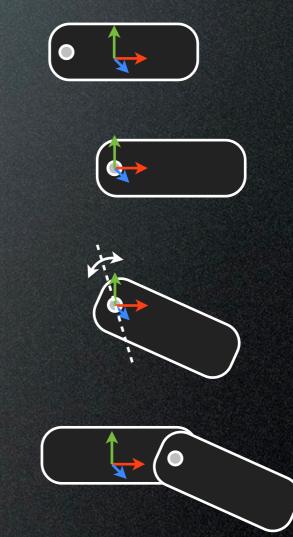
- Forward kinematics:
 - Given all the joint parameters, where are the bodies?
- Inverse kinematics:
 - Given where I want some body to be, what joint parameters do I need to set?

- Each body gets its own local coordinate system
 - Position of a vertex is fixed relative to local coordinate system
 - What is its position relative to world coordinates?



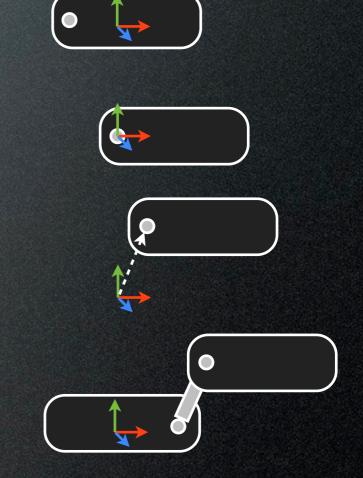
- Pinjoints
 - Translate inboard joint to origin
 - Apply rotation about axis
 - Translate origin to location of outboard joint on parent body

$$\mathbf{M} = \begin{bmatrix} \mathbf{I} & \mathbf{t}_{\text{parent}} \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \mathbf{R}(\theta) & \mathbf{0} \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \mathbf{I} & -\mathbf{t}_{\text{child}} \\ \mathbf{0} & 1 \end{bmatrix}$$

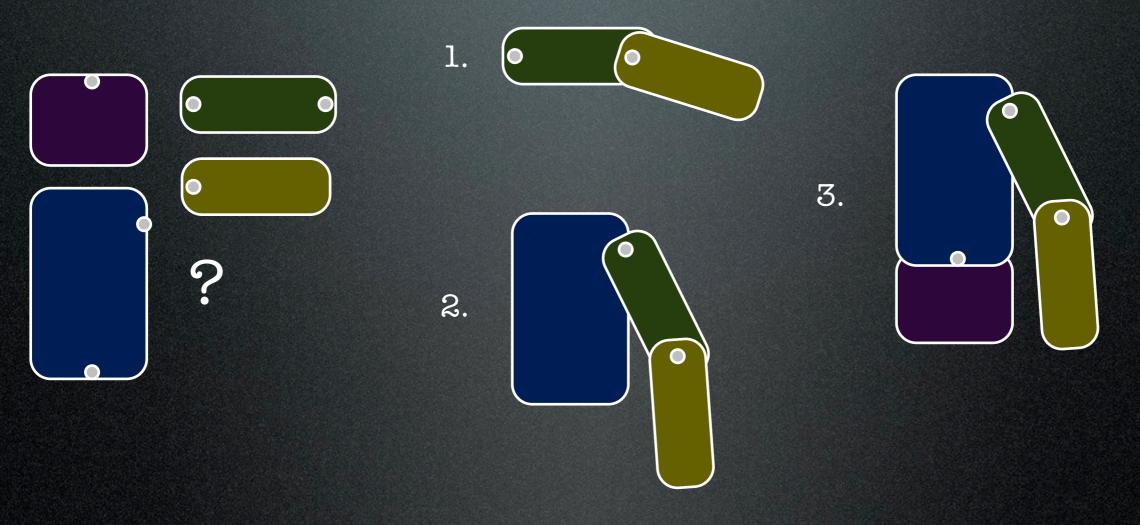


- Prism joints
 - Translate inboard joint to origin
 - Translate along axis
 - Translate origin to location of outboard joint on parent body

$$\mathbf{M} = \begin{bmatrix} \mathbf{I} & \mathbf{t}_{\text{parent}} \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \mathbf{I} & t\mathbf{a} \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \mathbf{I} & -\mathbf{t}_{\text{child}} \\ \mathbf{0} & 1 \end{bmatrix}$$

