

Lecture 8: Limiting, Finite R, and Slew Rate

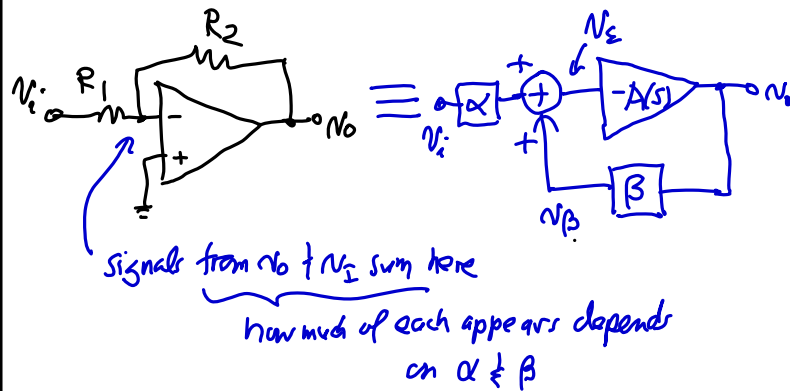
- Announcements:
- HW#3 online and due Friday via Gradescope
- Lab#2 will be a two week lab
 - ↳ Prelab is due in the second week
 - ↳ But you should have proof of having started it when you go to lab this week
 - ↳ You will still do the lab this week and continue next week
- This Wednesday, 9/12: I will be out of town.
 - ↳ So no ground lecture that day
 - ↳ Make up will probably need to be by video recording and put online

 • **Lecture Topics:**

- ↳ Limiting
 - ↳ Finite Input & Output Resistance
 - ↳ Slew Rate
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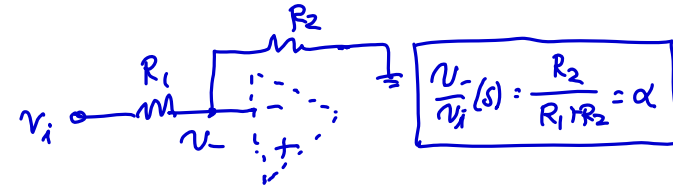
• **Last Time:** Finite gain-BW op amp circuits

Example. Inverting Amplifier



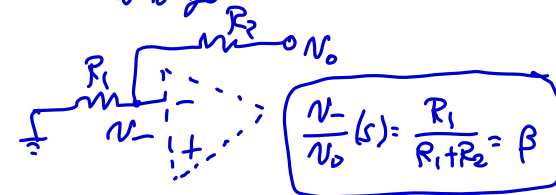
Determine α :

- ① Ground output & open loop
- ② Feed v_i forward to get T.F.



Determine β :

- ① Ground input, open loop
- ② Feedback v_o to get T.F.



Now, get the T.F. for the system block diagram:

$$\left. \begin{aligned} v_o &= -A(s)v_\Sigma \\ v_\Sigma &= \alpha v_i + \beta v_o \end{aligned} \right\} \begin{aligned} v_o &= -\alpha A(s)v_i - \beta A(s)v_o \\ v_o(1 + \beta A(s)) &= -\alpha A(s)v_i \end{aligned}$$

$$\therefore \frac{v_o}{v_i}(s) = -\frac{\alpha A(s)}{1 + \beta A(s)}$$

$$\left[A(s) = \frac{A_o}{1 + \frac{s}{\omega_b}} \right] \Rightarrow \frac{v_o}{v_i}(s) = \frac{-\alpha \frac{A_o}{1 + \frac{s}{\omega_b}}}{1 + \frac{\beta A_o}{1 + \frac{s}{\omega_b}}}$$

