

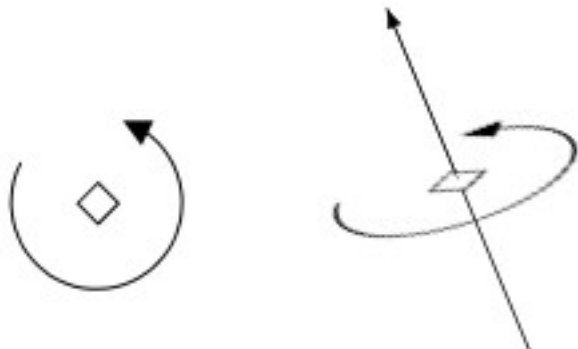
Rotations

- Rotations still orthonormal
- $\text{Det}(\mathbf{R}) = 1 \neq -1$
- Preserve lengths and distance to origin
- 3D rotations DO NOT COMMUTE!
- Right-hand rule DO NOT COMMUTE!
- Unique matrices



Axis-aligned 3D Rotations

- 2D rotations implicitly rotate about a third out of plane axis



Axis-aligned 3D Rotations

- 2D rotations implicitly rotate about a third out of plane axis

$$\mathbf{R} = \begin{bmatrix} \cos(\theta) & -\sin(\theta) \\ \sin(\theta) & \cos(\theta) \end{bmatrix} \quad \mathbf{R} = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

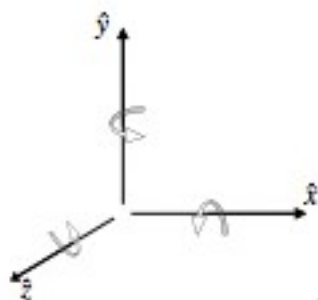


Axis-aligned 3D Rotations

$$\mathbf{R}_x = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & -\sin(\theta) \\ 0 & \sin(\theta) & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_y = \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_z = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



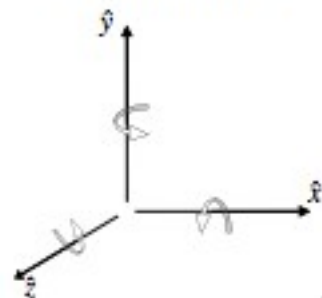
Axis-aligned 3D Rotations

$$\mathbf{R}_z = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & -\sin(\theta) \\ 0 & \sin(\theta) & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_y = \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_x = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

"Z is in your face"



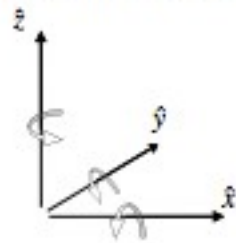
Axis-aligned 3D Rotations

$$\mathbf{R}_z = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & -\sin(\theta) \\ 0 & \sin(\theta) & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_y = \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_x = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Also right handed "Zup"



Axis-aligned 3D Rotations

- Also known as "direction-cosine" matrices

$$\mathbf{R}_x = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\theta) & -\sin(\theta) \\ 0 & \sin(\theta) & \cos(\theta) \end{bmatrix} \quad \mathbf{R}_y = \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & 0 & \cos(\theta) \end{bmatrix}$$

$$\mathbf{R}_z = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Arbitrary Rotations

- Can be built from axis-aligned matrices:

$$\mathbf{R} = \mathbf{R}_{\hat{z}} \cdot \mathbf{R}_{\hat{y}} \cdot \mathbf{R}_{\hat{x}}$$

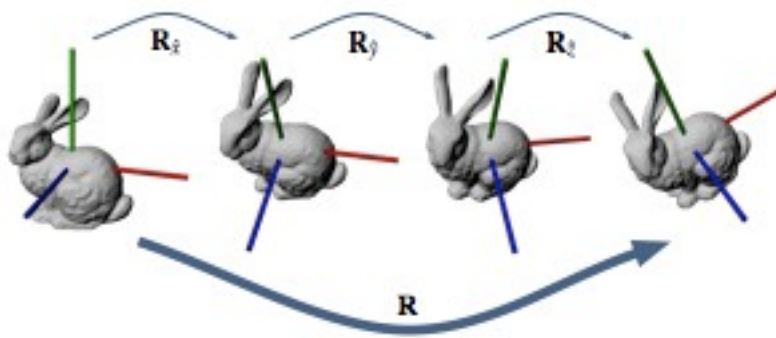
- Result due to Euler... hence called Euler Angles
- Easy to store in vector
- But NOT a vector:

$$\mathbf{R} = \text{rot}(x, y, z)$$



Arbitrary Rotations

$$\mathbf{R} = \mathbf{R}_{\hat{z}} \cdot \mathbf{R}_{\hat{y}} \cdot \mathbf{R}_{\hat{x}}$$



