

Lecture 32

CHAPTER 10... f RESPONSE
OF CE, CC, CB.

- Last time:
 - Frequency response of the CE as voltage amp
 - The Miller approximation
- Today : CC CB
 - Frequency response of voltage and current buffers
 - Start multi-stage amplifiers: Chapter 9

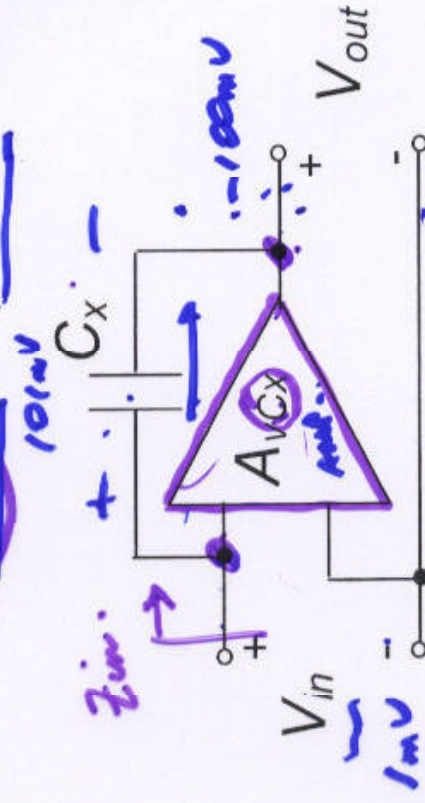
I - SOURCES.

Miller Capacitance C_M

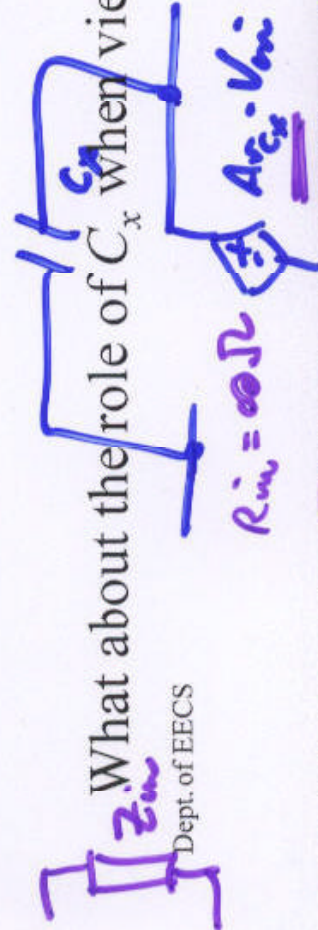
Effective input capacitance: $\leftarrow Z_{in}$