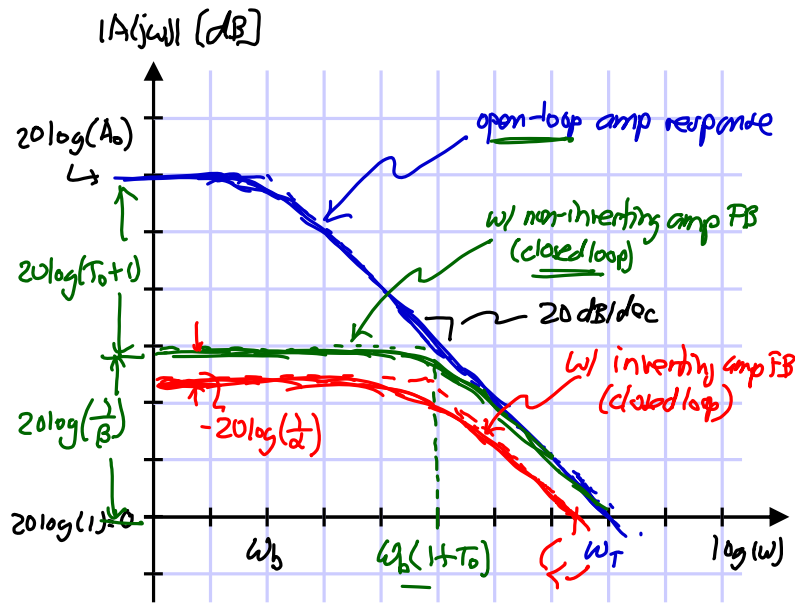
$$\frac{V_o}{V_i}(s) = \frac{-\alpha A_o}{1 + \beta A_o} \frac{1}{1 + \frac{s}{\omega_b(1 + \beta A_o)}}$$

Remarks.

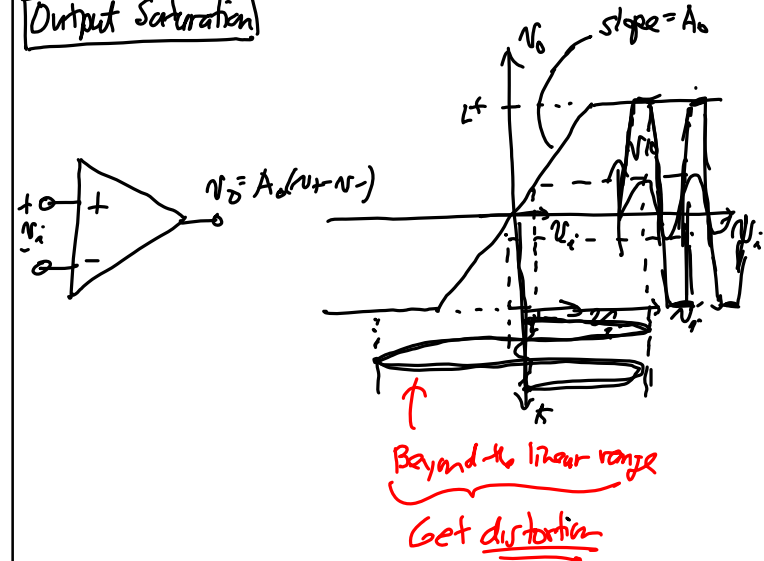
- ① Closed loop DC gain now modified by α .
- ② BW still $\omega_b(1 + \beta A_o)$ → same as for non-inverting case
- ③ ω_T or Gain-BW product now smaller than that of open-loop amplifier:

$$\text{gain-BW} = \alpha \omega_T$$

↑
[remember, $\alpha < 1$]