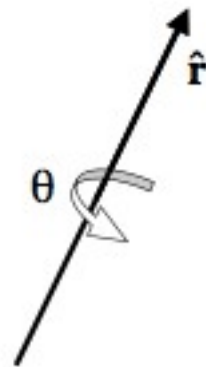
Arbitrary Rotations

- Allows tumbling
- Euler angles are non-unique
- Gimbal-lock
- Moving -vs- fixed axes
 - Reverse of each other

Exponential Maps

- Direct representation of arbitrary rotation
- AKA: axis-angle, angular displacement vector
- Rotate θ degrees about some axis
- Encode θ by length of vector

$$\theta = |\mathbf{r}|$$



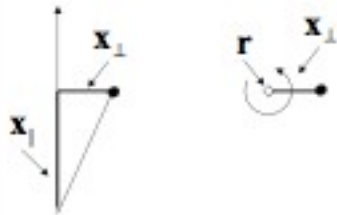
Exponential Maps

- Given vector \mathbf{r} , how to get matrix \mathbf{R}
- Method from text:
 1. rotate about x axis to put \mathbf{r} into the x - y plane
 2. rotate about z axis align \mathbf{r} with the x axis
 3. rotate θ degrees about x axis
 4. undo #2 and then #1
 5. composite together

Exponential Maps

• Rodriguez Formula

$$\mathbf{x}' = \hat{\mathbf{r}}(\hat{\mathbf{r}} \cdot \mathbf{x}) + \sin(\theta)(\hat{\mathbf{r}} \times \mathbf{x}) - \cos(\theta)(\hat{\mathbf{r}} \times (\hat{\mathbf{r}} \times \mathbf{x}))$$

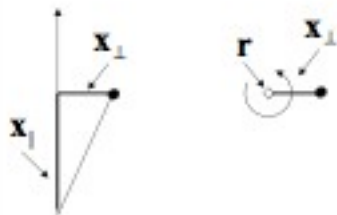


Actually a minor variation ...

Exponential Maps

• Rodriguez Formula

$$\mathbf{x}' = \hat{\mathbf{r}}(\hat{\mathbf{r}} \cdot \mathbf{x}) + \sin(\theta)(\hat{\mathbf{r}} \times \mathbf{x}) - \cos(\theta)(\hat{\mathbf{r}} \times (\hat{\mathbf{r}} \times \mathbf{x}))$$



Linear in \mathbf{x}

Actually a minor variation ...

Exponential Maps

- Building the matrix

$$\mathbf{x}' = ((\hat{\mathbf{r}}\hat{\mathbf{r}}^t) + \sin(\theta)(\hat{\mathbf{r}}\times) - \cos(\theta)(\hat{\mathbf{r}}\times)(\hat{\mathbf{r}}\times)) \mathbf{x}$$

$$(\hat{\mathbf{r}}\times) = \begin{bmatrix} 0 & -\hat{r}_z & \hat{r}_y \\ \hat{r}_z & 0 & -\hat{r}_x \\ -\hat{r}_y & \hat{r}_x & 0 \end{bmatrix}$$

Antisymmetric matrix

$$(\mathbf{a}\times)\mathbf{b} = \mathbf{a}\times\mathbf{b}$$

Easy to verify by expansion

Exponential Maps

- Allows tumbling
- No gimbal-lock!
- Orientations are space within π -radius ball
- Nearly unique representation
- Singularities on shells at 2π
- Nice for interpolation

Exponential Maps

- Why exponential?
- Recall series expansion of e^x

$$e^x = 1 + \frac{x}{1!} + \frac{x^2}{2!} + \frac{x^3}{3!} + \dots$$

.

Exponential Maps

- Why exponential?
- Recall series expansion of e^x
- Euler: what happens if you put in $i\theta$ for x

$$\begin{aligned} e^{i\theta} &= 1 + \frac{i\theta}{1!} + \frac{-\theta^2}{2!} + \frac{-i\theta^3}{3!} + \frac{\theta^4}{4!} + \dots \\ &= \left(1 + \frac{-\theta^2}{2!} + \frac{\theta^4}{4!} + \dots\right) + i\left(\frac{\theta}{1!} + \frac{-\theta^3}{3!} + \dots\right) \\ &= \cos(\theta) + i\sin(\theta) \end{aligned}$$

.

Exponential Maps

- Why exponential?

$$e^{(\hat{\mathbf{r}} \times) \theta} = \mathbf{I} + \frac{(\hat{\mathbf{r}} \times) \theta}{1!} + \frac{(\hat{\mathbf{r}} \times)^2 \theta^2}{2!} + \frac{(\hat{\mathbf{r}} \times)^3 \theta^3}{3!} + \frac{(\hat{\mathbf{r}} \times)^4 \theta^4}{4!} + \dots$$

But notice that: $(\hat{\mathbf{r}} \times)^3 = -(\hat{\mathbf{r}} \times)$

$$e^{(\hat{\mathbf{r}} \times) \theta} = \mathbf{I} + \frac{(\hat{\mathbf{r}} \times) \theta}{1!} + \frac{(\hat{\mathbf{r}} \times)^2 \theta^2}{2!} + \frac{-(\hat{\mathbf{r}} \times) \theta^3}{3!} + \frac{-(\hat{\mathbf{r}} \times)^2 \theta^4}{4!} + \dots$$