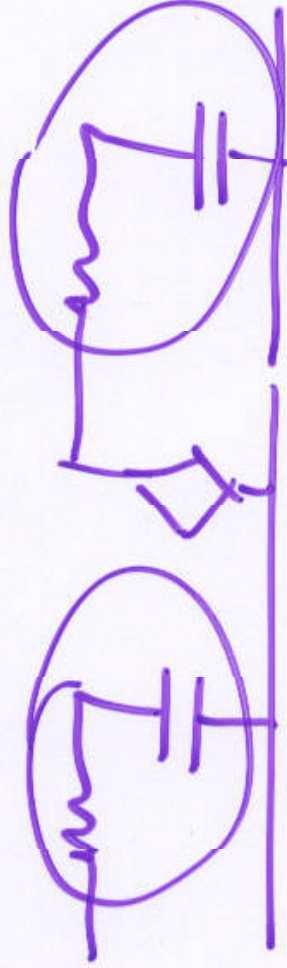
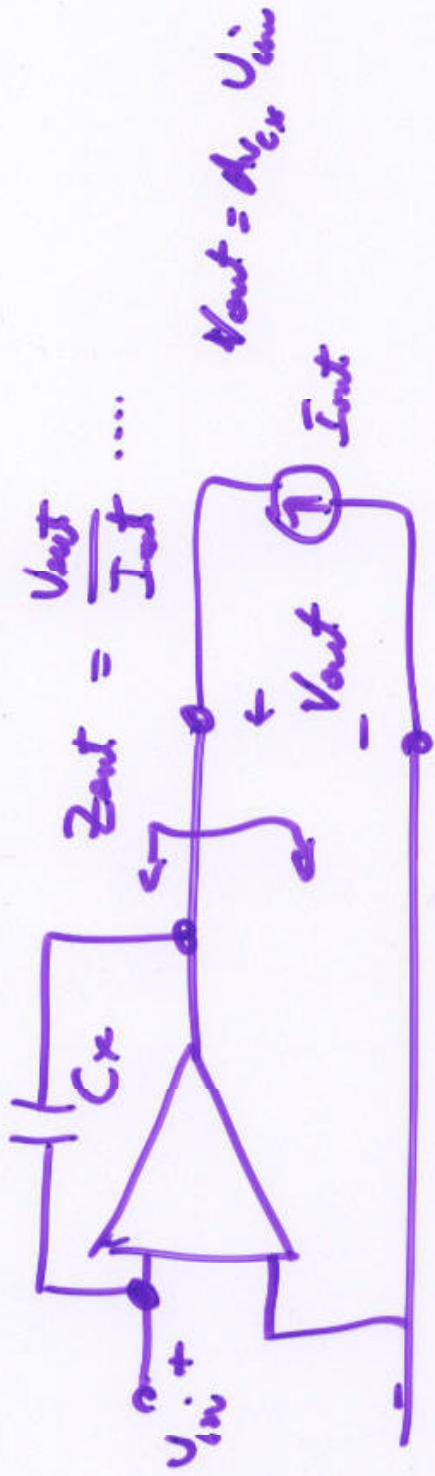
"Z_{in}" $\rightarrow Z_{in} = \frac{1}{j\omega C_M} = \left(\frac{1}{1 - A_{vC_\mu}} \right) \left(\frac{1}{j\omega C_\mu} \right) = \frac{1}{j\omega [(1 - A_{vC_\mu}) C_\mu]}$

$C_M = C_\mu (1 - A_{vC_\mu}) = C_\mu (1 + g_m R_{out}) \approx 100 C_\mu$

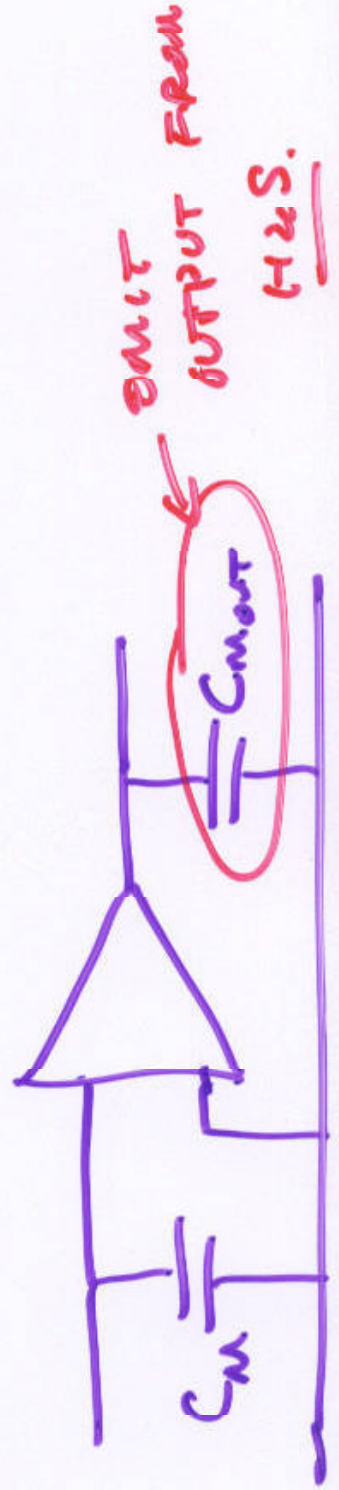


What about the role of C_x when viewed from the output port?





$$C_{n_{out}} = C_x \left(\frac{1}{1 - (1/A_{v_{ex}})} \right) \leftarrow \text{YOU DO THIS...}$$



NONLINEAR!



Some Examples

Common emitter/source amplifier:

DISKSTER!

