(Saturated) MOSFET Small-Signal Model

■ Concept: find an equivalent circuit which interrelates the *incremental* changes in i_D , v_{GS} , v_{DS} , etc. for the MOSFET in saturation

$$v_{GS} = V_{GS} + v_{gs}$$
, $i_D = I_D + i_d$ -- we want to find $i_d = (?) v_{gs}$

We have the functional dependence of the total drain current in saturation:

$$i_D = \mu_n C_{ox} (W/2L) (v_{GS} - V_{Tn})^2 (1 + \lambda_n v_{DS}) = i_D (v_{GS}, v_{DS})$$

Solution: do a Taylor expansion around the DC operating point (also called the quiescent point or Q point) defined by the DC voltages $Q(V_{GS}, V_{DS})$:

$$i_D = I_D + \frac{\partial i_D}{\partial v_{GS}} \bigg|_Q (v_{gs}) + \frac{1}{2} \frac{\partial^2 i_D}{\partial v_{GS}^2} \bigg|_Q (v_{gs})^2 + \dots$$

If the small-signal voltage is really "small," then we can neglect all everything past the linear term --

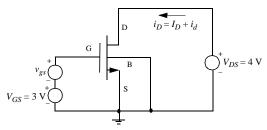
$$i_D = I_D + \frac{\partial i_D}{\partial v_{GS}} \bigg|_Q (v_{gs}) = I_D + g_m v_{gs}$$

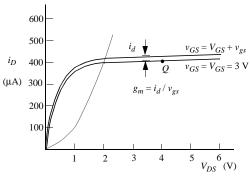
where the partial derivative is defined as the transconductance, g_m .

Transconductance

The small-signal drain current due to $v_{\rm gs}$ is therefore given by

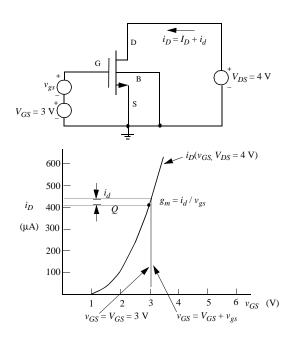
$$i_d = g_m v_{gs}$$





Another View of g_m

* Plot the drain current as a function of the gate-source voltage, so that the slope can be identified with the transconductance:



Transconductance (cont.)

■ Evaluating the partial derivative:

$$g_m = \mu_n C_{ox} \left(\frac{W}{L} \right) (V_{GS} - V_{Tn}) (1 + \lambda_n V_{DS})$$

■ In order to find a simple expression that highlights the dependence of g_m on the DC drain current, we neglect the (usually) small error in writing:

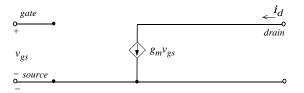
$$g_m = \sqrt{2\mu_n C_{ox} \left(\frac{W}{L}\right) I_D} = \frac{2I_D}{V_{GS} - V_{Tn}}$$

For typical values (W/L) = 10, $I_D = 100 \,\mu\text{A}$, and $\mu_n C_{ox} = 50 \,\mu\text{AV}^{-2}$ we find that

$$g_m = 320 \,\mu\text{AV}^{-1} = 0.32 \,\text{mS}$$

(Partial) Small-Signal Circuit Model

■ How do we make a circuit which expresses $i_d = g_m v_{gs}$? Since the current is not across its "controlling" voltage, we need a voltage-controlled current source:



Output Conductance/Resistance

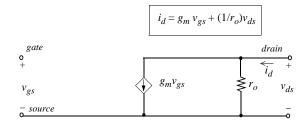
We can also find the change in drain current due to an increment in the drainsource voltage:

$$g_o = \frac{\partial i_D}{\partial v_{DS}} \bigg|_Q = \mu_n C_{ox} \left(\frac{W}{2L}\right) (V_{GS} - V_{Tn})^2 \lambda_n \cong \lambda_n I_D$$

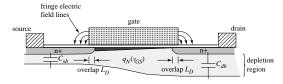
The output resistance is the inverse of the output conductance

$$r_o = \frac{1}{g_o} = \frac{1}{\lambda_n I_D}$$

The (partial) small-signal circuit model with r_o added looks like:



MOSFET Capacitances in Saturation



In saturation, the gate-source capacitance contains two terms, one due to the channel charge's dependence on v_{GS} [(2/3) WLC_{ox}] and one due to the overlap of gate and source (WC_{oy} , where C_{oy} is the *overlap capacitance* in fF per μ m of gate width)

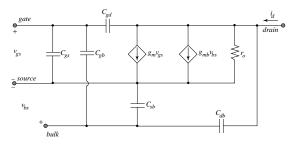
$$C_{gs} = \frac{2}{3}WLC_{ox} + WC_{ov}$$

In addition, there is the small but very important gate-drain capacitance (just the overlap capacitance $C_{gd}=C_{ov}$)

There are depletion capacitances between the drain and bulk (C_{db}) and between source and bulk (C_{sb}) . Finally, the extension of the gate over the field oxide leads to a small gate-bulk capacitance C_{eb} .

Complete Small-Signal Model

■ All these capacitances are "patched" onto the small-signal circuit schematic containing g_m and r_o ... g_{mb} is open-circuited for EECS 105 since $v_{bs} = 0$ V.

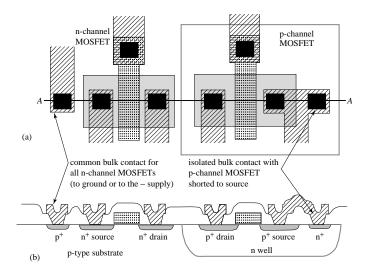


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p-channel MOSFETs

- Structure is *complementary* to the n-channel MOSFET
- In a CMOS technology, one or the other type of MOSFET is built into a *well* -- a deep diffused region -- so that there are electrically isolated "bulk" regions in the same substrate



p-channel MOSFET Models

■ DC drain current in the three operating regions: $-I_D > 0$

$$\begin{split} -I_D &= 0 \text{ A} \\ -I_D &= \mu_p C_{ox} (W/L) [V_{SG} + V_{Tp} - (V_{SD}/2)] (1 + \lambda_p V_{SD}) V_{SD} \\ -I_D &= \mu_p C_{ox} (W/L) [V_{SG} + V_{Tp} - (V_{SD}/2)] (1 + \lambda_p V_{SD}) V_{SD} \\ (V_{SG} \geq -V_{Tp}, V_{SD} \leq V_{SG} + V_{Tp}) \\ -I_D &= \mu_p C_{ox} (W/(2L)) (V_{SG} + V_{Tp})^2 (1 + \lambda_p V_{SD}) \\ (V_{SG} \geq -V_{Tp}, V_{SD} \geq V_{SG} + V_{Tp}) \end{split}$$

■ The threshold voltage with backgate effect is given by:

$$V_{Tp} = V_{TOp} - \gamma_p ((\sqrt{-V_{SB} + 2\phi_n}) - \sqrt{2\phi_n})$$

Numerical values:

 $\mu_p C_{ox}$ is a measured parameter. Typical value: $\mu_p C_{ox} = 25 \ \mu AV^{-2}$

$$\lambda_p \approx \frac{0.1 \, \mu \, \text{mV}^{-1}}{L}$$

 V_{Tp} = -0.7 to -1.0 V, which should be approximately - V_{Tn} for a well-controlled CMOS process

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p-channel MOSFET small-signal model

■ the source is the highest potential and is located at the top of the schematic