21

Exponential Maps

$$e^{(\hat{\mathbf{r}} \times) \theta} = \mathbf{I} + \frac{(\hat{\mathbf{r}} \times) \theta}{1!} + \frac{(\hat{\mathbf{r}} \times)^2 \theta^2}{2!} + \frac{-(\hat{\mathbf{r}} \times) \theta^3}{3!} + \frac{-(\hat{\mathbf{r}} \times)^2 \theta^4}{4!} + \dots$$

$$e^{(\hat{\mathbf{r}} \times) \theta} = (\hat{\mathbf{r}} \times) \left(\frac{\theta}{1!} - \frac{\theta^3}{3!} + \dots \right) + \mathbf{I} + (\hat{\mathbf{r}} \times)^2 \left(\frac{\theta^2}{2!} - \frac{\theta^4}{4!} + \dots \right)$$

$$e^{(\hat{\mathbf{r}} \times) \theta} = (\hat{\mathbf{r}} \times) \sin(\theta) + \mathbf{I} + (\hat{\mathbf{r}} \times)^2 (1 - \cos(\theta))$$

22

Quaternions

- More popular than exponential maps
- Natural extension of $e^{i\theta} = \cos(\theta) + i\sin(\theta)$
- Due to Hamilton (1843)
 - Interesting history
 - Involves "hermaphroditic monsters"

23

Quaternions

- Uber-Complex Numbers

$$q = (z_1, z_2, z_3, s) = (\mathbf{z}, s)$$

$$q = iz_1 + jz_2 + kz_3 + s$$

$$i^2 = j^2 = k^2 = -1 \quad \begin{array}{ll} ij = k & ji = -k \\ jk = i & kj = -i \\ ki = j & ik = -j \end{array}$$

24

Quaternions

- Multiplication natural consequence of defn.

$$\mathbf{q} \cdot \mathbf{p} = (\mathbf{z}_q s_p + \mathbf{z}_p s_q + \mathbf{z}_p \times \mathbf{z}_q, s_p s_q - \mathbf{z}_p \cdot \mathbf{z}_q)$$

- Conjugate

$$\mathbf{q}^* = (-\mathbf{z}, s)$$

- Magnitude

$$\|\mathbf{q}\|^2 = \mathbf{z} \cdot \mathbf{z} + s^2 = \mathbf{q} \cdot \mathbf{q}^*$$

21

Quaternions

- Vectors as quaternions

$$\mathbf{v} = (\mathbf{v}, 0)$$

- Rotations as quaternions

$$\mathbf{r} = (\hat{\mathbf{r}} \sin \frac{\theta}{2}, \cos \frac{\theta}{2})$$

- Rotating a vector

$$\mathbf{x}' = \mathbf{r} \cdot \mathbf{x} \cdot \mathbf{r}^*$$

- Composing rotations

$$\mathbf{r} = \mathbf{r}_1 \cdot \mathbf{r}_2$$

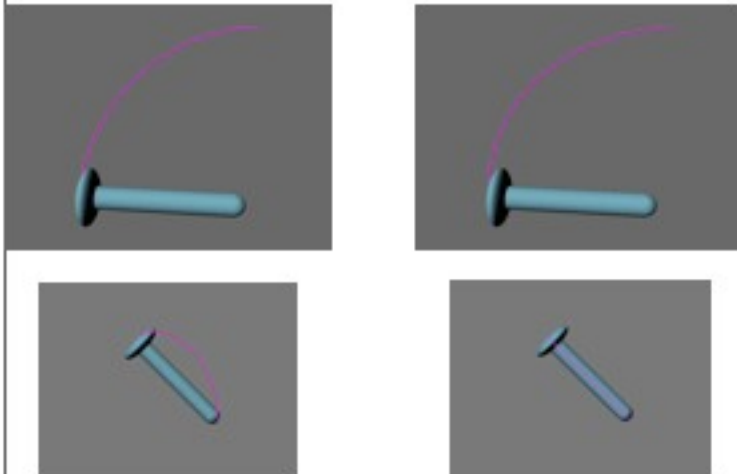
Compare to Exp. Map

22

Quaternions

- No tumbling
- No gimbal-lock
- Orientations are "double unique"
- Surface of a 3-sphere in 4D $\|r\| = 1$
- Nice for interpolation

Interpolation



Rotation Matrices

- Eigen system
 - One real eigenvalue
 - Real axis is axis of rotation
 - Imaginary values are 2D rotation as complex number
- Logarithmic formula

$$(\hat{\mathbf{f}} \times) = \ln(\mathbf{R}) = \frac{\theta}{2 \sin \theta} (\mathbf{R} - \mathbf{R}^T)$$
$$\theta = \cos^{-1} \left(\frac{\text{Tr}(\mathbf{R}) - 1}{2} \right)$$

