

EE128 LECTURE 6
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GOALS: understand and apply  
The NYQUIST STABILITY  
CRITERION  
to SISO systems

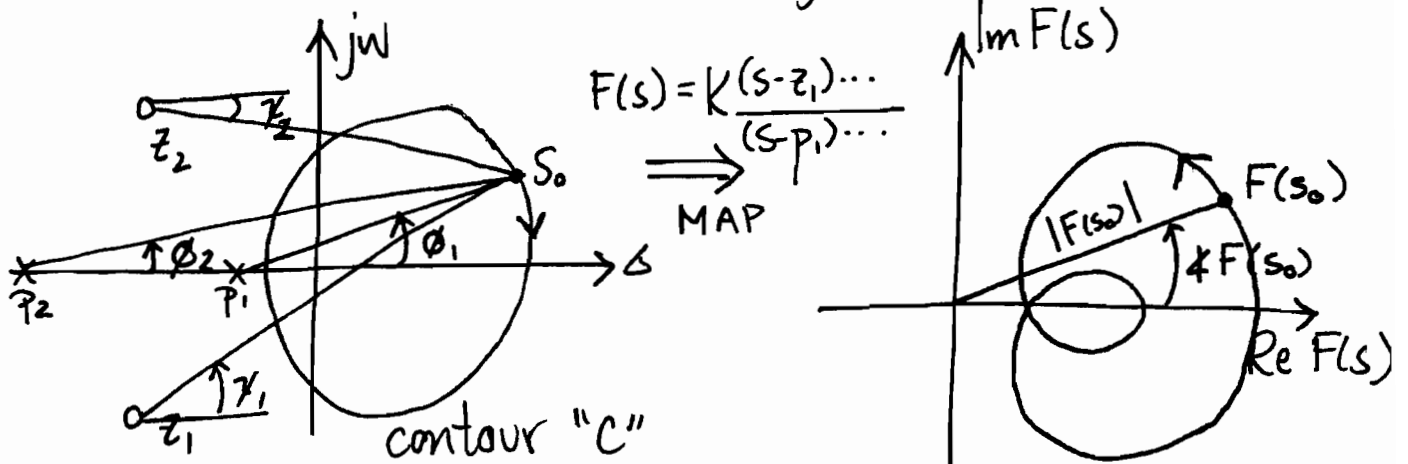
REFS: FPE §6.3, §6.4

# The Nyquist Stability Criterion

Harry Nyquist, Bell Labs  
1932

- how to explain these "reversals" in stability as  $K$  is increased?
- based on ...

## Cauchy's Principle of The Argument (B.10 FPE)

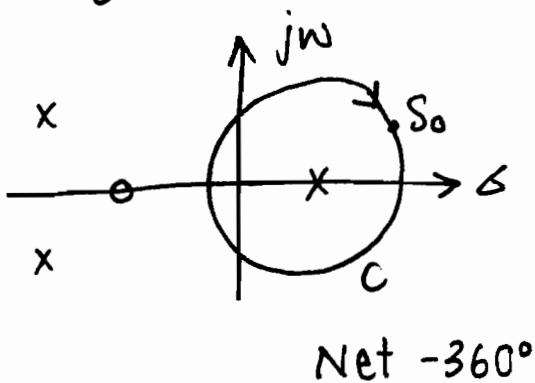


• as  $s_0$  moves around  $C$ , plot  $F(s_0)$  on  $F(s)$ -plane

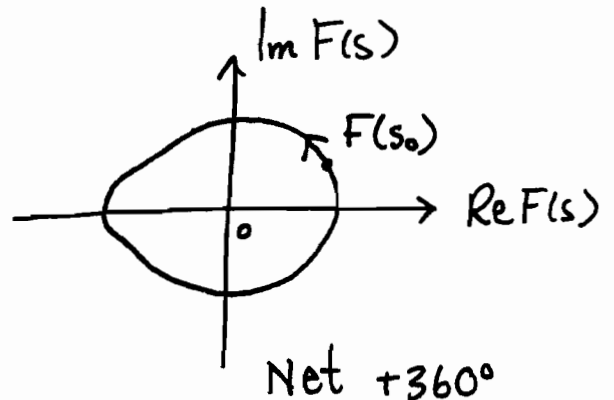
• net change of  $\angle F(s_0) = 0$  if no poles or zeros enclosed