$A_{vC_{\mu}}$ = Negative, large number (-100)

$$= -g_m (r_{o||r_{oc}||R_c}) \approx -B_{10}$$

$R_s = 0$

$$C_{\mu} = C_{\pi} (1 - [-g_m r_{o||r_{oc}||R_c}]) = 101 C_{\pi}$$

Common collector/drain amplifier:

$A_{vC_{\pi}}$ = Slightly less than 1

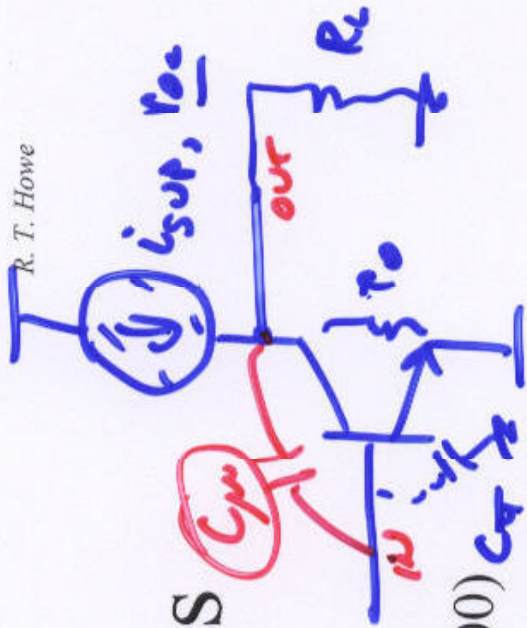
$$\approx 1 - C_{\mu} \omega p$$

"BOOTSTRAPPING"