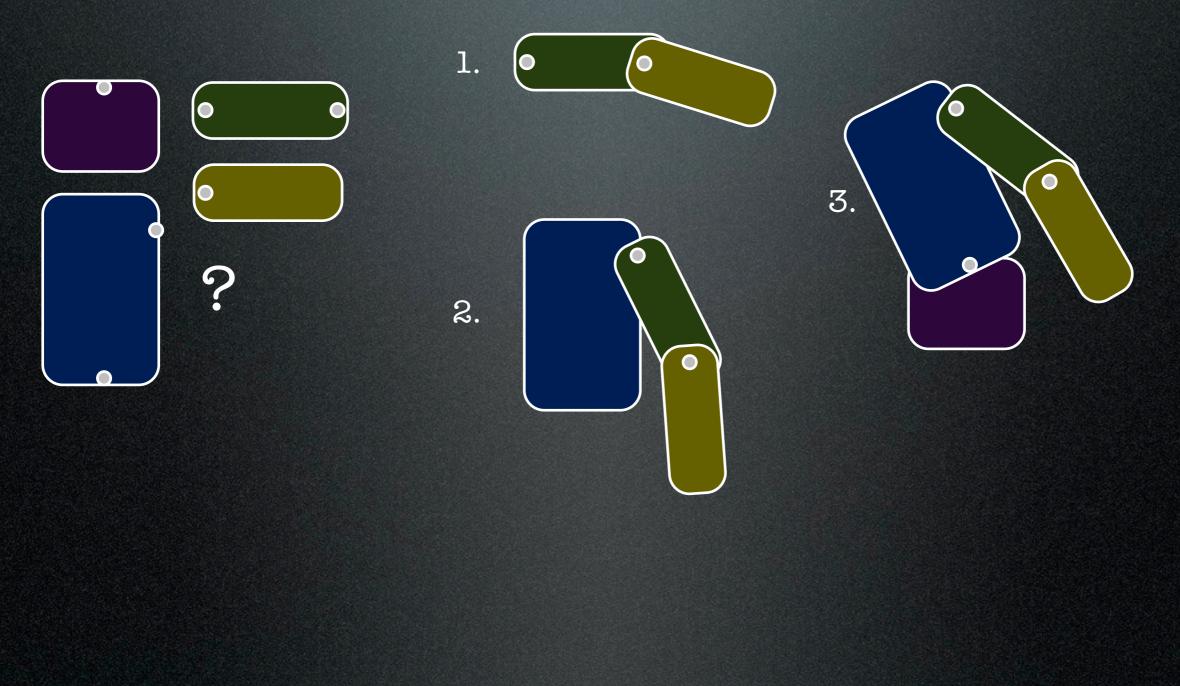


• Composite transformations up the hierarchy



• $\mathbf{M}_{world \leftarrow forearm} = \mathbf{M}_{world \leftarrow hip} \cdot \mathbf{M}_{hip \leftarrow torso} \cdot \mathbf{M}_{torso \leftarrow upperarm} \cdot \mathbf{M}_{upperarm \leftarrow forearm}$

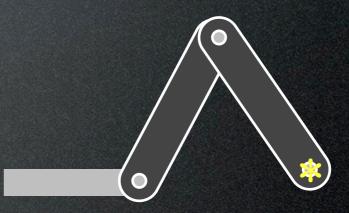
• Composite transformations up the hierarchy



Inverse kinematics

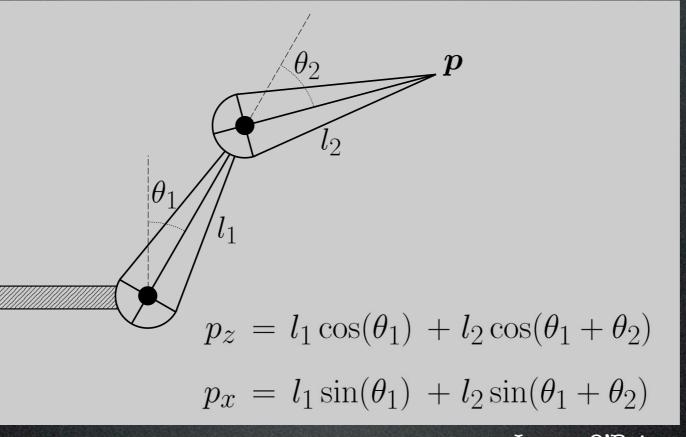
- Given
 - Root transformation
 - Initial configuration
 - Desired location of end point
- Find
 - Internal parameter settings