- symmetric?
- not necessarily - depends on contour

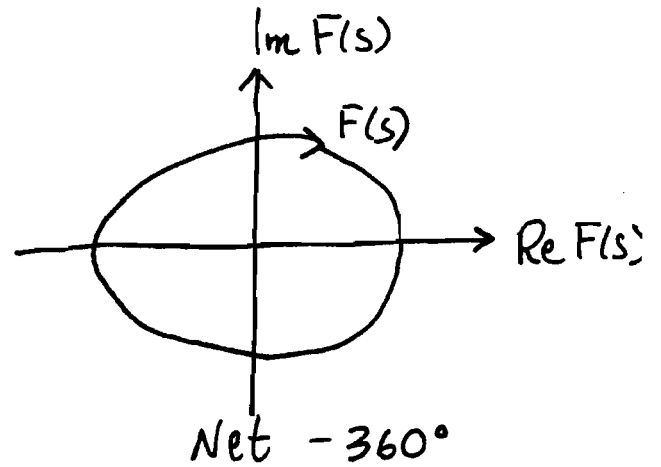
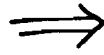
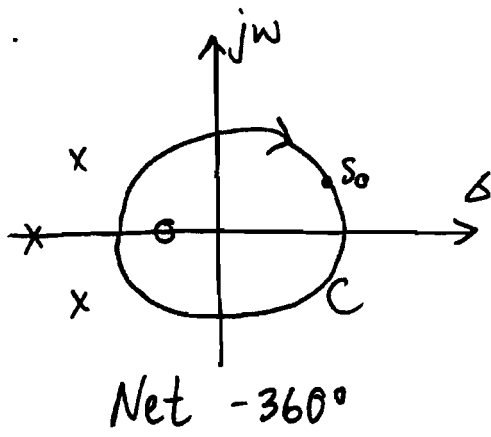
eg.



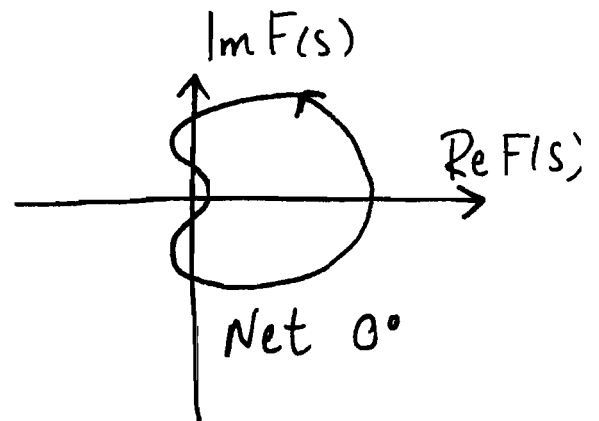
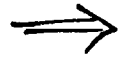
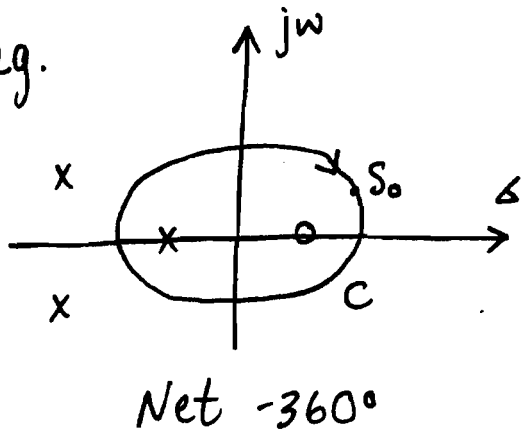
$\Rightarrow$



eg.



eg.



$$N = Z - P$$

$N$ : number of clockwise encirclements of  $F(s)$  of the origin in the  $F(s)$ -plane\*\*

$Z$ : zeros  
 $P$ : poles } of  $F(s)$  inside contour  $C$ \*

\* Assumed no poles or zeros on  $C$

\*\* Assumed contour  $C$  is taken clockwise

## Cauchy's Principle stated Concisely:

Let  $F(s)$  be the ratio of two polynomials in  $s$  and let the closed curve  $C$  in the  $s$ -plane be mapped onto the complex plane through the mapping  $F(s)$ . Assume  $F(s)$  has neither poles nor zeros on  $C$

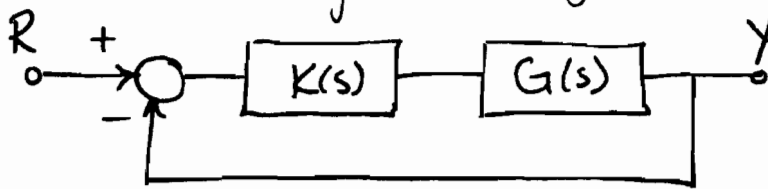
Then

$$N = Z - P$$

where  $Z$  is the number of zeros of  $F(s)$  in  $C$ ,  $P$  is the number of poles of  $F(s)$  in  $C$ , and  $N$  is the number of encirclements of  $F(s)$  (as  $s$  moves along  $C$ ) of the origin, taken in the same sense as  $C$ .

(section 6.3).