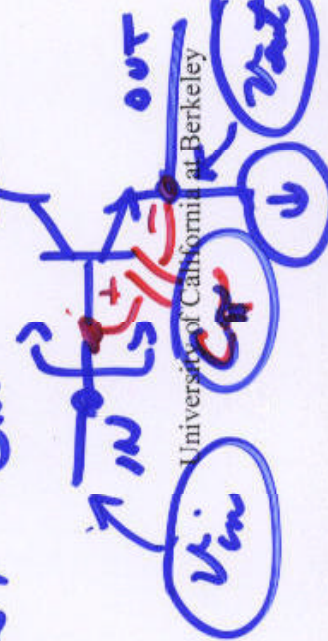
$$= C_{\pi} (1 - A_{vC_{\pi}})$$

$$= C_{\pi} (1 - 1)$$

$$= \phi$$

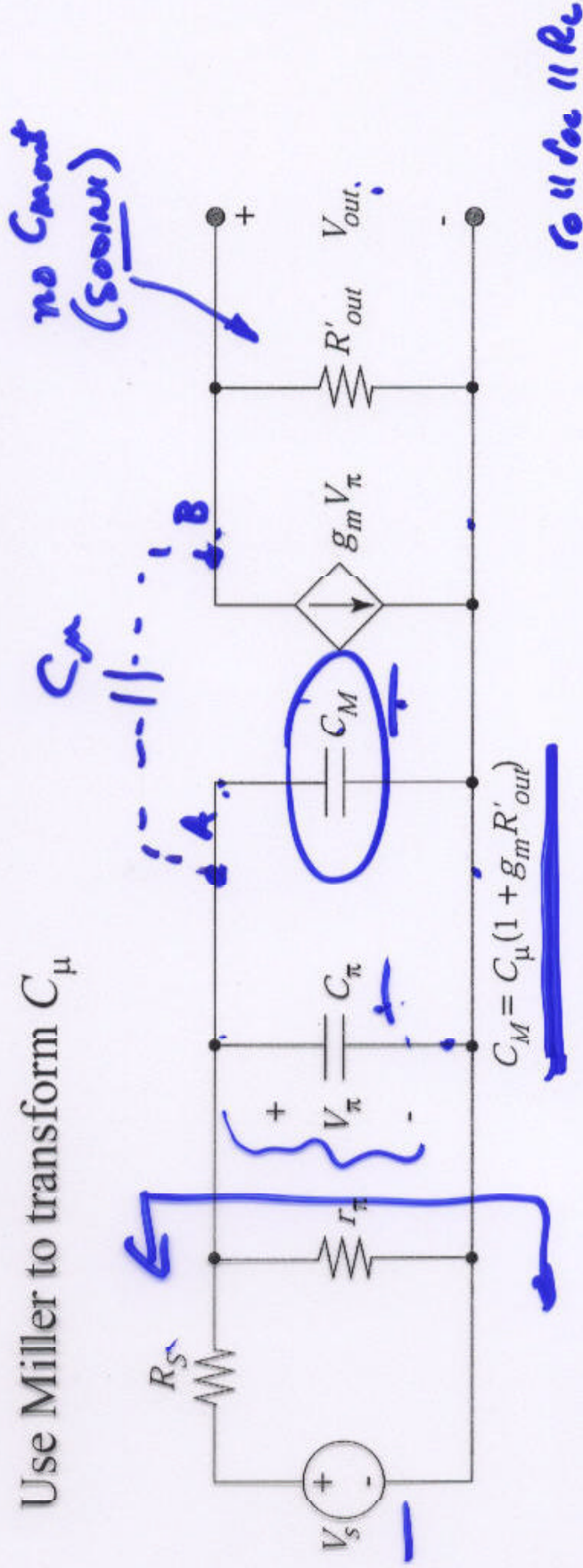


$\gg C_{\pi}$



CE Amplifier using Miller Approx.

Use Miller to transform C_μ



Analysis is straightforward now ... single pole!

$R_T \parallel R_S$



Comparison with “Exact Analysis”

UNDERSTANDING

Miller result:

$$\omega_{p1}^{-1} \approx R_{in} C_{in} = \underbrace{(R_S \parallel r_{\pi})}_{C_{\pi}} + \underbrace{(1 + g_m R_{out})}_{C_{\mu}} C_{in}$$

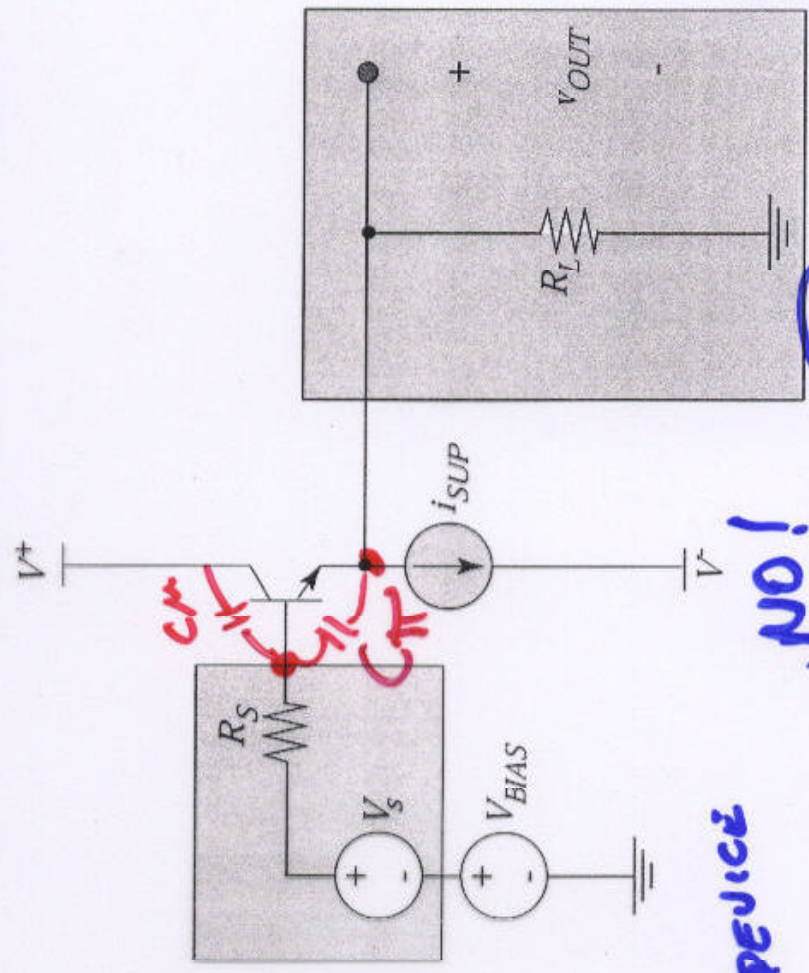
Exact result:

$$\omega_{p1}^{-1} \approx (R_S \parallel r_{\pi}) \{ C_{\pi} + (1 + g_m R'_{out}) C_{\mu} \} + \underbrace{R'_{out} C_{\mu}}$$

Narrowband.