Similar formulae as for exponential... »

Rotation Matrices

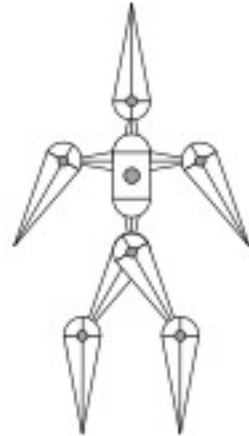
- Consider:

$$\mathbf{R}\mathbf{I} = \begin{bmatrix} r_{xx} & r_{xy} & r_{xz} \\ r_{yx} & r_{yy} & r_{yz} \\ r_{zx} & r_{zy} & r_{zz} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

- Columns are coordinate axes after transformation
(true for general matrices)
- Rows are original axes in original system
(not true for general matrices)

Forward Kinematics

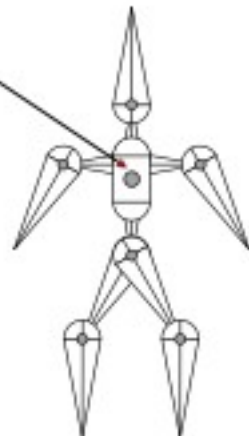
- Articulated skeleton
 - Topology (what's connected to what)
 - Geometric relations from joints
 - Independent of display geometry
 - Tree structure
 - Loop joints break "tree-ness"



31

Forward Kinematics

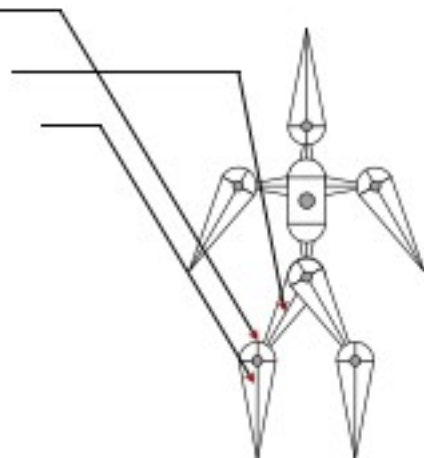
- Root body
 - Position set by "global" transformation
- Root joint
 - Position
 - Rotation
- Other bodies relative to root
- *Inboard* toward the root
- *Outboard* away from root



32

Forward Kinematics

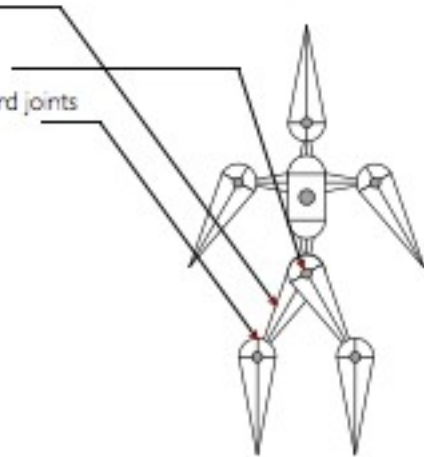
- A joint
 - Joint's inboard body
 - Joint's outboard body



33

Forward Kinematics

- A body
 - Body's inboard joint
 - Body's outboard joint
 - May have several outboard joints

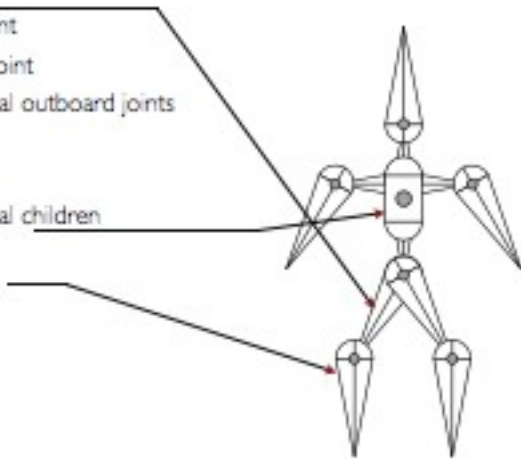


34

Forward Kinematics

- A body

- Body's inboard joint
- Body's outboard joint
 - May have several outboard joints
- Body's parent
- Body's child
 - May have several children

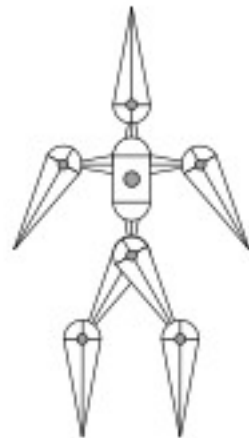


20

Forward Kinematics

- Interior joints

- Typically not 6 DOF joints
- Pin - rotate about one axis
- Ball - arbitrary rotation
- Prism - translation along one axis