## Stability Analysis of Control Systems: (using Cauchy's Principle)



$$K(s) = K \cdot \frac{N_K(s)}{D_K(s)}$$

$$G(s) = \frac{N(s)}{D(s)}$$

$$\frac{Y}{R} = \frac{KG}{1 + KG}$$

$$\Delta(s) = 1 + K(s)G(s) = 0$$

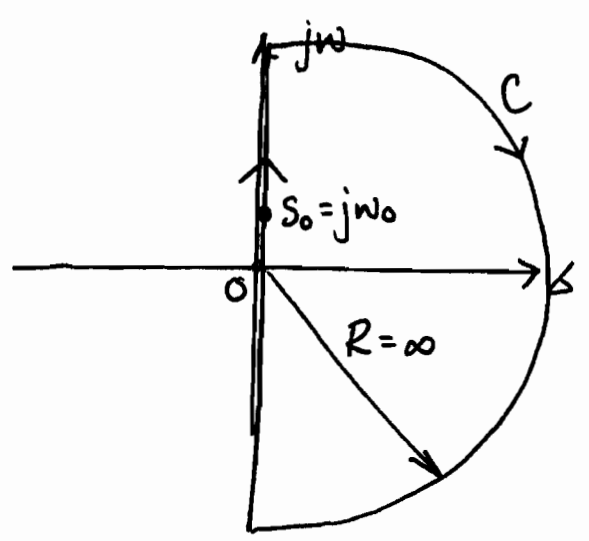
$$\therefore \Delta(s) = 1 + K \left( \frac{N_K(s)N(s)}{D_K(s)D(s)} \right) \rightarrow G_{OL}(s) \text{ "open loop TF"}$$

$$= \frac{D_K(s)D(s) + K N_K(s)N(s)}{D_K(s)D(s)}$$

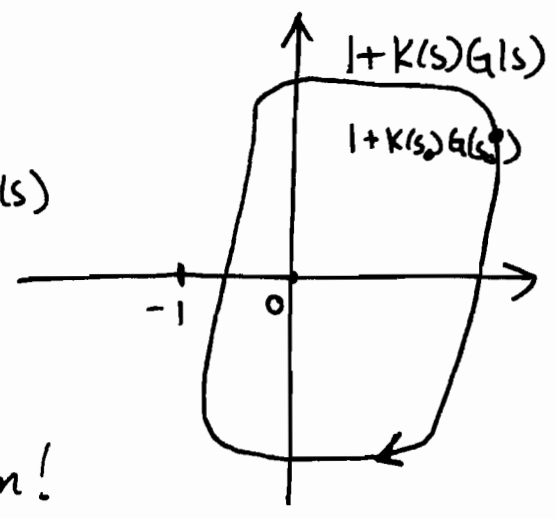
closed loop poles are zeros of  $\Delta(s)$

open loop poles are poles of  $\Delta(s)$

- use contour  $C$  which encircles the whole RHP:



$$1 + K(s)G(s) \Rightarrow$$



$$N = Z - P$$

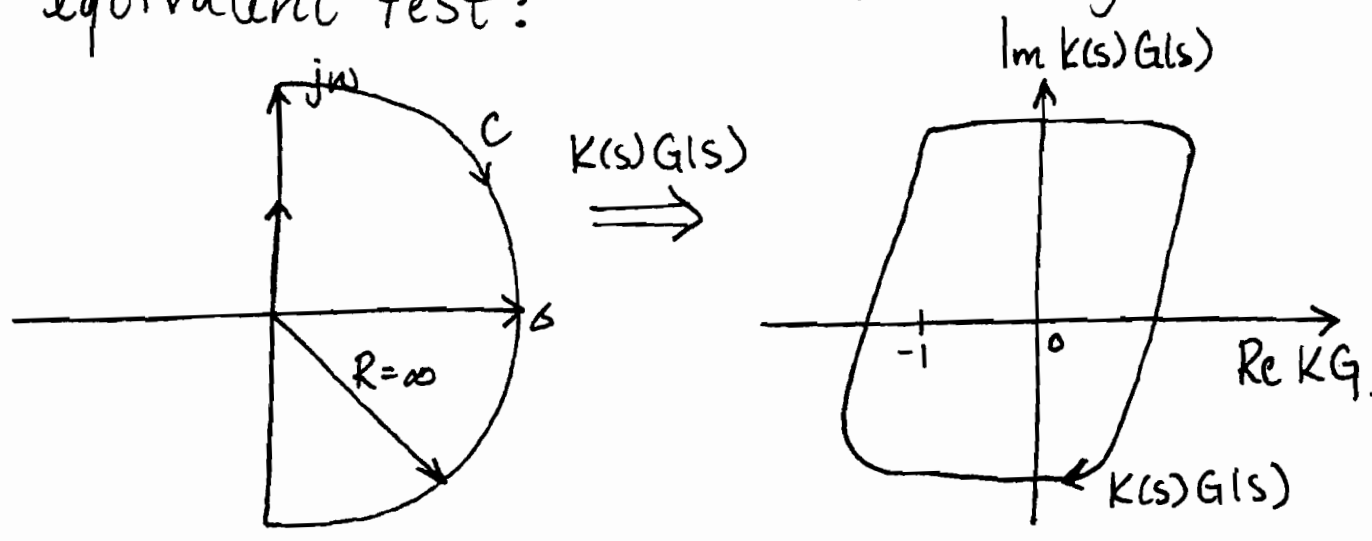
# encirclements of origin in  $F(s)$  plane

