Lecture 31

- Last time:
 - Short-circuit current gain of CE and CS amps
 - Unity-gain frequency ω_T
- Today :
 - Frequency response of the CE as voltage amp
 - The Miller approximation

Common-Emitter Voltage Amplifier



Small-signal model: omit C_{cs} due to avoid complicated analysis

CE Voltage Amp Small-Signal Model



Frequency Response

KCL at input and output nodes; analysis is made complicated due to Z_{μ} branch \rightarrow see H&S pp. 639-640.

$$\frac{V_{out}}{V_{in}} = \frac{-g_m \left(\frac{r_{\pi}}{r_{\pi} + R_s}\right) r_o \|r_{oc}\| R_L \left(1 - j\omega / \omega_z\right)}{\left(1 + j\omega / \omega_{p1}\right) \left(1 + j\omega / \omega_{p2}\right)}$$

Low-frequency gain:

Zero:
$$\omega_z > \omega_T = \frac{g_m}{C_\pi + C_\mu}$$



Decoupling Input and Output: the Miller Approximation

Results of complete analysis: not exact and little insight Look at how Z_{μ} affects the transfer function: find Z_{in}



Input Impedance $Z_{in}(j\omega)$

$$I_t = (V_t - V_{out}) / Z_\mu$$

At output node:

$$V_{out} = (-g_m V_t - I_t) R'_{out} \approx -g_m V_t R'_{out}$$
 Why?

 $I_{t} = (V_{t} - A_{vC_{\mu}}V_{t}) / Z_{\mu}$

$$Z_{in} = V_t / I_t = \frac{Z_{\mu}}{1 - A_{vC_{\mu}}}$$

Miller Capacitance C_M

Effective input capacitance:

$$Z_{in} = \frac{1}{j\omega C_{M}} = \left(\frac{1}{1 - A_{vC_{\mu}}}\right) \left(\frac{1}{j\omega C_{\mu}}\right) = \frac{1}{j\omega [(1 - A_{vC_{\mu}})C_{\mu}]}$$



What about the role of C_x when viewed from the output port?

Some Examples

Common emitter/source amplifier:

$$A_{vC_{\mu}}$$
 = Negative, large number (-100)

Common collector/drain amplifier:

$$A_{vC_{\pi}}$$
 = Slightly less than 1

CE Amplifier using Miller Approx.

Use Miller to transform C_{μ}



Analysis is straightforward now ... single pole!

Comparison with "Exact Analysis"

Miller result:

$$\omega_{p1}^{-1} =$$

Exact result:

$$\omega_{p1}^{-1} = (R_S \parallel r_\pi) \{ C_\pi + (1 + g_m R'_{out}) C_\mu \} + R'_{out} C_\mu$$