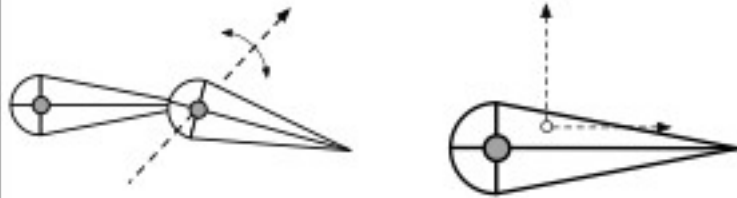


20

Forward Kinematics

• Pin Joints

- Translate inboard joint to local origin
- Apply rotation about axis
- Translate origin to location of joint on outboard body

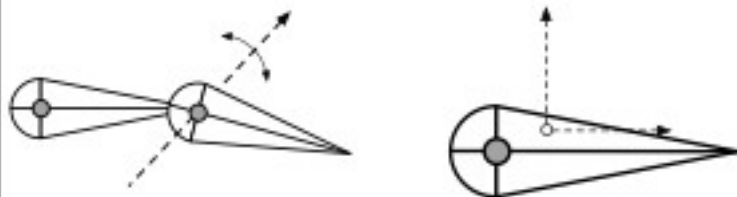


27

Forward Kinematics

• Ball Joints

- Translate inboard joint to local origin
- Apply rotation about arbitrary axis
- Translate origin to location of joint on outboard body

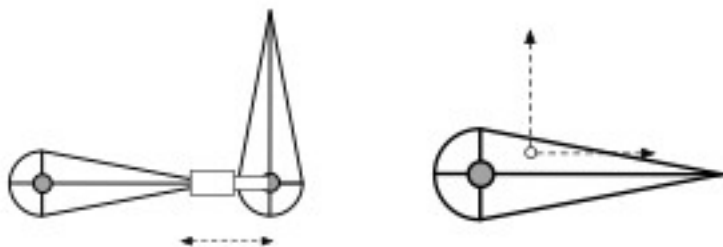


28

Forward Kinematics

- Prismatic Joints

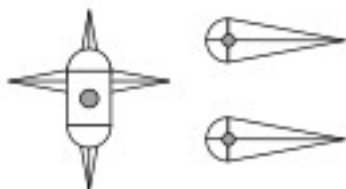
- Translate inboard joint to local origin
- Translate along axis
- Translate origin to location of joint on outboard body



39

Forward Kinematics

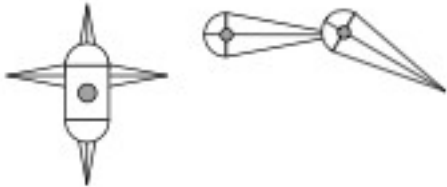
- Composite transformations up the hierarchy



40

Forward Kinematics

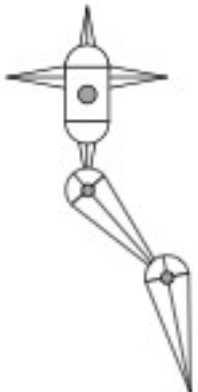
- Composite transformations up the hierarchy



41

Forward Kinematics

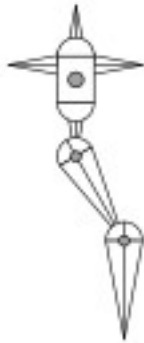
- Composite transformations up the hierarchy



42

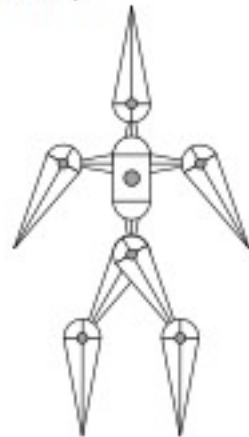
Forward Kinematics

- Composite transformations up the hierarchy



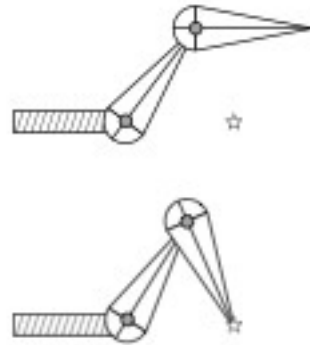
Forward Kinematics

- Composite transformations up the hierarchy

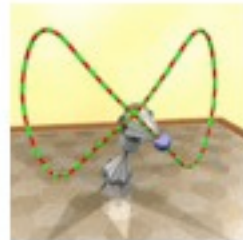


Inverse Kinematics

- Given
 - Root transformation
 - Initial configuration
 - Desired end point location
- Find
 - Interior parameter settings