# open loop poles in RHP

$$\therefore Z = N + P$$

(want this to be ZERO for stability)  
 # zeros of  $\Delta(s)$  in RHP  
 (= # CL poles in RHP)

Instead of mapping the contour C through  $1 + K(s)G(s)$  and counting encirclements of the origin, we do the following equivalent test:



$$KG = (1 + KG) - 1$$

$$N^{1+KG} \text{ wrt. } 0 = N^{KG} \text{ wrt. } -1$$

$$Z = N + P$$

# zeros of  $\Delta(s)$  in RHP.

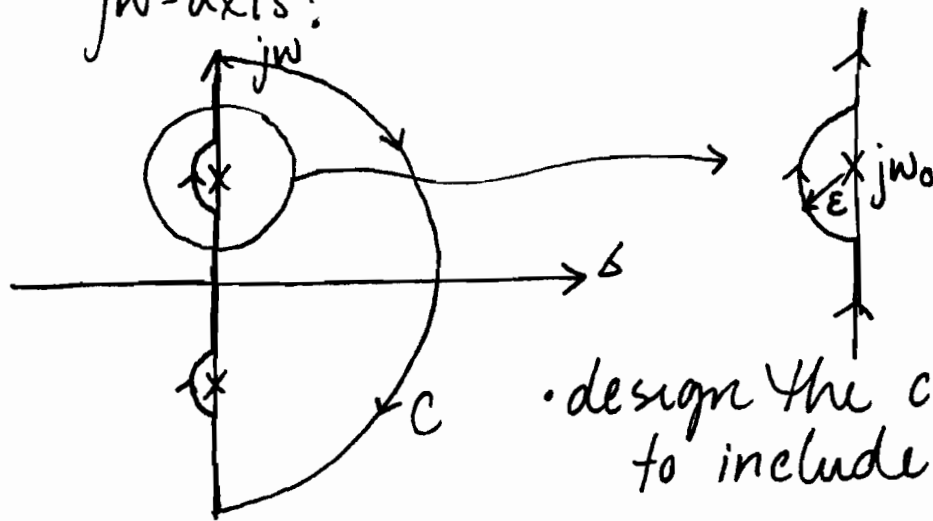
# of encirclements of  $-1 + j0$  in  $K(s)G(s)$ -plane

# OL poles in RHP

want to be zero for stability.

The map of this contour C through the characteristic equation is called the NYQUIST PLOT, and the criterion that  $N = -P$  is called NYQUIST STABILITY CRITERION

What to do if you have poles or zeros on  $j\omega$ -axis?



• design the contour  $C$  to include these.

Also, we can use the Nyquist plot and Nyquist stability criterion to determine the range of  $K$  for which  $1 + KG_{OL}(s) = 0$  has roots in the RHP, by determining the Nyquist plot of  $G_{OL}(s) = \frac{N_K(s)N(s)}{D_K(s)D(s)}$  and enumerating encirclements of  $-\frac{1}{K} + j0$ .

Why?

Because, stability depends on the location of the roots of:

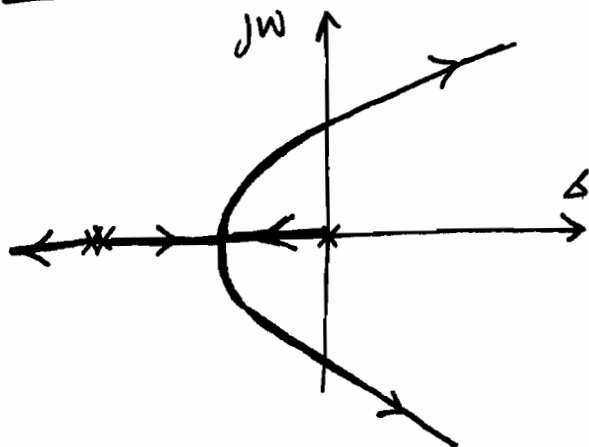
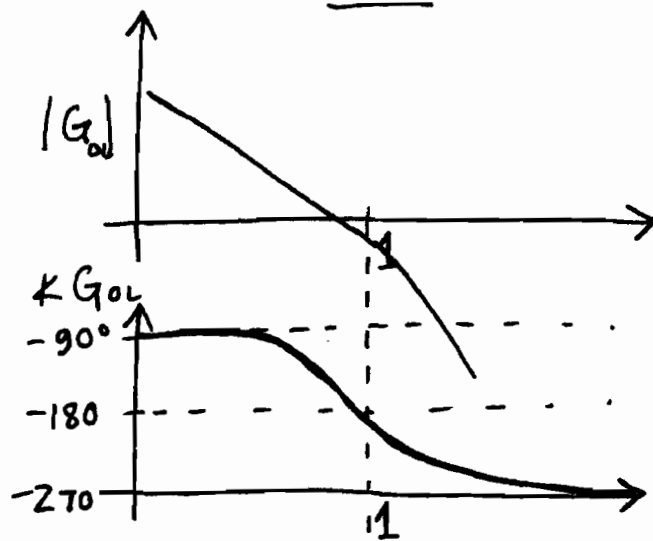
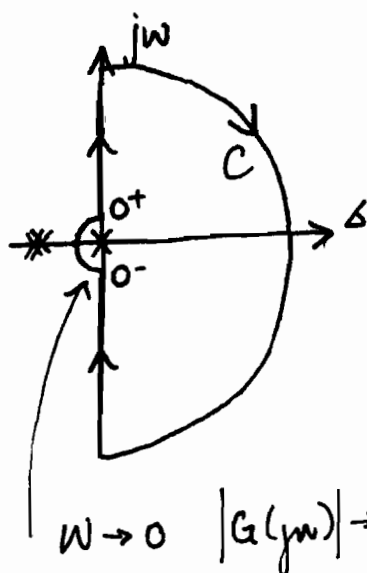
$$1 + KG_{OL}(s) = 0$$

$$\Rightarrow K \left[ \frac{1}{K} + G_{OL}(s) \right] = 0$$

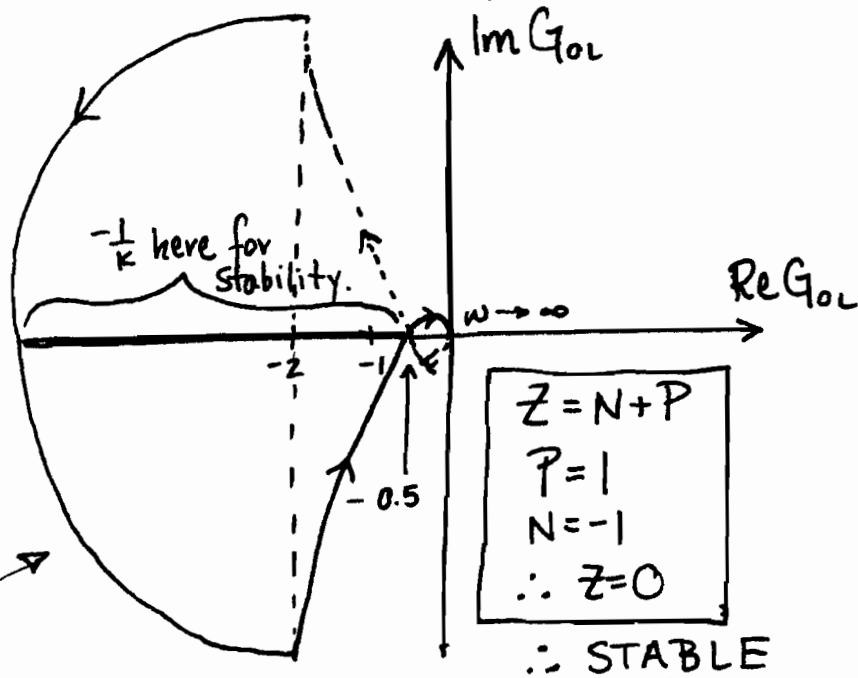
$\therefore$  Nyquist plot critical around  $-\frac{1}{K}$

Example

$$G_{ol}(s) = \frac{K}{s(s+1)^2} \quad (\text{let } K=1 \text{ first})$$

Root LocusBodeNYQUIST :

