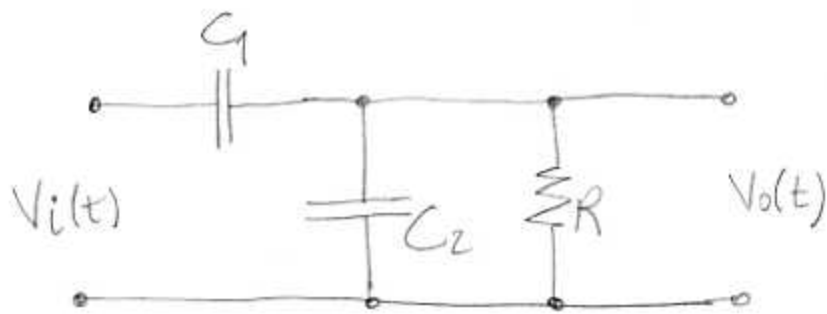


A) Given the following circuit



A.1) Compute the transfer function

$$F(s) = \frac{V_o(s)}{V_i(s)}$$

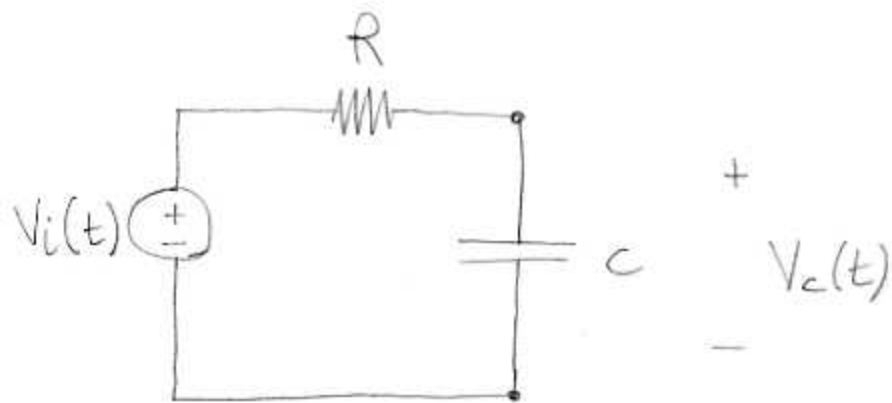
A.2) Compute the frequency response

$$F(j\omega)$$

A.3) Compute $|F(j\omega)|$

A.4 Extra question) Plot $|F(j\omega)|$ and $\angle F(j\omega)$
as a function of ω

B) Given the following circuit:



B.1) Considering the input $V_i(t)$ as in figure B.f1, plot the output $V_c(t)$. (you have to do the work, don't just plot

$V_c(t)$ but compute $V_c(t)$ as a function of time).

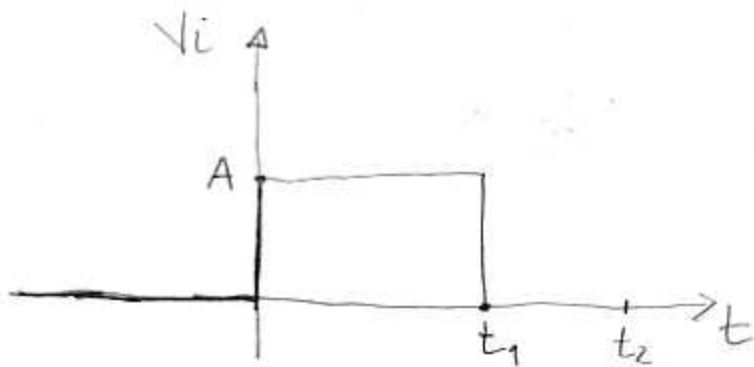
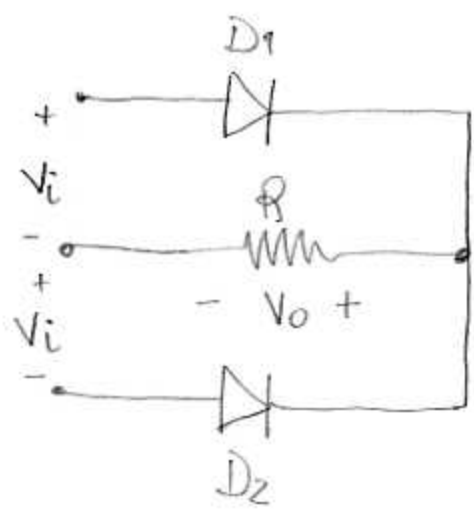