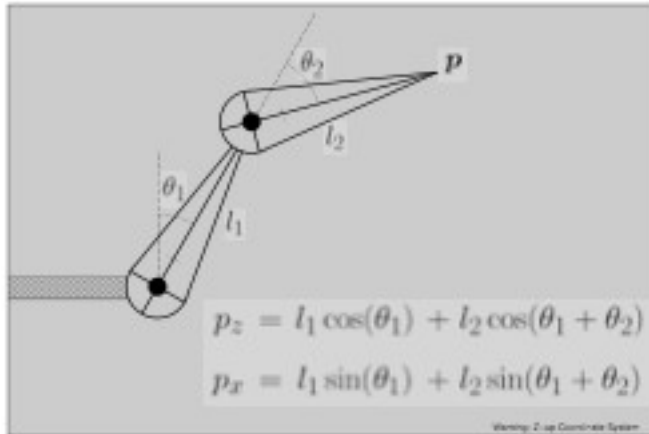


Inverse Kinematics



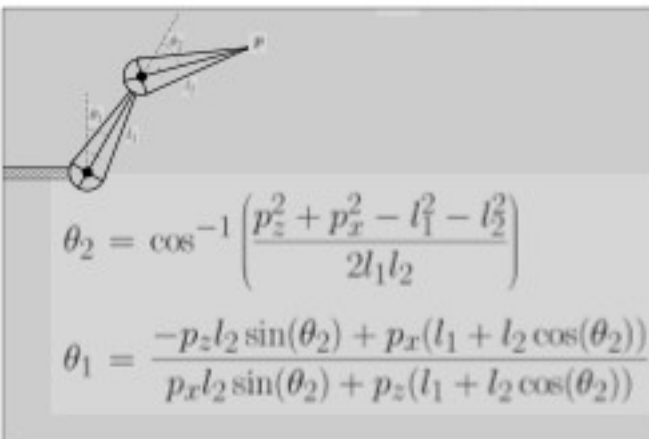
Inverse Kinematics

- A simple two segment arm in 2D



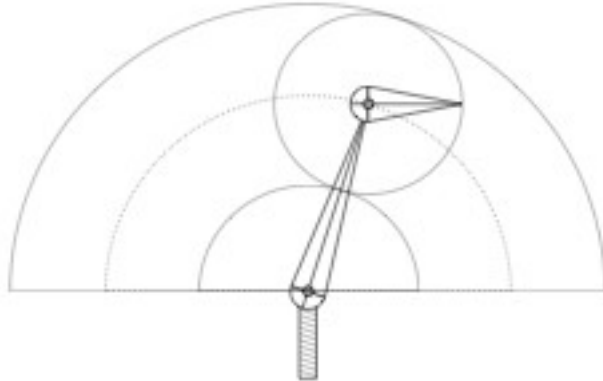
Inverse Kinematics

- Direct IK: solve for the parameters



Inverse Kinematics

- Why is the problem hard?
 - Solutions may not always exist

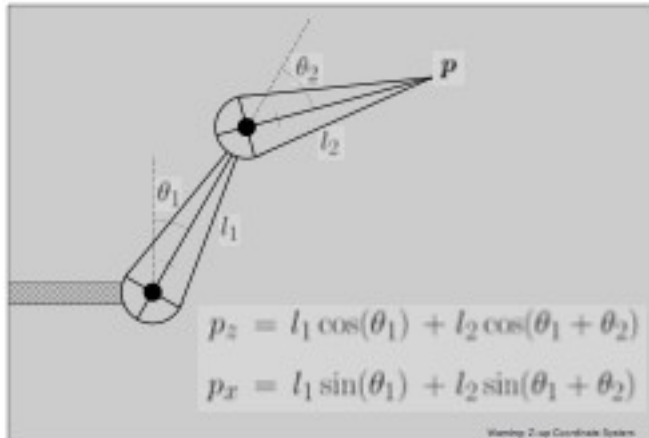


Inverse Kinematics

- Numerical Solution
 - Start in some initial configuration
 - Define an error metric (e.g. goal pos - current pos)
 - Compute Jacobian of error wrt. inputs
 - Apply Newton's method (or other procedure)
 - Iterate...

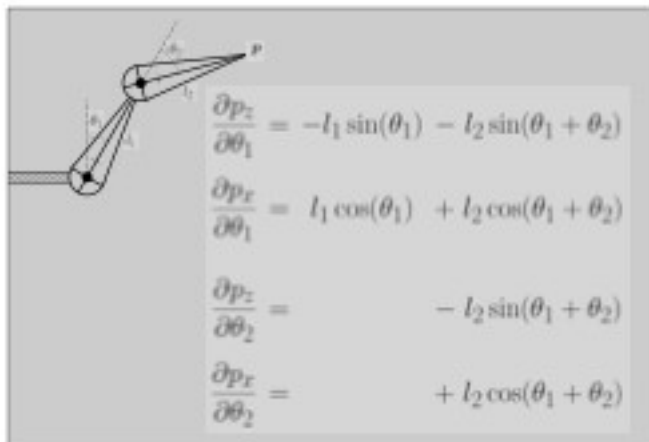
Inverse Kinematics

- Recall simple two segment arm:

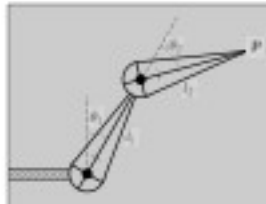


Inverse Kinematics

- We can write of the derivatives



Inverse Kinematics



Direction in Config. Space

$$\theta_1 = c_1 \theta_*$$
$$\theta_2 = c_2 \theta_*$$
$$\frac{\partial p_z}{\partial \theta_*} = c_1 \frac{\partial p_z}{\partial \theta_1} + c_2 \frac{\partial p_z}{\partial \theta_2}$$