$\omega \rightarrow 0 \quad |G(j\omega)| \rightarrow \infty$



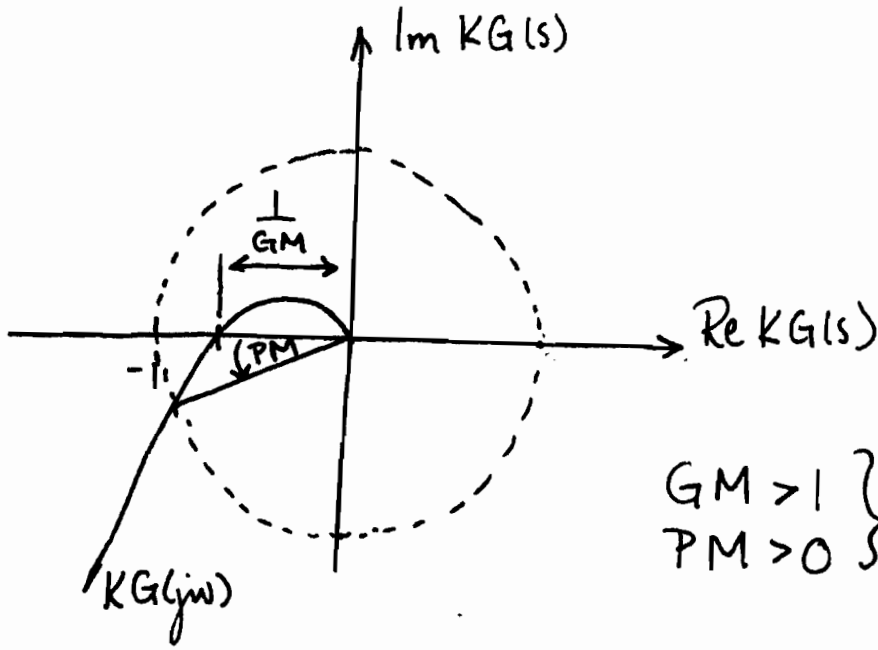
Asymptote : Find real part of  $G_{ol}(j\omega)$  : for  $K=1$ .

$$G_{ol}(j\omega) = \frac{1}{j\omega(j\omega+1)^2} = \frac{-2\omega^2 - j\omega(1-\omega^2)}{4\omega^2 + \omega^2(1-\omega^2)}$$

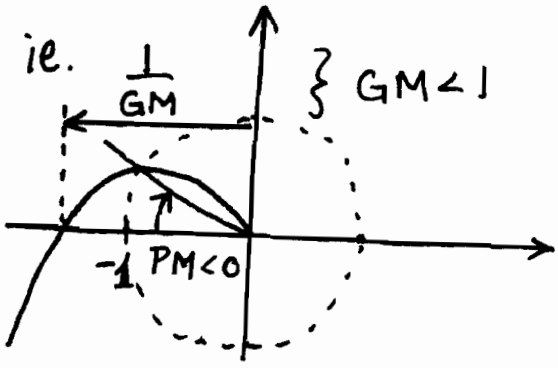
$$\therefore \text{Re}(G_{ol}(j\omega)) = \frac{-2}{1+\omega^4+2\omega^2} \rightarrow -2 \quad \text{as } \omega \rightarrow 0$$



# Gain Margin and Phase Margin on Nyquist 6-10

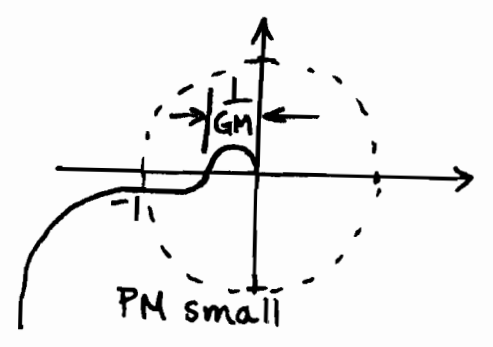


$GM > 1$   
 $PM > 0$  } for stability.

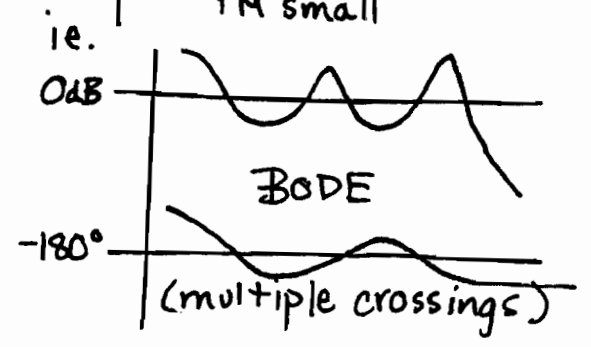
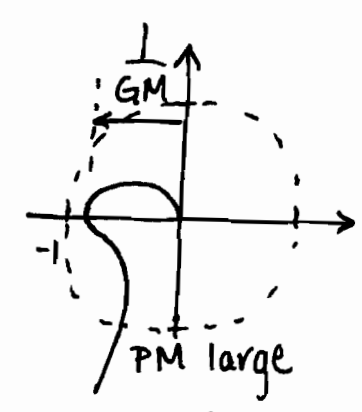


unstable!