Inverse kinematics

• A simple two segment arm in 2D



James O'Brien

Direct IK

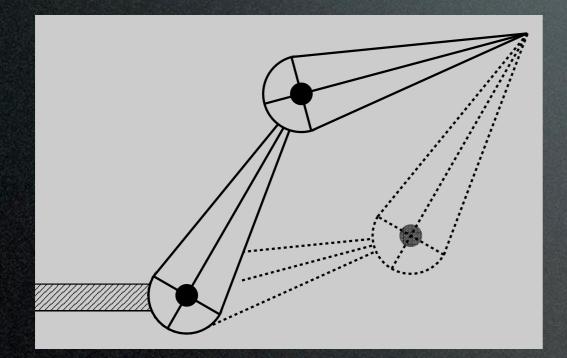
• Just solve for the parameters! What's the problem?

$$\theta_{2} = \cos^{-1} \left(\frac{p_{z}^{2} + p_{x}^{2} - l_{1}^{2} - l_{2}^{2}}{2l_{1}l_{2}} \right)$$

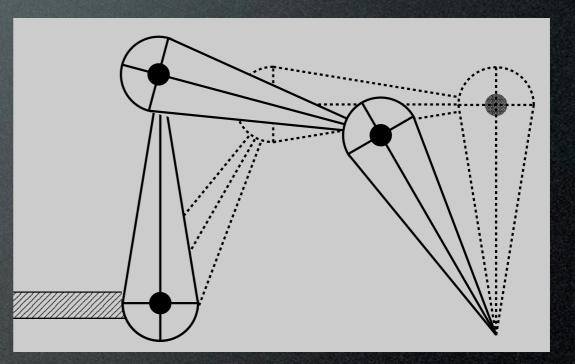
$$\theta_{1} = \frac{-p_{z}l_{2}\sin(\theta_{2}) + p_{x}(l_{1} + l_{2}\cos(\theta_{2}))}{p_{x}l_{2}\sin(\theta_{2}) + p_{z}(l_{1} + l_{2}\cos(\theta_{2}))}$$

Why is this hard?

Multiple disconnected solutions

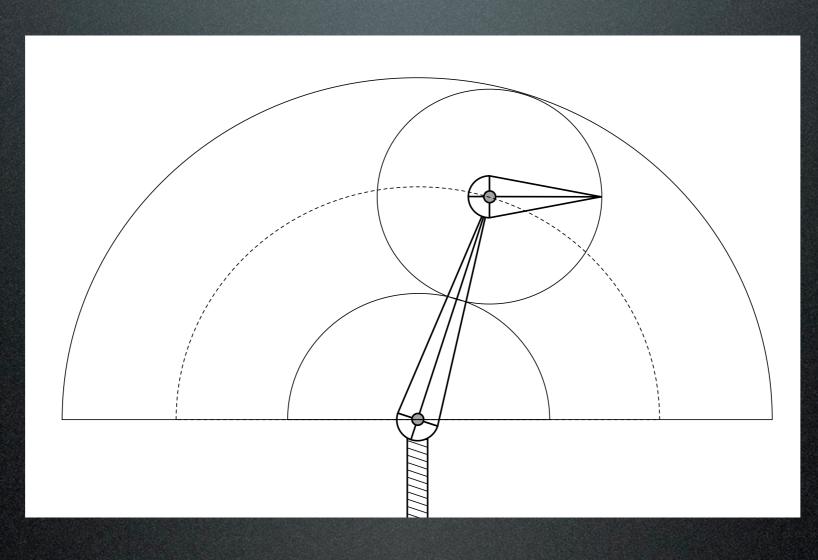


Multiple **connected** solutions



Why is this hard?

