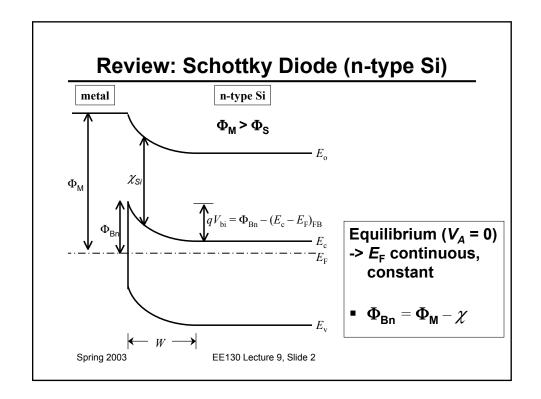
Lecture #9

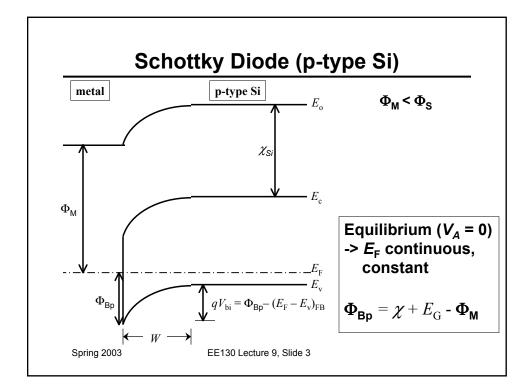
OUTLINE

- Metal-semiconductor contacts (cont.)
 - » I-V characteristics
 - » practical ohmic contacts
 - » small-signal capacitance

Reading: Finish Chapter 14

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Depleted Layer Width, W

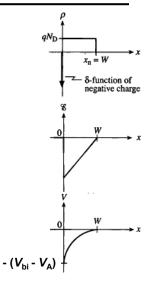
Last time, we found that

$$V(x) = \frac{-qN_D}{2K_S\varepsilon_0}(W-x)^2$$

At
$$x = 0$$
, $V = -(V_{bi} - V_{A})$

$$\Rightarrow W = \sqrt{\frac{2\varepsilon_s(V_{bi} - V_A)}{qN_D}}$$

- W increases with increasing $-V_{\rm A}$ W decreases with increasing $N_{\rm D}$



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W for p-type Semiconductor

$$V(x) = \frac{qN_A}{2K_S\varepsilon_0}(W - x)^2$$

At
$$x = 0$$
, $V = V_{bi} + V_A$

$$\Rightarrow W = \sqrt{\frac{2\varepsilon_s(V_A + V_{bi})}{qN_A}}$$

- W increases with increasing V_A
- W decreases with increasing N_A

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EE130 Lecture 9, Slide 5

Current Flow in a Schottky Diode

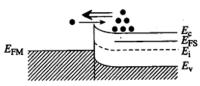
- Diode current is determined by majoritycarrier flow across the MS junction
 - Under forward bias, majority-carrier diffusion from the semiconductor into the metal dominates the current
 - Under reverse bias, majority-carrier diffusion from the metal into the semiconductor dominates the current

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Thermionic Emission Theory

· Electrons can cross the junction if

$$KE_{x} = \frac{1}{2} m v_{x}^{2} \ge q(V_{bi} - V_{A})$$
$$|v_{x}| \ge v_{\min} \equiv \sqrt{\frac{2q}{m_{*}^{*}} (V_{bi} - V_{A})}$$



The current for electrons at a given velocity is:

$$I_{s \bullet \to M, v_x} = -qAv_x n(v_x)$$

So, the total current over the barrier is:

$$I_{s \bullet \to M} = -qA \int_{-\infty}^{-\nu_{\min}} v_x n(v_x) dv_x$$

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EE130 Lecture 9, Slide 7

Schottky Diode I - V

· Given that

$$n(v_x) = \left[\frac{4\pi kT m_n^{*2}}{h^3}\right] e^{(E_F - E_c)/kT} e^{-(m_n^*/2kT)v_x^2}$$

· We obtain

$$I_{S \bullet \to M} = \frac{4\pi q m_n k^2}{h^3} A T^2 e^{-q\Phi_B/kT} e^{qV_A/kT}$$
$$= A T^2 J_S e^{qV_A/kT}, \text{ where } J_S \approx 120 e^{-q\Phi_B/kT} \text{ A/cm}^2$$

• In the other direction, we always see the same barrier $\Phi_{\rm Bn}$: $I_{M\bullet\to S}=-I_{S\bullet\to M}(V_A=0)$

• Therefore
$$I = I_S(e^{qV_A/kT} - 1)$$
 where $I_S = AT^2J_S$

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Applications of Schottky Diodes

- $I_{\rm S}$ of a Schottky diode is 10³ to 108 times larger than a pn junction diode, depending on $\Phi_{\rm B}$.
- ⇒ Schottky diodes are preferred rectifiers for low voltage, high current applications.

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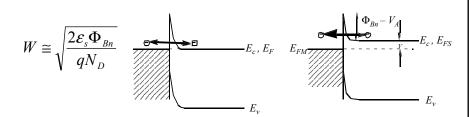
EE130 Lecture 9. Slide 9

Practical Ohmic Contact

· In practice, most M-S contacts are rectifying

- To achieve a contact which conducts easily in both directions, we dope the semiconductor very heavily
 - → W is so narrow that carriers can tunnel directly through the barrier

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tunneling probability $P = e^{-H(\Phi_{Bn}-V_A)/\sqrt{N_D}}$

$$H = 4\pi \sqrt{\varepsilon_s m_n} / h = 5.4 \times 10^9 \sqrt{m_n / m_o} \text{ cm}^{-3/2} \text{V}^{-1}$$
$$J_{S \to M} \approx q N_D v_{thx} P = q N_D \sqrt{kT / 2\pi m_n} e^{-H(\Phi_{Bn} - V_A) / \sqrt{N_D}}$$

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Specific Contact Resistance

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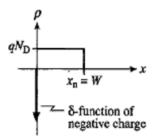
Voltage Drop across an Ohmic Contact

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EE130 Lecture 9, Slide 13

Review: MS-Contact Charge Distribution

- In a Schottky contact, charge is stored on either side of the MS junction
- · This charge is modulated by the applied voltage



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Schottky Diode: Small-Signal Capacitance

- If an A.C. voltage is applied in series with the D.C. bias V_A , the charge stored in the Schottky contact will be modulated
 - → displacement current will flow

$$C = \frac{\mathcal{E}_s}{W} A$$

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EE130 Lecture 9. Slide 15

Using C-V Data to Determine Φ_{B}

$$\frac{1}{C^2} = \frac{2(V_{bi} - V_A)}{qN_D \varepsilon_s A^2}$$

Once $V_{\rm bi}$ is known, $\Phi_{\rm Bn}$ can be determined:

$$qV_{\rm bi} = q\Phi_{\rm Bn} - (E_{\rm c} - E_{\rm F})_{\rm FB} = q\Phi_{\rm Bn} - kT \ln \frac{N_{\rm c}}{N_{\rm D}}$$

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Summary

in the metal, which be thought of as he	n-type Semiconductor	p-type Semiconductor
$\Phi_{\rm M} > \Phi_{\rm S}$	Rectifying	Ohmic
$\Phi_{\mathrm{M}} < \Phi_{\mathrm{S}}$	Ohmic	Rectifying

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