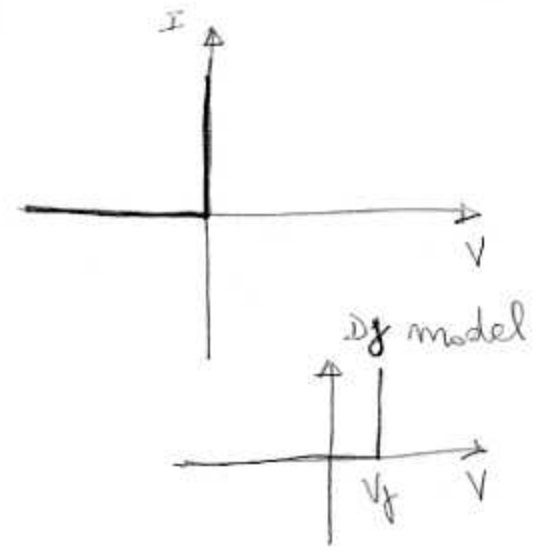
fig. B.f1

B.2) Compute $V_c(t_2)$

C) Consider the following circuit

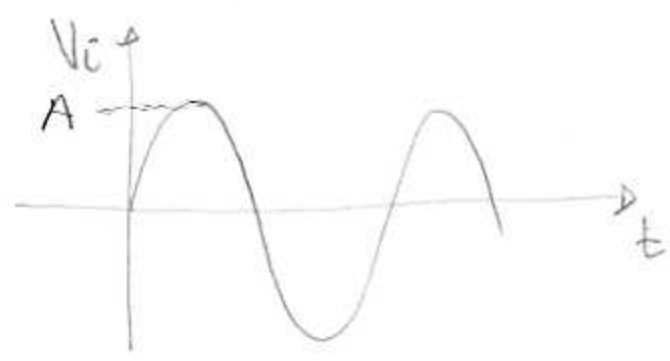


Ideal Diode model



C.1) Using the ideal model for the diode (open-circuit, short-circuit) plot the transfer characteristic (V_o vs. V_i)

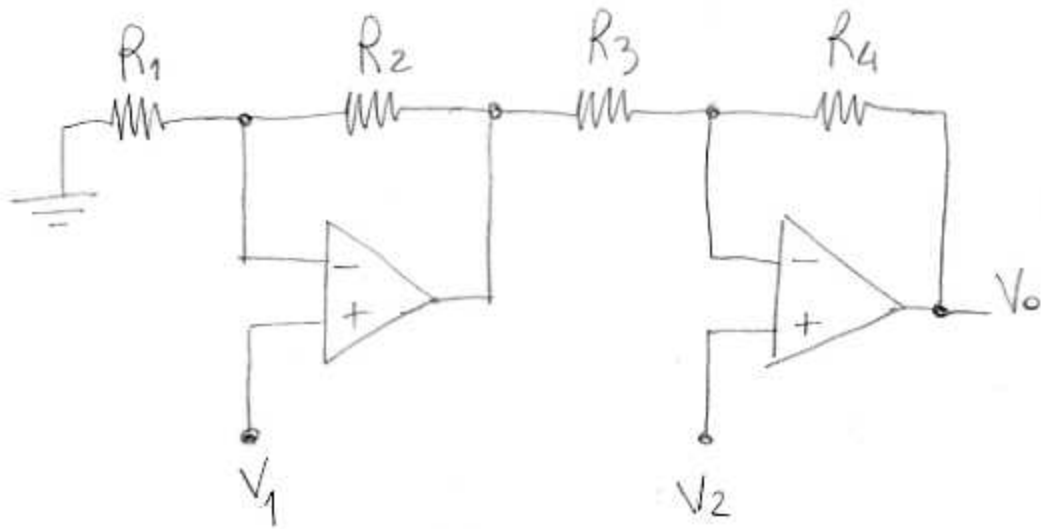
C.2) If the input is a sinusoid:



Plot the output

C.3 Extra question) Plot the transfer characteristic using the D_y model

D) Given the circuit:



with $R_1 = R_4$, $R_2 = R_3$

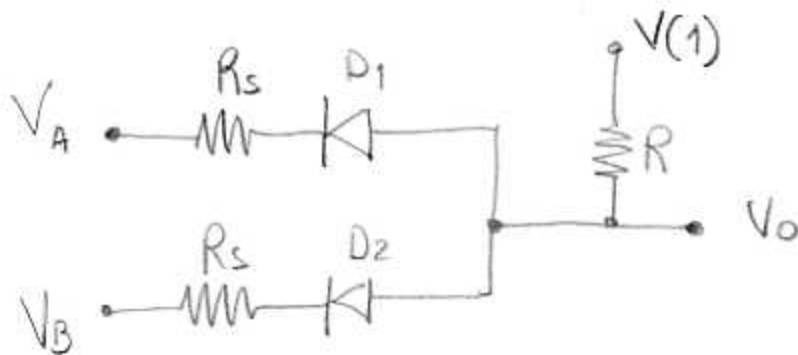
D.1) Compute V_0 as a function of V_1, V_2

D.2) What is the input resistance for V_1 and V_2 ?

D.4 Extra question) If a noise signal $n(t)$ is injected in both V_1 and V_2 , what is the noise at the output?

E Extra of the Extras) Consider a positive ^{MOD.5} logic where the two digits 0 and 1 are encoded by two voltages $V(0)$, $V(1)$ where $V(1) > V(0)$.

Given the following logic device:

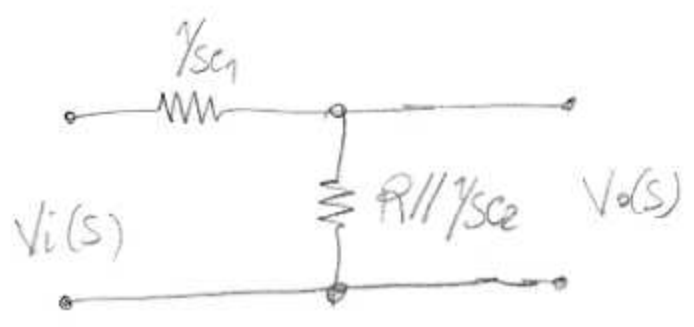
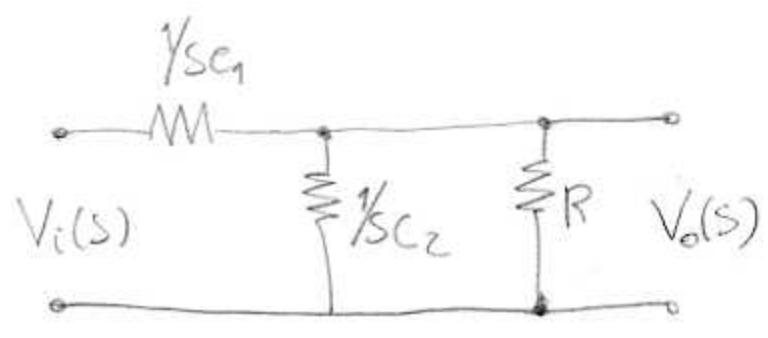


E.1) Write the truth table of this device :

A	B	O

(Considering the diode ideal and $R \gg R_s$.)

A.1) Using Laplace transform:



$$R // \frac{1}{sC_2} = Z_2 = \frac{R}{sC_2 R + 1}$$

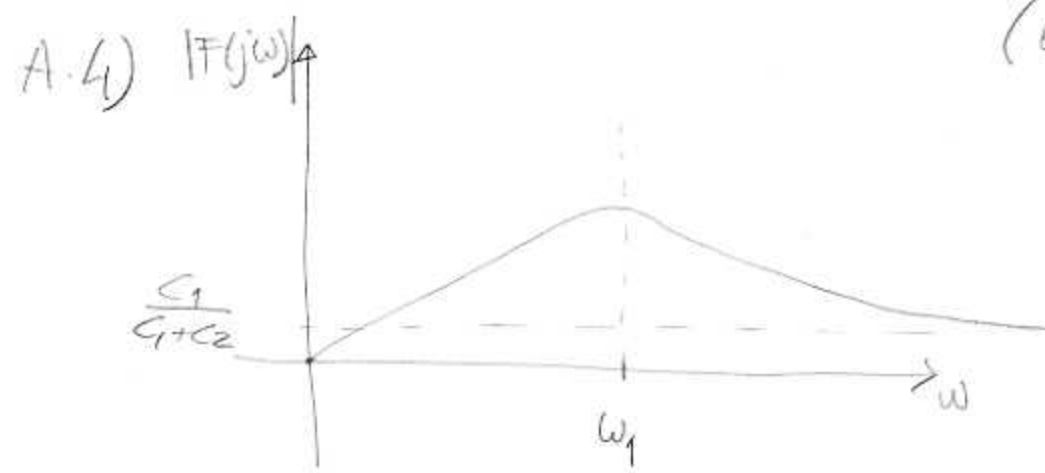
$$V_o(s) = \frac{Z_2}{\frac{1}{sC_1} + Z_2} V_i(s)$$

$$F(s) = \frac{R}{\left(\frac{1}{sC_1} + \frac{R}{sC_2 R + 1}\right)} =$$

$$= \frac{sC_1 R}{sC_2 R + 1 + sC_1 R} = \frac{sC_1 R}{sR(C_1 + C_2) + 1}$$

A.2)
$$F(j\omega) = \frac{j\omega C_1 R}{j\omega R (C_1 + C_2) + 1}$$

$$A.3) |F(j\omega)| = \frac{\omega C_1 R}{\sqrt{1 + \omega^2 R^2 (C_1 + C_2)^2}}$$



(Assuming you don't know anything about Bode diagram)

$$\frac{d|F(j\omega)|}{d\omega} = \frac{\omega R C_1 \frac{2\omega R^2 (C_1 + C_2)^2}{\sqrt{1 + \omega^2 R^2 (C_1 + C_2)^2}} - C_1 R \sqrt{1 + \omega^2 R^2 (C_1 + C_2)^2}}{1 + \omega^2 R^2 (C_1 + C_2)^2}$$

$$\frac{d|F(j\omega)|}{d\omega} = 0 \Rightarrow \frac{2\omega^3 R^3 C_1 (C_1 + C_2)^2}{\sqrt{1 + \omega^2 R^2 (C_1 + C_2)^2}} = C_1 R \sqrt{1 + \omega^2 R^2 (C_1 + C_2)^2}$$

$$\Rightarrow 2\omega^2 R^3 C_1 (C_1 + C_2)^2 - C_1 R (1 + \omega^2 R^2 (C_1 + C_2)^2)$$

$$\Rightarrow 2R^2 (C_1 + C_2)^2 \omega^2 = 1 + \omega^2 R^2 (C_1 + C_2)^2$$

$$\Rightarrow R^2 (C_1 + C_2)^2 \omega^2 = 1 \Rightarrow \omega_1 = \sqrt{\frac{1}{R^2 (C_1 + C_2)^2}} = \frac{1}{R(C_1 + C_2)}$$

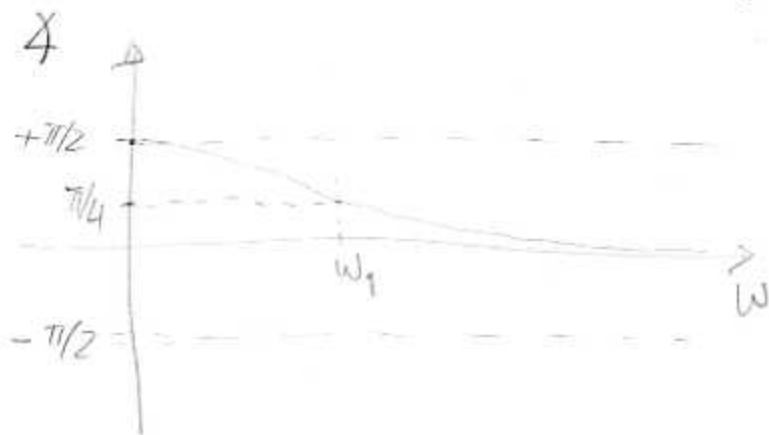
↑
this is a
max

for $\omega \rightarrow 0$ $|F(j\omega)| \rightarrow 0$ also for $\omega \rightarrow \infty$

