

Lecture 27

- Last time:
 - ✓ Current-source supplies
 - ✗ Common-gate amplifier

Ai

- Today :

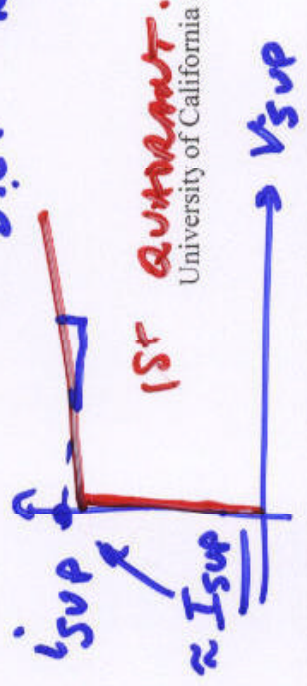
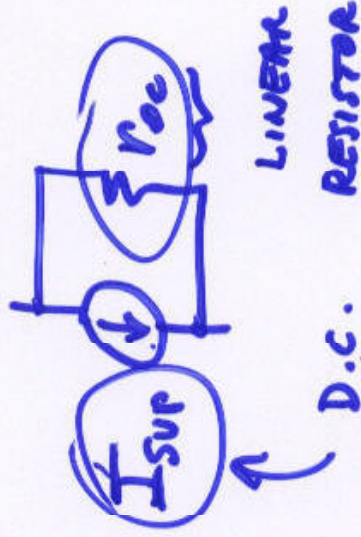
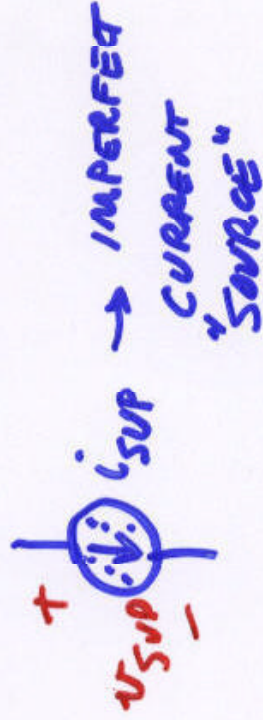
- Finish common-gate
- Common-drain amplifier

• LARGE r_{oc}

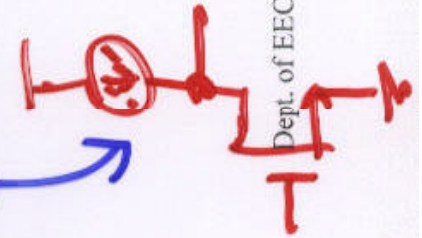
• LARGE

$I_{SUP} \Rightarrow I_{D}$

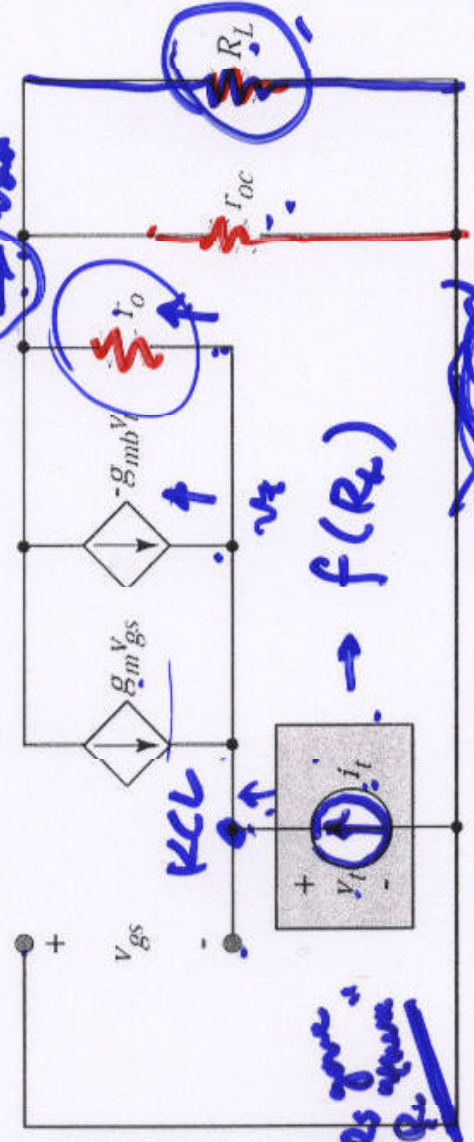
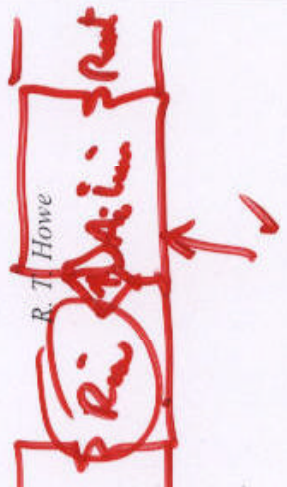
$I_D \Rightarrow g_m$