Solutions don't always exist



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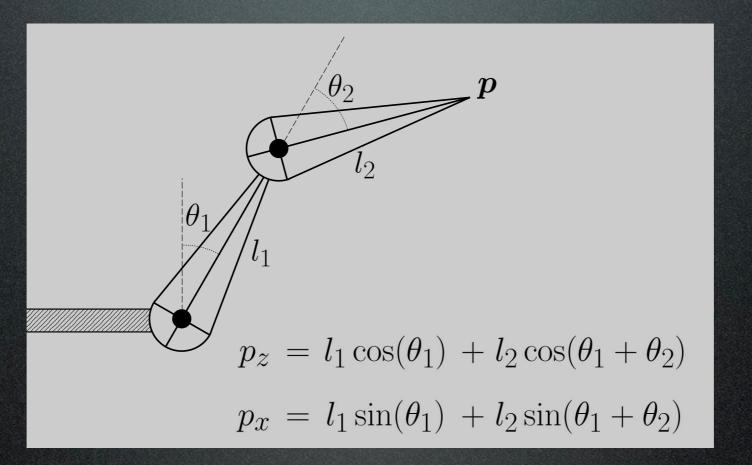
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Numerical IK

- Start in some initial configuration
- Define an error metric (e.g. $\mathbf{p}_{goal} \mathbf{p}_{current}$)
- Compute Jacobian of error w.r.t joint angles θ
- Apply Newton's method (or other procedure)
- Iterate...

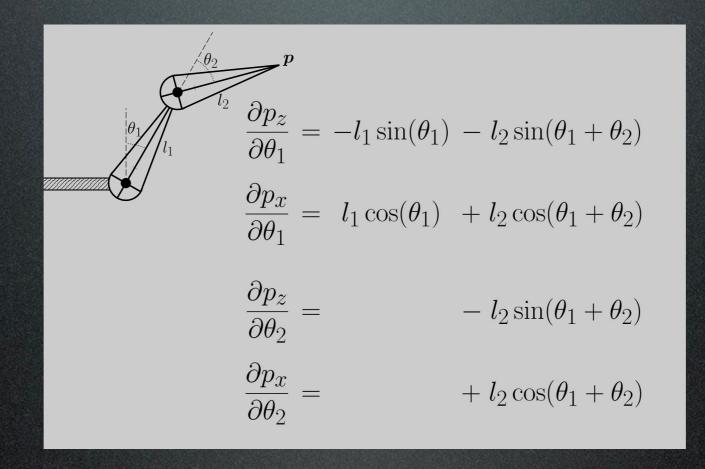
Inverse kinematics

• Recall the simple two segment arm:



Numerical IK

• We can write the derivatives



Numerical IK

$$\frac{\partial p_{z}}{\partial t_{1}} = -l_{1}\sin(\theta_{1}) - l_{2}\sin(\theta_{1} + \theta_{2})$$

$$\frac{\partial p_{x}}{\partial \theta_{1}} = l_{1}\cos(\theta_{1}) + l_{2}\cos(\theta_{1} + \theta_{2})$$

$$\frac{\partial p_{z}}{\partial \theta_{2}} = -l_{2}\sin(\theta_{1} + \theta_{2})$$

$$\frac{\partial p_{x}}{\partial \theta_{2}} = +l_{2}\cos(\theta_{1} + \theta_{2})$$

• If we change the angles by a small amount $d\theta_1$ and $d\theta_2$, this tells us how p_x and p_z change.

The Jacobian

- Matrix of partial derivatives $J_{ij} = \frac{\partial p_i}{\partial \theta_j}$
- For a two segment arm in 2D,

$$\mathbf{J} = \begin{bmatrix} \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} \\ \frac{\partial p_z}{\partial \theta_1} & \frac{\partial p_z}{\partial \theta_2} \end{bmatrix}$$

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The Jacobian

• A small change in θ leads to a small change in \mathbf{p}

$$dp_{x} = \frac{\partial p_{x}}{\partial \theta_{1}} d\theta_{1} + \frac{\partial p_{x}}{\partial \theta_{2}} d\theta_{2} \qquad dp = \begin{bmatrix} \frac{\partial p_{x}}{\partial \theta_{1}} & \frac{\partial p_{x}}{\partial \theta_{2}} \\ \frac{\partial p_{z}}{\partial \theta_{1}} & \frac{\partial p_{z}}{\partial \theta_{2}} \end{bmatrix} \cdot \begin{bmatrix} d\theta_{1} \\ d\theta_{2} \end{bmatrix} = \mathbf{J} \cdot d\theta$$

• So... if we want to change \mathbf{p} , this tells us how to change θ ?