M102-9

$$\lim_{\omega \rightarrow \infty} \frac{\omega C_1 R}{\sqrt{1 + \omega^2 R^2 (C_1 + C_2)^2}} = \lim_{\omega \rightarrow \infty} \frac{C_1 R}{\sqrt{\frac{1}{\omega^2} + R^2 (C_1 + C_2)^2}} = \frac{C_1}{C_1 + C_2}$$

$$\angle F(j\omega) = \pi/2 - \tan^{-1} \left(\frac{1}{\omega R (C_1 + C_2)} \right)$$



B.1) Using N.V.A.

$$\frac{V_i(t) - V_c(t)}{R} = i_c(t) = C \frac{dV_c(t)}{dt}$$

$$\frac{dV_c(t)}{dt} + \frac{1}{RC} V_c(t) = \frac{V_i(t)}{RC}$$

If in the example I did using the inductor, you replace $I(t)$ with $V_c(t)$ you obtain the same solution.

$$V_c(t) = K_1 e^{\alpha t} + K_2$$

0 \leq t $<$ t₁

$$V_i(t) = A$$

$K_2 = A$ because if $V_c(t) = K_2$ then

$$\cancel{\frac{dK_2}{dt}} + \frac{K_2}{RC} = \frac{A}{RC}$$

$$\frac{d K_1 e^{\alpha t}}{dt} + \frac{1}{RC} K_1 e^{\alpha t} = 0 \Rightarrow \cancel{K_1 \alpha e^{\alpha t}} + \frac{K_1}{RC} e^{\alpha t} = 0$$

$$\alpha = -1/RC$$

$$V_c(t) = K_1 e^{-t/RC} + A \quad \text{but } V_c(0) = 0 \Rightarrow K_1 = -A$$

$$V_c(t) = A(1 - e^{-t/\tau})$$

$$\text{In } t_1 \Rightarrow V_c(t_1) = A(1 - e^{-t_1/\tau})$$

now we shift the time to t_1

$$\boxed{t \geq t_1} \quad V_i(t) = 0$$

$$\frac{dV_c(t)}{dt} + \frac{1}{RC} V_c(t) = 0$$

$$V_c(t_1) = A(1 - e^{-t_1/\tau})$$

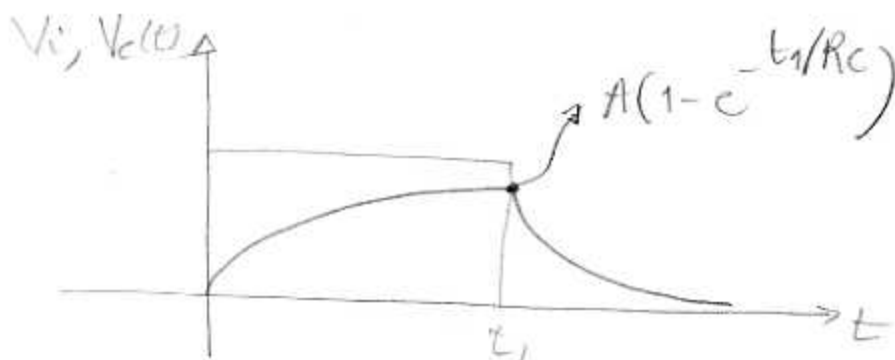
$$V_c(t) = K_1 e^{-t/RC} \Rightarrow V_c(t_1) = K_1 e^{-t_1/RC}$$