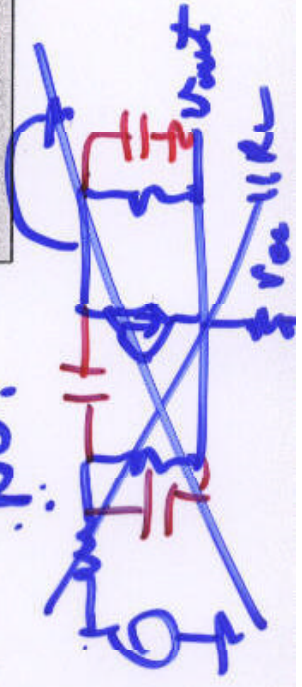
$\omega_{PEE} \ll \omega_T$

Common-Collector Amplifier



PEVICI

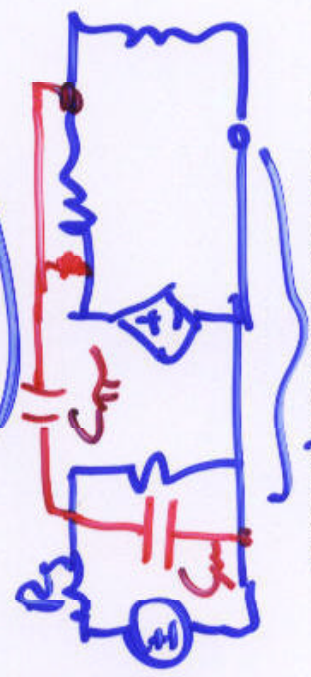
NO!



Procedure:

1. Small-signal two-port model
2. Add device (and other) capacitors

YES

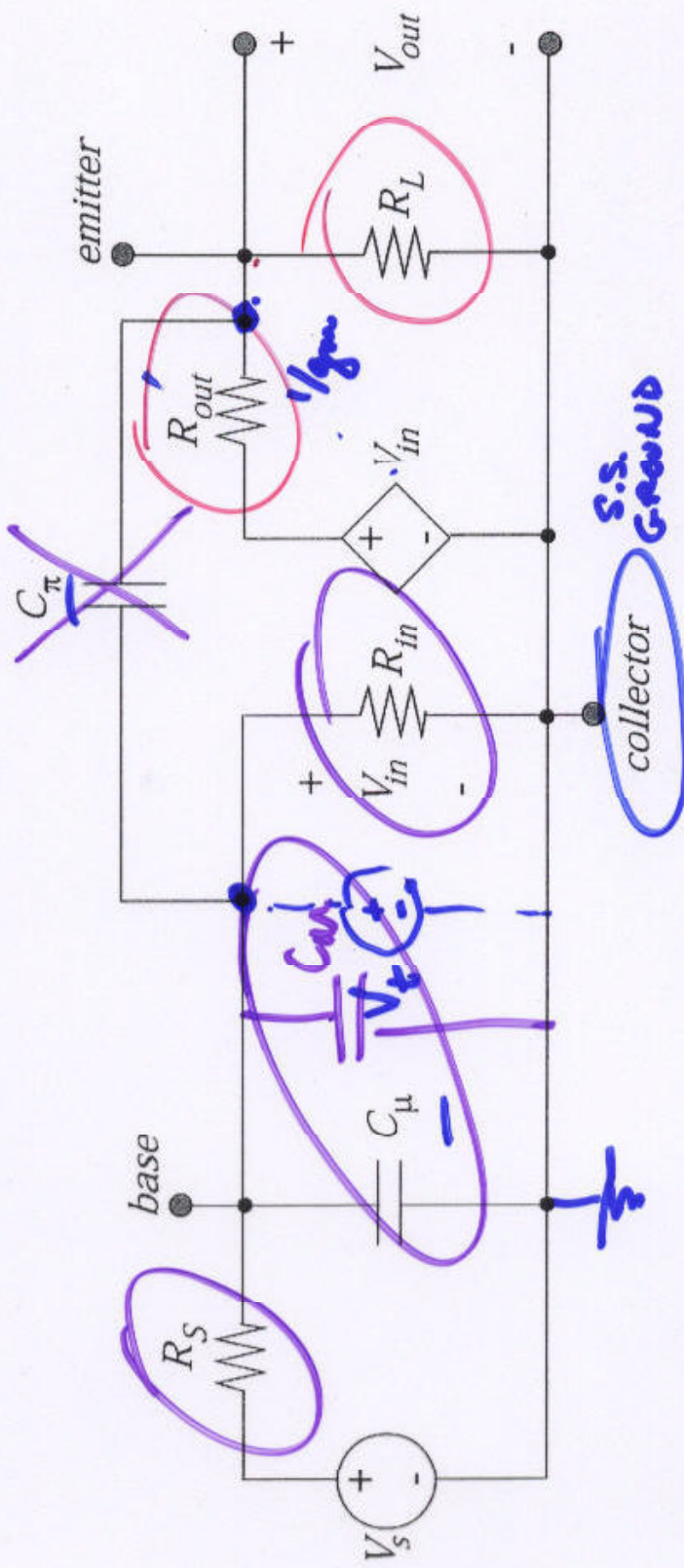


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2-PORT!

Two-Port CC Model with Capacitors



Find Miller capacitor for C_π -- note that the base-emitter capacitor is Between the input and output.

$$R_{out} = \frac{1}{g_m} + \frac{R_S}{\beta_0} \Big|_{\text{output } R_S}$$

$$A_{V_{CE}} = \frac{R_L}{\frac{1}{g_m} + R_C} = \frac{g_m R_L}{1 + g_m R_C}$$

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Voltage Gain $A_{vC\pi}$ Across C_π

$$A_{vC\pi} = \frac{g_m R_L}{1 + g_m R_L} (1 - A_{vC\pi}) = \frac{1 + \cancel{g_m R_L}}{1 + g_m R_L} \rightarrow \frac{\cancel{g_m R_L}}{1 + g_m R_L}$$

Note: this voltage gain is neither the two-port gain nor the "loaded" voltage gain.

$$C_{in} = C_\mu + C_M = C_\mu + (1 - A_{vC\pi}) C_\pi$$

$$\frac{C_\pi}{C_\mu} \approx 10 = C_\mu + \underbrace{\frac{C_\pi}{1 + g_m R_L}}_{\text{BOOTS TRAP } C_\pi}$$

Bandwidth of CC Amplifier

Input low-pass filter's -3 dB frequency:

$$\omega_p^{-1} = (\underline{R_S} \parallel R_{in}) \left(C_\mu + \frac{C_\pi}{1 + g_m R_L} \right)$$

$$R_{in} = r_\pi + (\beta + 1)(R_E \parallel R_C) \\ = \text{BIG.}$$

- Substitute favorable values of R_S , R_L : **BEST CASE**

$$\bullet \underline{R_S} \approx 1/g_m \quad \underline{R_L} \gg 1/g_m$$

$$\omega_p^{-1} \approx (1/g_m) \left(C_\mu + \frac{C_\pi}{1 + \text{BIG}} \right)$$