 $d\mathbf{p} = \mathbf{J} \cdot d\theta$ $d\theta = \mathbf{J}^{-1} \cdot d\mathbf{p}?$

The Jacobian

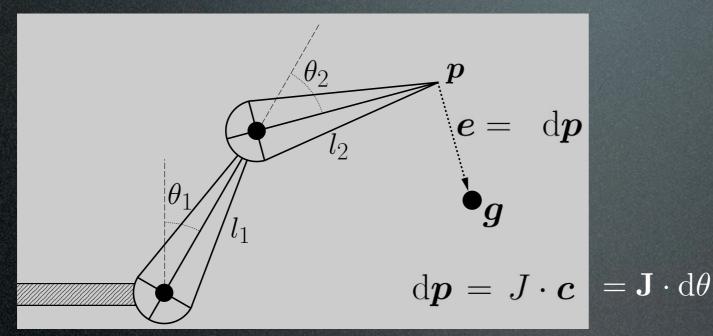
• Put another way, J tells us approximately how much x will change in world space when we adjust a joint parameter q_i.

 $\Delta \boldsymbol{x} \approx \Delta \boldsymbol{q}_i(\boldsymbol{K}_1,\cdots,\boldsymbol{K}_6)$

Approximate Actual

Bill Baxter

Back to inverse kinematics



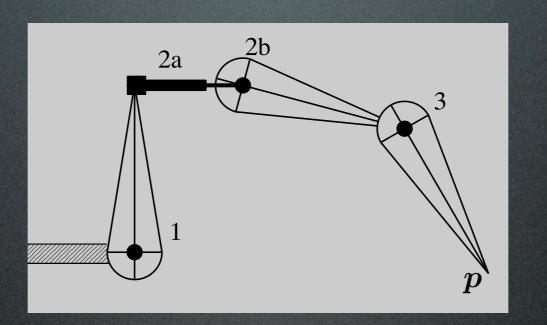
- We want **p** to change by d**p**
- Can we simply change $\boldsymbol{\theta}$ by d $\boldsymbol{\theta} = \mathbf{J}^{-1} d\mathbf{p}$?
 - ...Is **J** invertible?

Inverse kinematics

- Problems:
 - Jacobian may (will!) not be invertible → use pseudo-inverse, or use more robust numerical method
 - Jacobian is not constant \rightarrow take small steps
- Nonlinear optimization, but (mostly) well-behaved

Multiple links

• We need a generic way of building the Jacobian



$$\mathbf{q} = \begin{bmatrix} \theta_1 \\ d_{2a} \\ \theta_{2b} \\ \theta_3 \end{bmatrix} \qquad \mathbf{J} = \begin{bmatrix} \frac{\partial \mathbf{p}}{\partial \theta_1} & \frac{\partial \mathbf{p}}{\partial d_{2a}} & \frac{\partial \mathbf{p}}{\partial \theta_{2b}} & \frac{\partial \mathbf{p}}{\partial \theta_3} \end{bmatrix} = ?$$

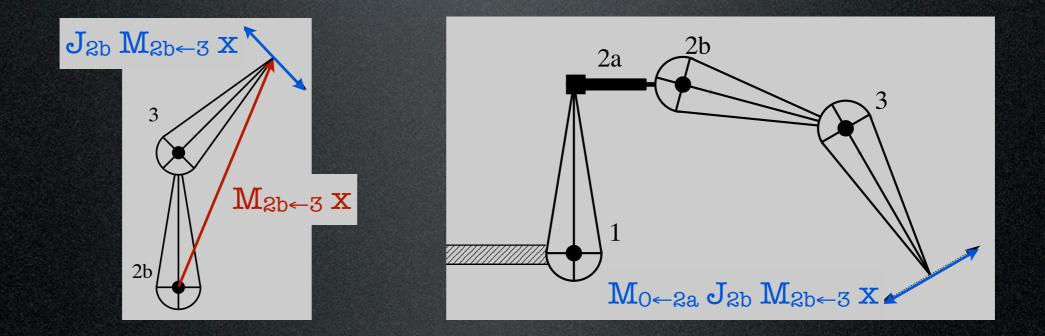
Remember forward kinematics

• World position of point is given by composition of transformations

$$\mathbf{p} = \mathbf{M}_{0\leftarrow 1} \cdot \mathbf{M}_{1\leftarrow 2a} \cdot \mathbf{M}_{2a\leftarrow 2b} \cdot \mathbf{M}_{2b\leftarrow 3} \cdot \mathbf{x}$$