$$\parallel$$

$$A(1 - e^{-t_1/RC})$$

$$\Rightarrow K_1 = \frac{A(1 - e^{-t_1/RC})}{e^{-t_1/RC}} = A e^{t_1/RC} - A$$

$$V_c(t) = (A e^{t_1/RC} - A) e^{-t/RC} = A e^{(t_1-t)/RC} - A e^{-t/RC}$$



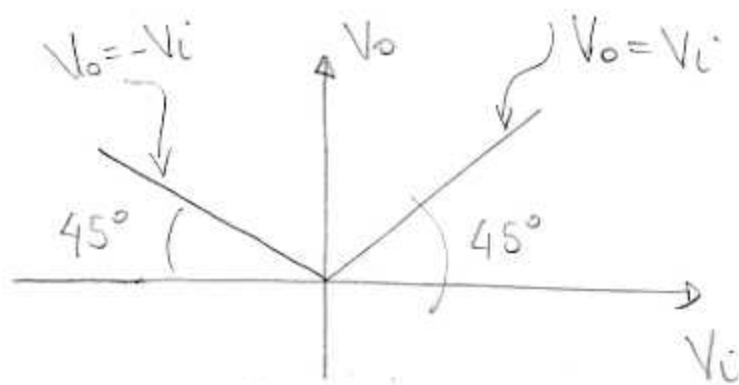
$$B.2) V_c(t_2) = (Ae^{t_1/RC} - A) e^{-t_2/RC} = Ae^{t_1-t_2/RC} - Ae^{-t_2/RC} \quad \text{Mid 11}$$

C.1) If $V_i > 0 \Rightarrow D_1$ is on and D_2 is off

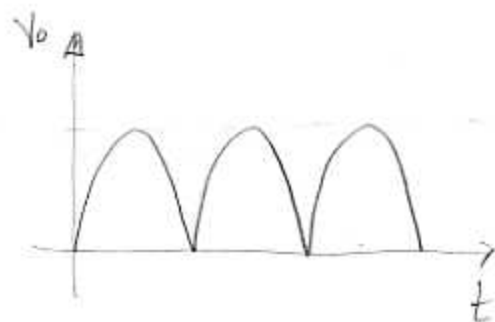
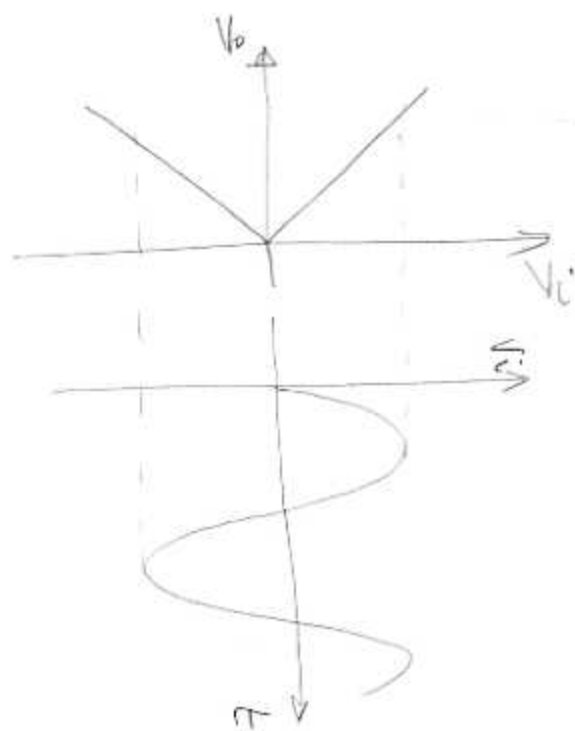
$$V_o = V_i$$

If $V_i < 0 \Rightarrow D_2$ is on and D_1 is off

$$V_o = -V_i$$



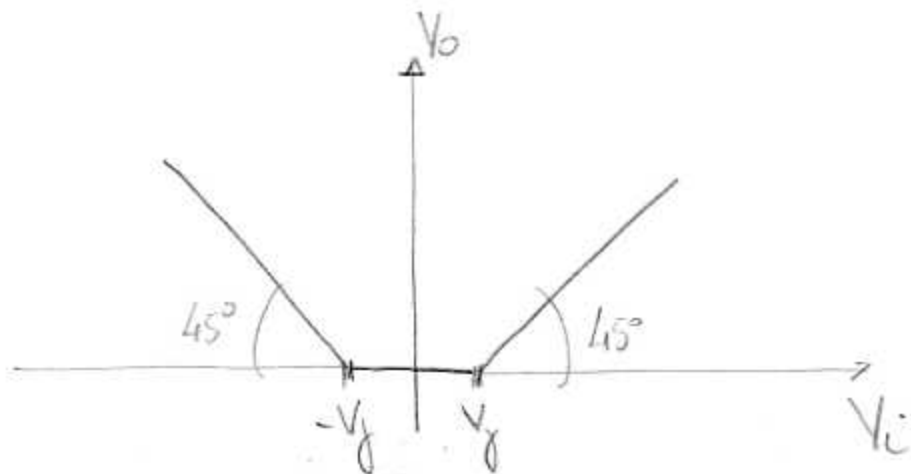
C.2)