ABSTRACT



CG Input Resistance



$R_{in} = \frac{v_t}{i_t} \Big|_{R_s = 0}$
 $R_s = 0$
 R_L left on.

At input:

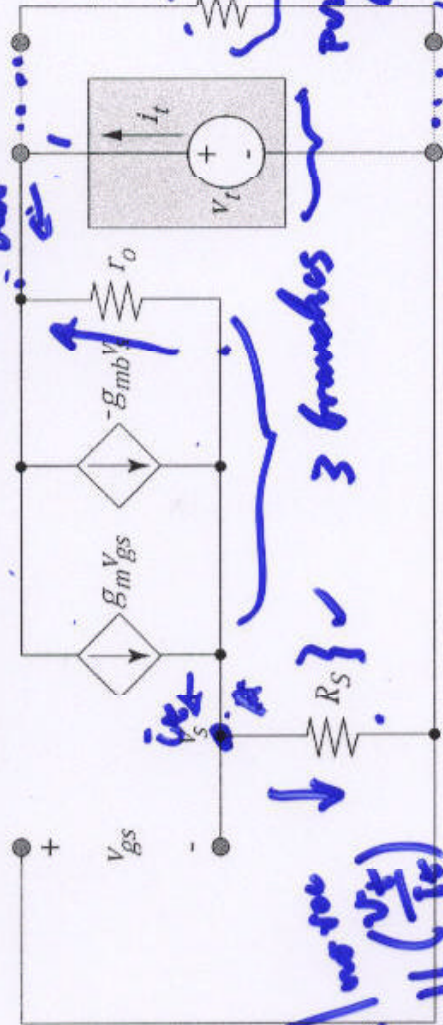
$i_t = -g_m v_{gs} + g_{mb} v_t + \frac{v_t - v_{out}}{r_o}$

Output voltage: $-i_{out} (r_{oc} \parallel R_L) = -(-i_t)(r_{oc} \parallel R_L)$



$I_{out} = -I_{in}$

CG Output Resistance



$$i_t = (g_m + g_{mb}) v_t$$

$$0.5 \text{ mA} = \frac{1}{20 \text{ k}\Omega} v_t$$

$$g_{mb} = 0.1 \text{ gm}$$

$$r_o = 250 \text{ k}\Omega$$

$$v_t = R_{in} i_t$$

$$R_{in} = \frac{1}{g_m + g_{mb}}$$

①

* Kirchoff's current law at the source resistor node: sum currents leaving node

$$\frac{v_s}{R_S} - g_m v_{gs} - (-g_{mb} v_s) + \frac{v_s - v_t}{r_o} = 0$$

A

$$v_s \left(\frac{1}{R_S} + g_m + g_{mb} + \frac{1}{r_o} \right) = \frac{v_t}{r_o}$$

$i_t R_S$

"SMALL"

Common-Gate Output Resistance r_{oc}

Substituting $v_s = i_t R_S$

"A PAIN"

$$i_t R_S \left(\frac{1}{R_S} + g_m + g_{mb} + \frac{1}{r_o} \right) = \frac{v_t}{r_o}$$

The output resistance is $(v_t / i_t) \parallel r_{oc}$

SIMPLIFY

$$R_{out} = r_{oc} \parallel \left(R_S \left[\frac{r_o}{R_S} + g_m r_o + g_{mb} r_o + 1 \right] \right)$$

HUGE!
= BIG!