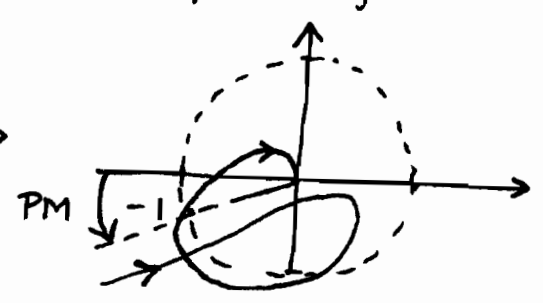
ie. extreme cases :



or



⇒



## Worked Nyquist Problems

1. Consider the system  $G(s) = \frac{1}{(s+10)(s+2)^2}$  in unity feedback with constant gain  $K$  in series. For what range of  $K$  is the system stable?
- Q.

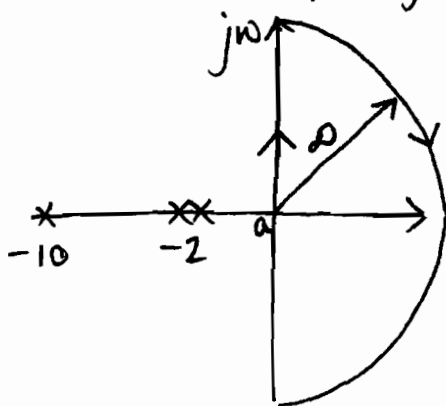
- as  $\omega \rightarrow 0$   $|G(j\omega)| = \frac{1}{40}$ ,  $\angle G(j\omega) = 0^\circ$
- as  $\omega \rightarrow \infty$   $|G(j\omega)| \rightarrow 0$ ,  $\angle G(j\omega) = -270^\circ$
- Stability: find where  $G(j\omega)$  is real:

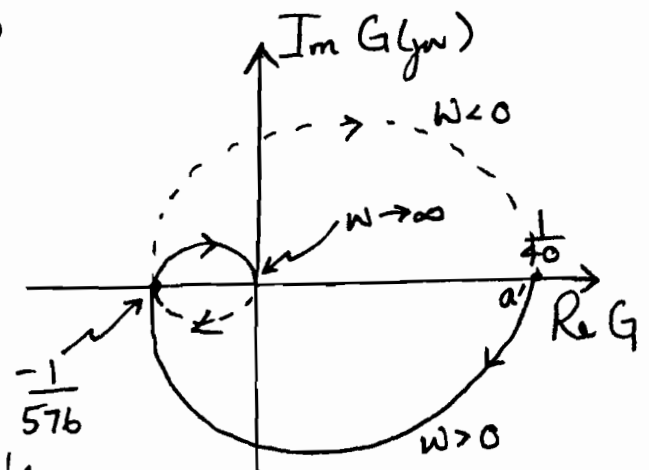
$$G(j\omega) = \frac{1}{(j\omega+10)(j\omega+2)^2} = \frac{1}{40 - 14\omega^2 + j(44\omega - \omega^3)}$$