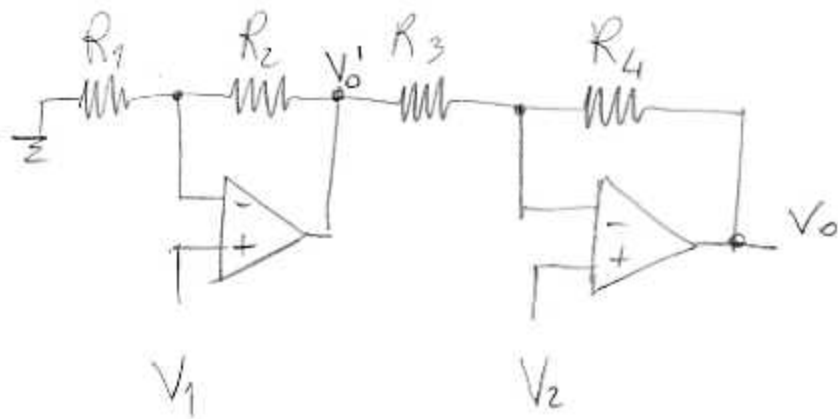
(3) If we use D_1 model then V_i has to be greater than V_f in order for D_1 to be on, and less than $-V_f$ in order for D_2 to be on.

If for instance D_1 is on then $V_o = V_i - V_f$

The transfer characteristic is like the following



D.1)



By superposition:

$$V_1 = 0 \quad V_2 \neq 0$$

$$V_0' = 0, \quad V_0 = V_2 \left(1 + \frac{R_4}{R_3} \right) \quad (\text{non inverting ampl.})$$

$$V_2 = 0 \quad V_1 \neq 0$$

$$V_0' = V_1 \left(1 + \frac{R_2}{R_1} \right) \quad \text{non inverting ampl.}$$

$$V_0 = -V_0' \left(\frac{R_4}{R_3} \right) \quad \text{inverting ampl.}$$

$$V_0 = V_2 \left(1 + \frac{R_4}{R_3} \right) - V_1 \left(1 + \frac{R_2}{R_1} \right) \frac{R_4}{R_3} =$$

$$= V_2 \left(1 + \frac{R_4}{R_3} \right) - V_1 \left(\frac{R_4}{R_3} + 1 \right) = (V_2 - V_1) \left(1 + \frac{R_4}{R_3} \right)$$

D.2) Since the op amp is ideal, $I_+ is zero,$

So

$$R_{in1} = \infty$$

$$R_{in2} = \infty$$

D.4)

$$\begin{aligned}
 V_o &= (V_2' - V_1') \left(1 + \frac{R_1}{R_2} \right) = (V_2 + m(t) - V_1 - m(t)) \left(1 + \frac{R_1}{R_2} \right) \\
 &= (V_2 - V_1) \left(1 + \frac{R_1}{R_2} \right)
 \end{aligned}$$

So the output noise is zero.

E.1) If $V_A = V_B = V(0)$ then D_1 and D_2 are
 (0,0) on so

$$V_o = V(0) + (V(1) - V(0)) \frac{R_s // R_s}{R + R_s // R_s} =$$

$$= V(0) + (V(1) - V(0)) \frac{R_s}{2R + R_s} \approx V(0)$$

\uparrow
 $R \gg R_s$

(0,1) If $V_A = V(0)$ and $V_B = V(1)$
 then D_1 is on and D_2 is off

$$V_o = V(0) + (V(1) - V(0)) \frac{R_s}{R + R_s} \approx V(0)$$

(1,0) is symmetric to the previous case, so
 D_2 is on and D_1 is off.

(1,1) D_1 and D_2 are both on $\Rightarrow V_o = V(1)$

A	B	O
0	0	0
0	1	0
1	0	0
1	1	1

it is an AND gate