22

Inverse Kinematics

The Jacobian (of p w.r.t. θ)

$$J_{ij} = \frac{\partial p_i}{\partial \theta_j}$$

Example for two segment arm

$$J = \begin{bmatrix} \frac{\partial p_z}{\partial \theta_1} & \frac{\partial p_z}{\partial \theta_2} \\ \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} \end{bmatrix}$$

23

Inverse Kinematics

The Jacobian (of p w.r.t. θ)

$$J = \begin{bmatrix} \frac{\partial p_z}{\partial \theta_1} & \frac{\partial p_z}{\partial \theta_2} \\ \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} \end{bmatrix}$$

$$\frac{\partial \mathbf{p}}{\partial \theta_*} = J \cdot \begin{bmatrix} \frac{\partial \theta_1}{\partial \theta_*} \\ \frac{\partial \theta_2}{\partial \theta_*} \end{bmatrix} = J \cdot \begin{bmatrix} c_1 \\ c_2 \end{bmatrix}$$

27

Inverse Kinematics

Solving for c_1 and c_2

$$\mathbf{c} = \begin{bmatrix} c_1 \\ c_2 \end{bmatrix} \quad d\mathbf{p} = \begin{bmatrix} dp_z \\ dp_x \end{bmatrix}$$

$$d\mathbf{p} = J \cdot \mathbf{c}$$

$$\mathbf{c} = J^{-1} \cdot d\mathbf{p}$$

28

Inverse Kinematics

Solving for c_1 and c_2

θ_1 , θ_2 , l_1 , l_2 , p , $e = dp$, g

$$dp = J \cdot c$$
$$c = J^{-1} \cdot dp$$

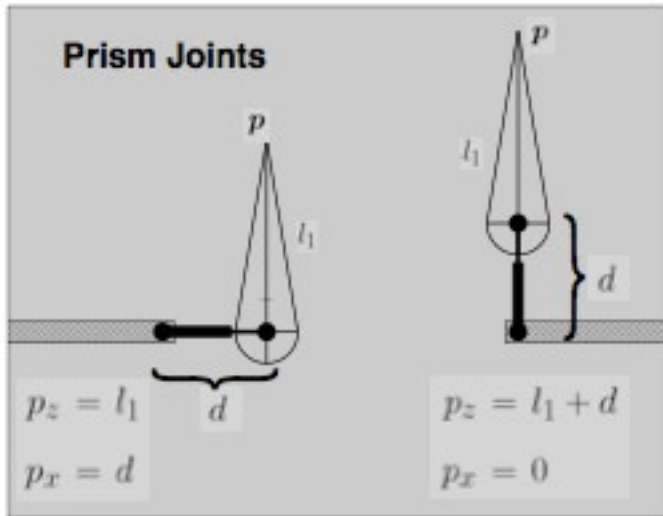
Is the Jacobian invertible?

Inverse Kinematics

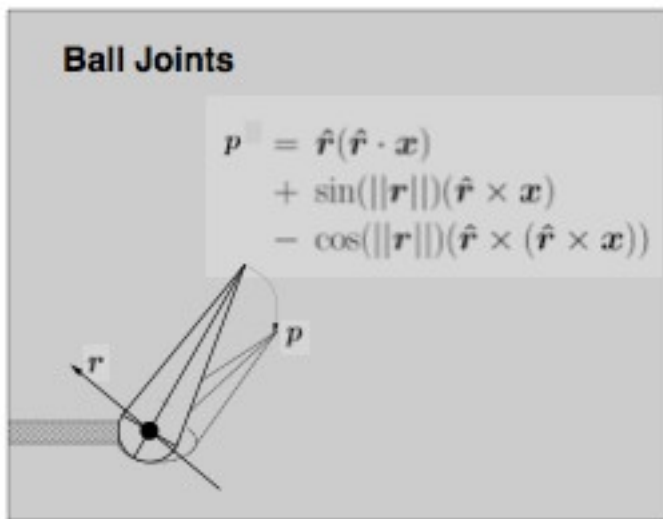
- Problems
 - Jacobian may (will) not always be invertible
 - Use pseudo inverse (SVD)
 - Robust iterative method
 - Jacobian is not constant

- Nonlinear $J = \begin{bmatrix} \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} \\ \frac{\partial p_y}{\partial \theta_1} & \frac{\partial p_y}{\partial \theta_2} \end{bmatrix} = J(\theta)$ (usually) well behaved

Inverse Kinematics



Inverse Kinematics



Inverse Kinematics

Ball Joints (moving axis)

$$d\mathbf{p} = [d\mathbf{r}] \cdot e^{[\mathbf{r}]} \cdot \mathbf{x} = [d\mathbf{r}] \cdot \mathbf{p} = -[\mathbf{p}] \cdot d\mathbf{r}$$