BIG

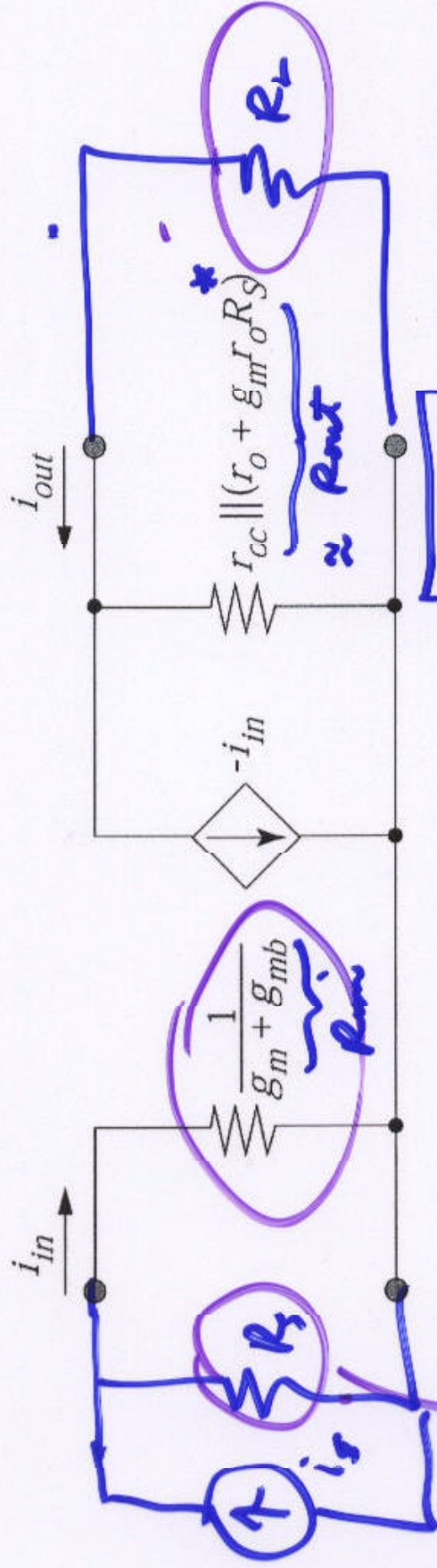
$$\frac{v_t}{i_t}$$

$$B_{10} = r_{oc} \parallel (\text{mess})$$

$$\left(\frac{1}{2 \mu S} \cdot 200 \mu r_o \right) \approx 100.$$

WE ARE FINISHED!

Common-Gate Two-Port Model



Function: a current buffer

$$\frac{i_{out}}{i_s} = \left[\frac{R_S}{R_S + \frac{1}{g_m + g_{mb}}} \right] (-1) \left[\frac{r_{o1} \parallel (r_o \parallel (1 + g_m r_o))}{r_{o1} + r_{o2} \parallel (r_o \parallel (1 + g_m r_o))} \right]$$

Post R_S small R_S
OPEN & LOAD
SMALL
1.

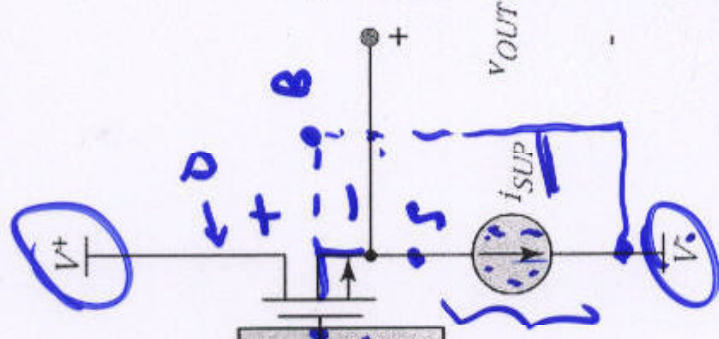
$I_D = \mu_n C_{ox} (W/L) (V_{GS} - V_{TH})^2$ (circled in red)

Common-Drain Amplifier

CS
CG

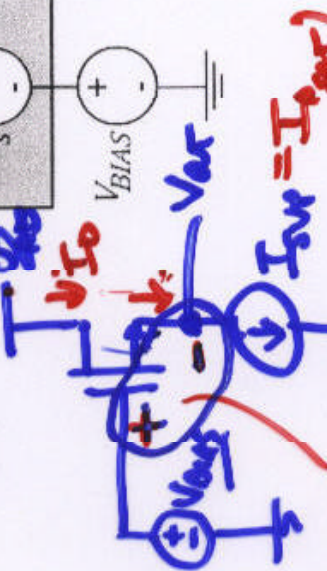
$\frac{dV_{out}}{dV_{in}} = 1$

Backgate terminal



D.C. BIAS.