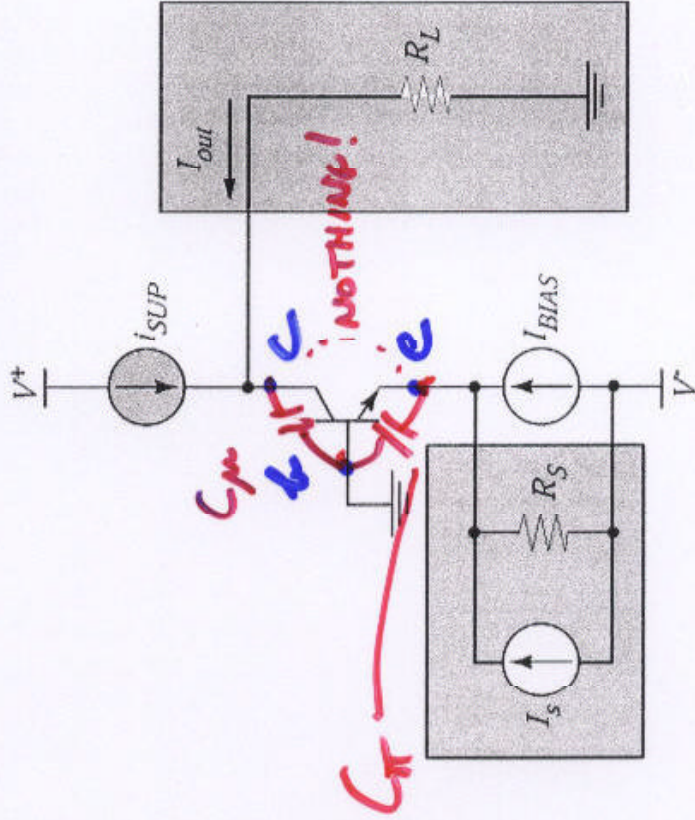
0 , **SMALL**
 $\approx C_\mu / g_m$

CC...

WIDEBAND

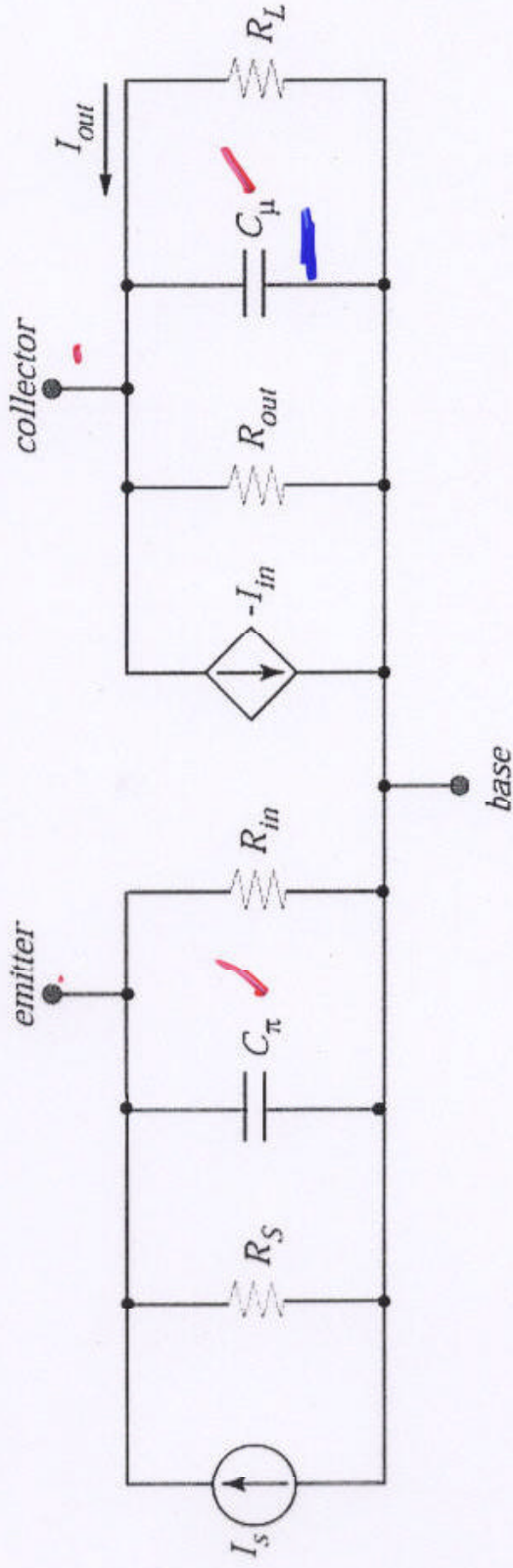
$$\omega_p = g_m / C_\mu \approx \omega_T$$

Bandwidth of the Common-Base Current Buffer



Same procedure: start with two-port model and capacitors

Two-Port CB Model with Capacitors



No Miller-transformed capacitor! *Good!*

Unity-gain frequency is on the order of ω_T for small R_L

$$\omega_p^{-1} = (R_{in} || R_S) C_{\pi} = \frac{C_{\pi}}{g_m} \approx \omega_T$$

$$\omega_p = g_m / C_{\pi} \approx \omega_T$$

Summary of Single-Stage Amplifier Frequency Response

- *n.b.* CE, CS: suffer from Miller-magnified capacitor for high-gain case
- CC, CD: Miller transformation \rightarrow nulled capacitor \rightarrow “wideband stage” $*$
- *n.b.* CB, CG: no Millerized capacitor \rightarrow wideband stage (for low load resistance) $*$