That is the Jacobian for this joint

$$[\mathbf{r}] = \begin{bmatrix} 0 & -r_3 & r_2 \\ r_3 & 0 & -r_1 \\ -r_2 & r_1 & 0 \end{bmatrix}$$

$$[\mathbf{r}] \cdot \mathbf{x} = \mathbf{r} \times \mathbf{x}$$

53

Inverse Kinematics

Ball Joints (fixed axis)

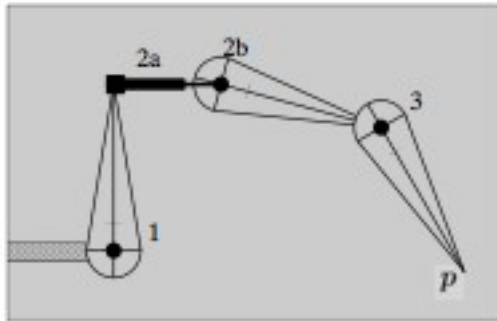
$$d\mathbf{p} = (d\theta)[\hat{\mathbf{r}}] \cdot \mathbf{x} = -[\mathbf{x}] \cdot \hat{\mathbf{r}} d\theta$$

That is the Jacobian for this joint

54

Inverse Kinematics

- Many links / joints
 - Need a generic method for building Jacobian



6

Inverse Kinematics

- Can't just concatenate individual matrices

The same diagram of the 3-link robotic arm is shown. Above it, the Jacobian matrix is given as $\tilde{J} = [J_3 J_{2b} J_{2a} J_{1b}]$, with a red 'X' over the entire expression. To the right, the vector d is defined as $d = \begin{bmatrix} d_3 \\ d_{2b} \\ d_{2a} \\ d_{1b} \end{bmatrix}$. Below the diagram, a red box contains the equation $dp \neq \tilde{J} \cdot dd$.

6

Inverse Kinematics

Transformation from body to world

$$X_{0 \leftarrow i} = \prod_{j=1}^i X_{(j-1) \leftarrow j} = X_{0 \leftarrow 1} \cdot X_{1 \leftarrow 2} \cdots$$

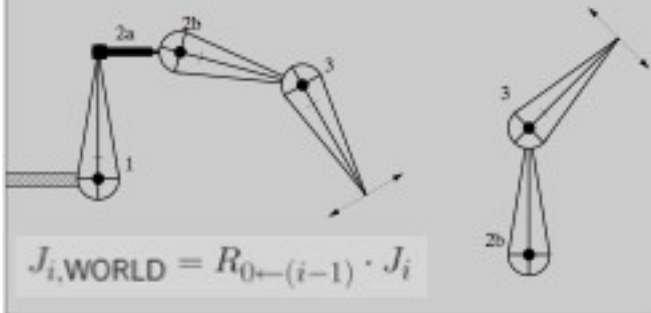
Rotation from body to world

$$R_{0 \leftarrow i} = \prod_{j=1}^i R_{(j-1) \leftarrow j} = R_{0 \leftarrow 1} \cdot R_{1 \leftarrow 2} \cdots$$

4

Inverse Kinematics

Need to transform Jacobians to common coordinate system (WORLD)



4

Inverse Kinematics

$$J = \begin{bmatrix} R_{0 \leftarrow 2b} \cdot J_3(\theta_3, \mathbf{p}_3) \\ R_{0 \leftarrow 2a} \cdot J_{2b}(\theta_{2b}, X_{2b \leftarrow 3} \cdot \mathbf{p}_3) \\ R_{0 \leftarrow 1} \cdot J_{2a}(\theta_{2a}, X_{2a \leftarrow 3} \cdot \mathbf{p}_3) \\ J_1(\theta_1, X_{1 \leftarrow 3} \cdot \mathbf{p}_3) \end{bmatrix}^T$$
$$\mathbf{d} = \begin{bmatrix} d_3 \\ d_{2b} \\ d_{2a} \\ d_{1b} \end{bmatrix}$$

Note: Each row in the above should be transposed...

$$d\mathbf{p} = J \cdot d\mathbf{d}$$

A Cheap Alternative

- Estimate Jacobian (or parts of it) using finite differences
- Cyclic Coordinate Descent
 - Solve for each DOF one at a time
 - Iterate till good enough / run out of time

Inverse Kinematics

- More complex systems
 - More complex joints (prism and ball)
 - More links
 - Other criteria (COM or height)
 - Hard constraints (eg foot plants)
 - Unilateral constraints (eg joint limits)
 - Multiple criteria and multiple chains
- Smoothness over time
 - DOF are determined by control points of a curve (chain rule)

21

Inverse Kinematics

- Some issues
 - How to pick from multiple solutions?
 - Robustness when no solutions
 - Contradictory solutions
 - Smooth interpolation
 - Interpolation aware of constraints

22