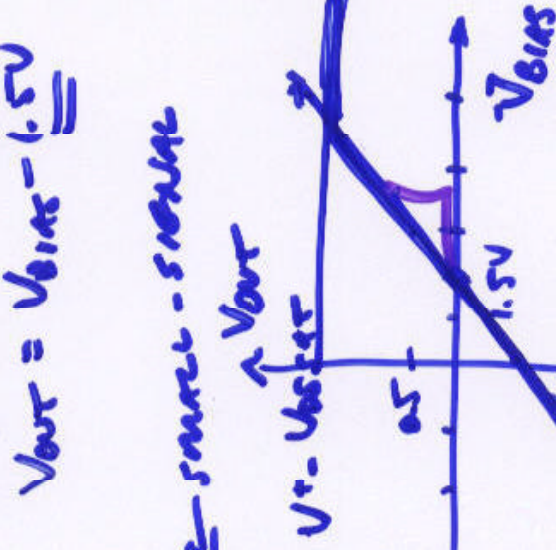
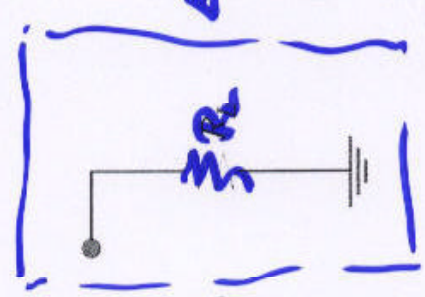
$V_{out} = V_{BIAS} - I_{out} R_S$



$V_{GS} = V_{BIAS} - V_{out}$
LET'S NAME V_{BIAS} .

$V_{out} \approx 0V$

↑ EASY!



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2.5V, 0.5V, 0.1V

$V_{GS} = V_{in} + \sqrt{\mu_n C_{ox} (W/L)}$

→ Approximating the CG R_{out}

$$R_{out} = r_{oc} \parallel [r_o + g_m r_o R_S + g_{mb} r_o R_S + R_S]$$

0.1 gm ro RS

The exact result is complicated, so let's try to make it simpler: 24R

$$g_m \approx 500 \mu S \quad g_{mb} \approx 50 \mu S \quad r_o \approx 200 k\Omega$$

$$R_{out} \approx r_{oc} \parallel [r_o + g_m r_o R_S + R_S] \quad \text{PRETTY GOOD}$$

Assuming the source resistance is less than r_o ,

$$R_{out} \approx r_{oc} \parallel [r_o + g_m r_o R_S] = r_{oc} \parallel [r_o (1 + g_m R_S)]^*$$

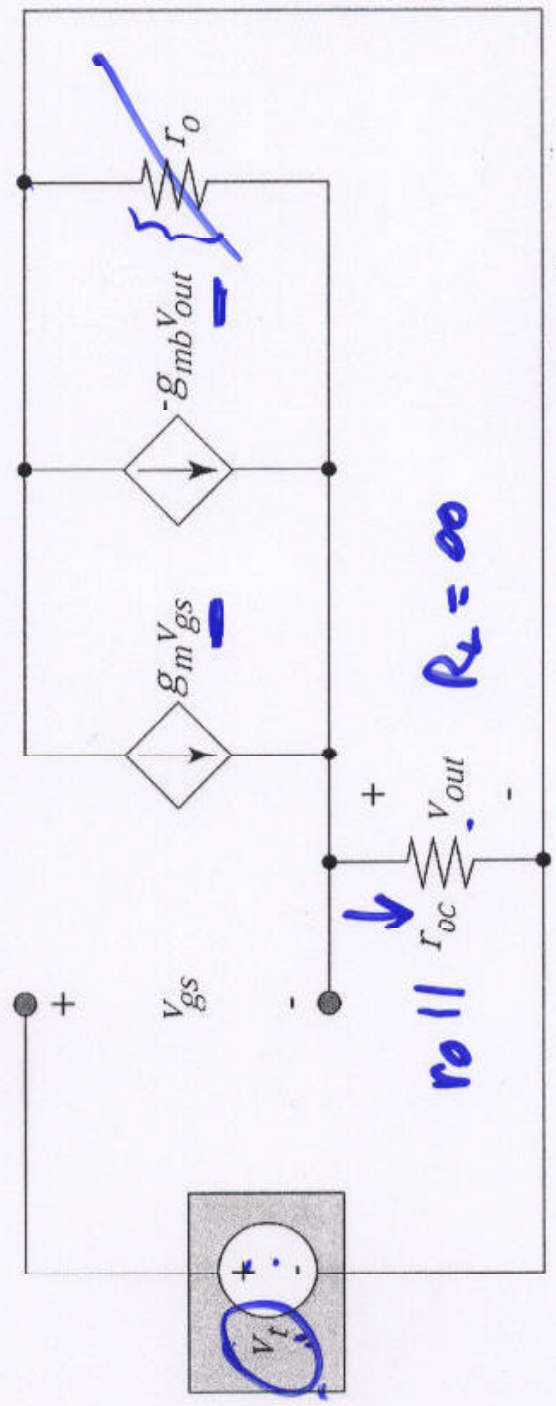
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$$r_{oc} \parallel r_o (1 + 25)$$