• If joint 2b moves, only $\mathbf{M}_{2a\leftarrow 2b}$ changes

$$\frac{\partial \mathbf{p}}{\partial \theta_{2b}} = \mathbf{M}_{0\leftarrow 1} \cdot \mathbf{M}_{1\leftarrow 2a} \cdot \frac{\partial}{\partial \theta_{2b}} \mathbf{M}_{2a\leftarrow 2b} \cdot \mathbf{M}_{2b\leftarrow 3} \cdot \mathbf{x}$$
$$= \mathbf{M}_{0\leftarrow 1} \cdot \mathbf{M}_{1\leftarrow 2a} \cdot \mathbf{J}_{2b}(\theta_{2b}) \cdot \mathbf{M}_{2b\leftarrow 3} \cdot \mathbf{x}$$



Multiple links

• Compute each joint's Jacobian locally (between outboard and inboard bodies)

$$\begin{array}{ll} \frac{\partial \mathbf{p}}{\partial \theta_1} = & \mathbf{J}_1(\theta_1) \ \mathbf{M}_{1 \leftarrow 3} \mathbf{x} \\ \frac{\partial \mathbf{p}}{\partial d_{2a}} = & \mathbf{M}_{0 \leftarrow 1} \mathbf{J}_{2a}(d_{2a}) \mathbf{M}_{2a \leftarrow 3} \mathbf{x} \\ \frac{\partial \mathbf{p}}{\partial \theta_{2b}} = & \mathbf{M}_{0 \leftarrow 2a} \mathbf{J}_{2b}(\theta_{2b}) \mathbf{M}_{2b \leftarrow 3} \mathbf{x} \\ \frac{\partial \mathbf{p}}{\partial \theta_3} = & \mathbf{M}_{0 \leftarrow 2b} \ \mathbf{J}_3(\theta_3) \ \mathbf{x} \end{array} \qquad \mathbf{q} = \begin{bmatrix} \theta_1 \\ \theta_{2a} \\ \theta_{2b} \\ \theta_3 \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} \frac{\partial \mathbf{p}}{\partial \theta_1} & \frac{\partial \mathbf{p}}{\partial d_{2a}} & \frac{\partial \mathbf{p}}{\partial \theta_{2b}} & \frac{\partial \mathbf{p}}{\partial \theta_3} \end{bmatrix} \qquad (\mathbf{d}\mathbf{p} = \mathbf{J} \cdot \mathbf{d}\mathbf{q})$$

Multiple links

• Compute each joint's Jacobian locally (between outboard and inboard bodies)

$$\mathbf{J} = \begin{bmatrix} \cdot \mathbf{J}_{1}(\theta_{1}) \cdot \mathbf{M}_{1 \leftarrow 3} \mathbf{x}, \\ \mathbf{M}_{0 \leftarrow 1} \cdot \mathbf{J}_{2a}(d_{2a}) \cdot \mathbf{M}_{2a \leftarrow 3} \mathbf{x}, \\ \mathbf{M}_{0 \leftarrow 2a} \cdot \mathbf{J}_{2b}(\theta_{2b}) \cdot \mathbf{M}_{2b \leftarrow 3} \mathbf{x}, \\ \mathbf{M}_{0 \leftarrow 2b} \cdot \mathbf{J}_{3}(\theta_{3}) \cdot \mathbf{x} \end{bmatrix}$$

(each entry here is a column of the matrix)

$$\mathbf{q} = egin{bmatrix} heta_1 \ heta_{2a} \ heta_{2b} \ heta_3 \end{bmatrix}$$

$$d\mathbf{p} = \mathbf{J} \cdot d\mathbf{q}$$