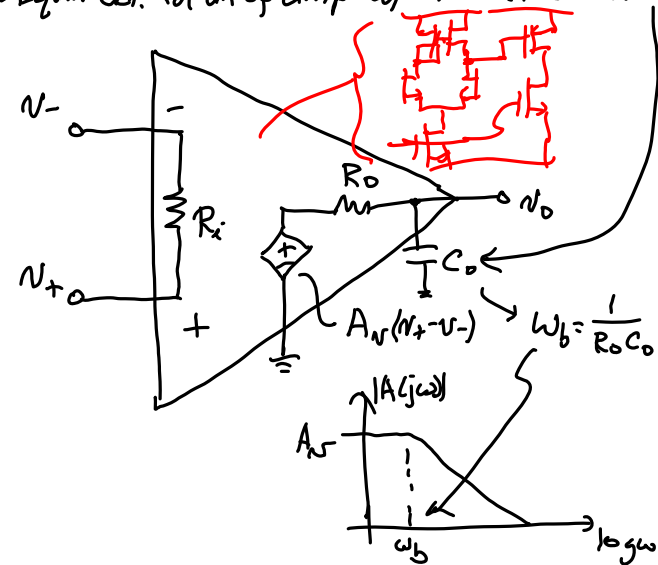


Output Saturation



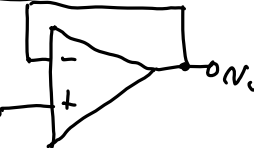
Finite Input & Output Resistances

⇒ Equiv. ckt. for an op-amp w/ finite $R_i, R_o, A_o, \beta, \omega_b$



Slew Rate

Unity Gain Follower -

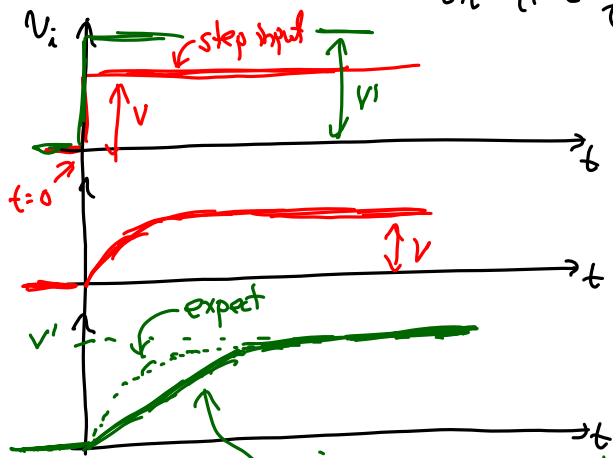


$$\frac{V_o}{V_i}(s) = \frac{1}{1 + \frac{s}{\omega_T}}$$

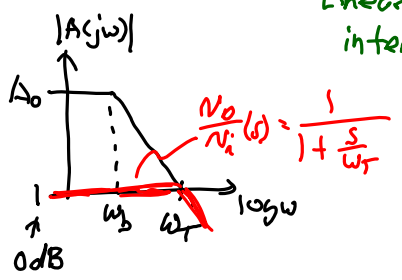
Step Response: *assume $V_o = 0V$*

$$V_o(t) = V_o|_{t=0^-} (V_o|_{t=0^+} - V_o|_{t=0^-}) e^{-t/\tau}$$

$$= V_o|_{t=0^+} (1 - e^{-t/\tau})$$

$$\tau = \frac{1}{\omega_T}$$


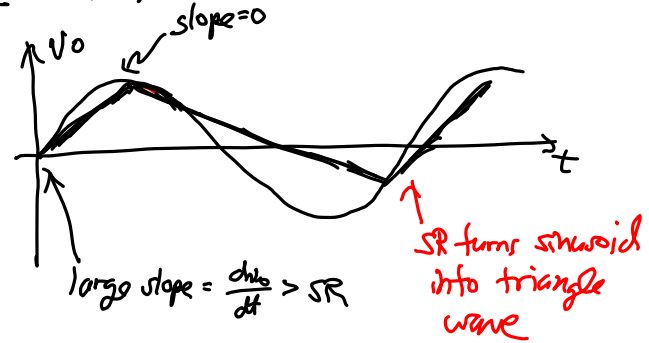
Linear increase caused by internal limitation that limit the output current of the op amp.



$$\frac{V_o}{V_i}(w) = \frac{1}{1 + \frac{jw}{\omega_T}}$$

max. rate of change of output voltage } \approx Slew Rate = SR = $\left. \frac{dV_o}{dt} \right|_{\max}$ [V/ μ s]

Example. Outputting a sinusoid (or at least try to...)



Full Power Bandwidth $\Rightarrow f_M$

- Suppose you wanted your op amp circuit to output a signal with a maximum amplitude V_{omax}
- Then the full power bandwidth is the maximum frequency of this V_{omax} amplitude that the op amp can track without slewing

$$V_o = V_{omax} \sin \omega t$$

$$\frac{dV_o}{dt} = \omega V_{omax} \cos \omega t$$

$$= \left. \frac{dV_o}{dt} \right|_{\max} \text{ of the max. expected signal}$$

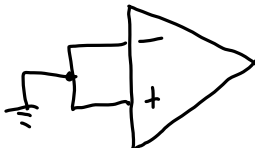
this must equal SR for sufficient tracking:

$$\omega_M V_{omax} = SR$$

$$\therefore f_M = \frac{SR}{2\pi V_{omax}}$$

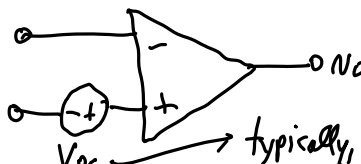
Full Power Bandwidth

Input Offset Voltage, V_{os}



$v_o = A(v_+ - v_-)$
Ideal Case: $v_o = 0V$
Reality: $v_o \neq 0V$
(usually, $v_o = L^+$ or L^- ;
it rails out)

Model this w/ equivalent
input offset voltage, V_{os} :



typically, $V_{os} \sim 1mV - 5mV$

Effect of V_{os} on Op Amp Ckt. -