#### 1. (Reading Assignment)

Sections 6.2, 6.3, 6.6 and 6.8 of Chapter 6 as well as sections 11.1 and 11.2 of Chapter 11: Hambley 3<sup>rd</sup> edition.

## 2. Problem 5.53

Since the reactance is negative, the load is capacitive

Power delivered is  $P_d = I_{rms}^2 \times R = (15)^2 \times 100 = 22.5 kW$ 

Reactive power is  $P_r = I_{rms}^2 \times X = (15)^2 \times (-50) = -11.25 kVAR$ Power factor is

$$P_f = \cos(\mathbf{q}) = \cos\left[\tan^{-1}\left(\frac{P_r}{P_d}\right)\right] = \cos\left[\tan^{-1}(-0.5)\right] = \cos\left[26.57^\circ\right] = 89.44\%$$

## 3. Problem 5.56

First let us compute the rms current  $(I_{rms})$ 

$$I = \frac{240\sqrt{2}\angle 50^{\circ} - 220\sqrt{2}\angle 30^{\circ}}{1+j2} = 52.\angle 52.71^{\circ} \Rightarrow I_{rms} = 36.8A$$

Knowing the current  $(I_{rms})$ , we can now compute the power for each source (absorbed or delivered)

- Power delivered by source A  $P_A = 240I_{rms} \times \cos(50 - 52.71) = 8.8kW$  $Q_A = 240I_{rms} \times \sin(50 - 52.71) = -0.42KVAR$
- Power dissipated/absorbed by source B  $P_B = 220I_{rms} \times \cos(30 - 52.71) = 7.5kW$  $Q_B = 220I_{rms} \times \sin(30 - 52.71) = -3.1KVAR$
- Power dissipated/absorbed by the resistor  $P_R = I_{rms}^2 \times R = (36.8)^2 \times 1\Omega = 1.35kW$
- Power dissipated/absorbed by the inductor  $P_r = I_{rms}^2 \times X = (36.8)^2 \times (2\Omega) = 2.7 kVAR$

# 4. Problem 5.68

We are asked to find the Thevenin and Norton of the circuit given: After Zeroing the sources, we have:



Now we can compute the Thevenin impedance as follow:

$$Z_t = \frac{1}{1/10 + 1/j5} = 4.472\angle 63.43^\circ = 2 + j4$$

Using KCL to compute for the current flowing at the upper end of the current source under open circuit conditions, we get:

$$\frac{V_{oc} - 100 \angle 45^{\circ}}{10} + \frac{V_{oc}}{j5} = 5, \text{ Solving for } V_{OC}, \text{ we get}$$
$$V_t = V_{oc} = 62.56 \angle 93.80^{\circ}$$
And  $I_t = \frac{V_t}{Z_t} = 13.99 \angle 30.36^{\circ}$ 

Therefore, the Thevenin and Norton equivalences are given by:



• The maximum power that this circuit can deliver to a load with complex impedance is computed as follow:

$$P_{load} = I_{rms-load}^{2} \times Z_{load}$$

Given 
$$Z_{load} = 2 - j4$$
 and  $I_{load} = \frac{V_t}{Z_t + Z_{load}} = \frac{62.56 \angle 93.80^\circ}{2 + j4 + 2 - j4} = 15.64 \angle 93.80^\circ$   
 $P_{load} = I_{rms-load}^2 \times Z_{load} = 244.6W$ 

• The maximum power that this circuit can deliver to a load with complex impedance is computed as follow:

$$P_{load} = I_{rms-load}^2 \times Z_{load}$$

Given  $Z_{load} = R_{load} = 4.472 \& I_{load} = \frac{V_t}{Z_t + Z_{load}} = \frac{62.56 \angle 93.80^\circ}{2 + j4 + 4.472} = 8.223 \angle -62.08^\circ$  $P_{load} = I_{rms-load}^2 \times R_{load} = 151.2W$ 

### 5. Problem 6.9

The phasors for the steady state input and output of this filter are given as follow:  $V_{in} = 2\angle -25^{\circ}$  and  $V_{out} = 1\angle 20^{\circ}$ 

Therefore, the complex value of the filter transfer function at f=5,000Hz will be given as:

$$H(5,000) = \frac{V_{out}}{V_{in}} = 0.5 \angle 45^{\circ}$$

## 6. Problem 6.12

Given the input signal provided as  $V_{in}(t) = 1 + 2\cos(2000pt) + 3\sin(3000pt) + 4\cos(4000pt)$ One can extract the following frequency components: 0, 1000, 1500 and 2000 Hz The transfer function for each of these frequencies is compute by dividing the corresponding output to the input. This results in the following:

$$H(0) = \frac{3}{1} = 3, \qquad H(1,000) = \frac{4\angle 30^{\circ}}{2\angle 0^{\circ}} = 2\angle 30^{\circ}$$
$$H(1,500) = \frac{3\angle 0^{\circ}}{3\angle -90^{\circ}} = 1\angle 90^{\circ}, \quad H(2,000) = \frac{0}{4\angle 0^{\circ}} = 0$$

#### 7. Problem 6.19

Given the input signal to be  $V_{in}(t) = 1 + 2\cos(2000pt) + 3\sin(3000pt) + 4\cos(4000pt)$  with frequencies components of 250, 500 and 1000 Hz

The half power of the filter frequency is  $f_b = \frac{1}{2pRC} = 500Hz$ 

The transfer function is given by equation 6.9 in the text book  $H(f) = \frac{1}{1 + (f/f_b)}$ 

After computing the transfer function for the different component frequencies of  $V_{in}$ , we get the following:

$$H(250) = \frac{1}{1 + j(\frac{250}{500})} = 0.89 \angle -26.57^{\circ}$$
$$H(500) = \frac{1}{1 + j(\frac{500}{500})} = 0.707 \angle -45^{\circ}$$
$$H(1000) = \frac{1}{1 + j(\frac{1000}{500})} = 0.44 \angle -63.43^{\circ}$$

Applying the appropriate value of the transfer function to each of these component of the input signal allows us to an expression for the output signal which results to:  $V_{out}(t) = 4.472\cos(500pt - 26.57^\circ) + 3.535\cos(1000pt - 45^\circ) + 2.236\cos(2000pt - 63.43^\circ)$ 

### 8. Problem 6.33

To convert to decibels, we need to take 20 times the common logarithm of a transfer function. Therefore, we have:  $20\log(0.5) = -6.021dB$  and  $20\log(2) = +6.021dB$