$$R_S \ll r_o$$

CD Voltage Gain



$r_{oc} \parallel R_L = \infty$

$$A_v = \frac{v_{out}}{v_{in}} \Big|_{R_s=0, R_L=\infty}$$

Note $v_{gs} = v_t - v_{out}$

$$\frac{v_{out}}{v_{in}} = g_m v_{gs} - g_m v_{out}$$

$$= g_m (v_t - v_{out}) - g_m v_{out}$$

CD Voltage Gain (Cont.)

KCL at source node:

$$v_{out} \left(\frac{1}{r_{o1||r_{o2}} + g_m v_{out} + g_{m2} v_{out} \right) = g_m v_{in}$$

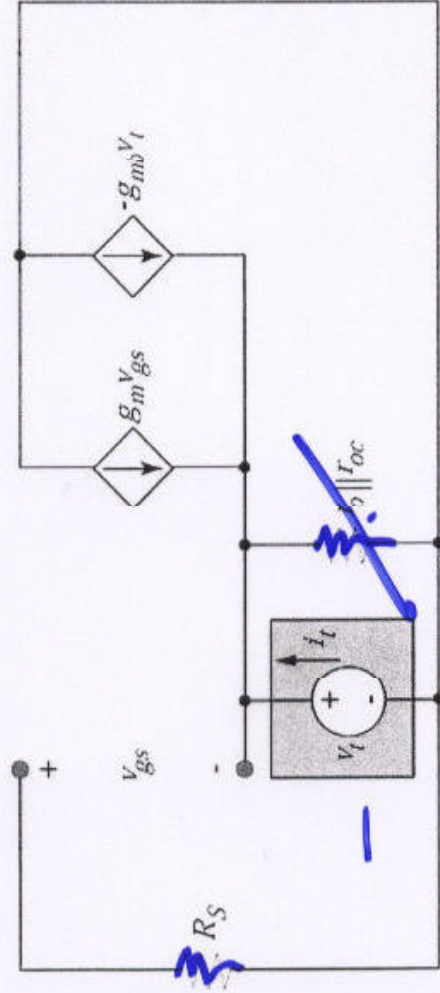
Voltage gain (for v_{SB} not zero):

$$\frac{v_{out}}{v_{in}} \equiv A_v = \frac{g_m}{g_m + g_{m1} + \frac{1}{r_{o1||r_{o2}}}}$$

$$\approx \frac{g_m}{g_m + g_{m1}} \approx 1.$$

CD Output Resistance

$R_{out} = \infty$



Sum currents at output (source) node:

$$R_{out} = (R_S \parallel R_{oc}) \parallel \left\{ \frac{v_t}{i_t} \right\}$$

$$i_t + g_m v_{gs} + -g_m v_t = 0$$

$$i_t = (g_m + g_{mb}) v_t$$

CD Output Resistance (Cont.)

$r_o \parallel r_{oc}$ is much larger than the inverses of the transconductances \rightarrow ignore

$$R_{out} = \cancel{(r_o \parallel r_{oc})} \parallel \left\{ \frac{1}{g_m + g_{mb}} \right\} = \frac{1}{g_m + g_{mb}}$$