$$G(j\omega) \text{ is real when } 44\omega = \omega^3$$

$$\Rightarrow \omega = 0, \omega^2 = 44$$

$$\text{and } |G(j\sqrt{44})| = \frac{1}{576}$$



$$\xrightarrow{G(j\omega)}$$


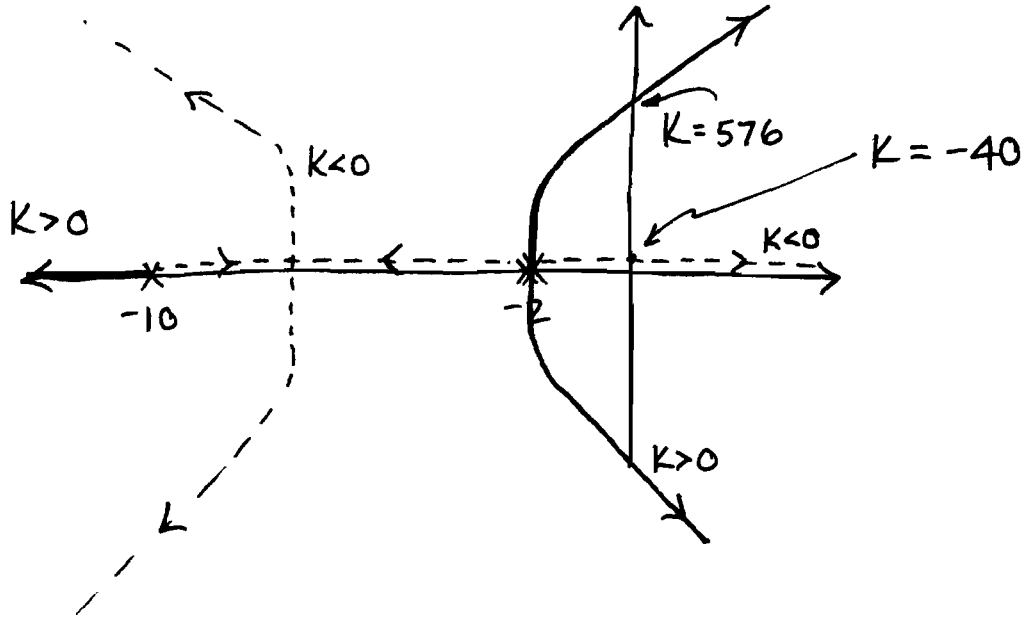
No open loop unstable pole

$$\Rightarrow P = 0, Z = N$$

$$\Rightarrow -40 < K < 576, Z = N = 0$$

system stable

check root locus:

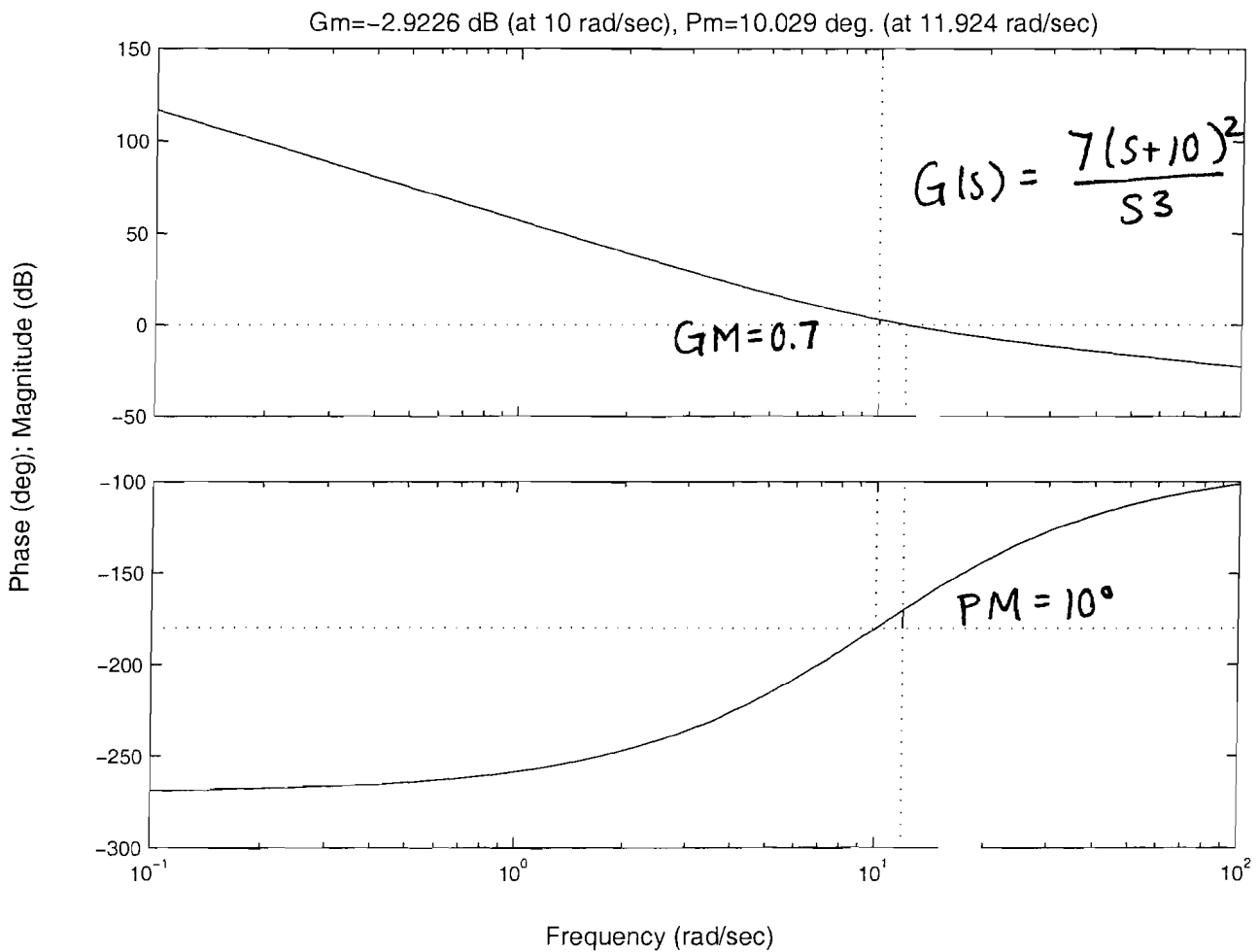


2. When is Bode not that useful?

example:  $G(s) = \frac{K(s+10)^2}{s^3}$

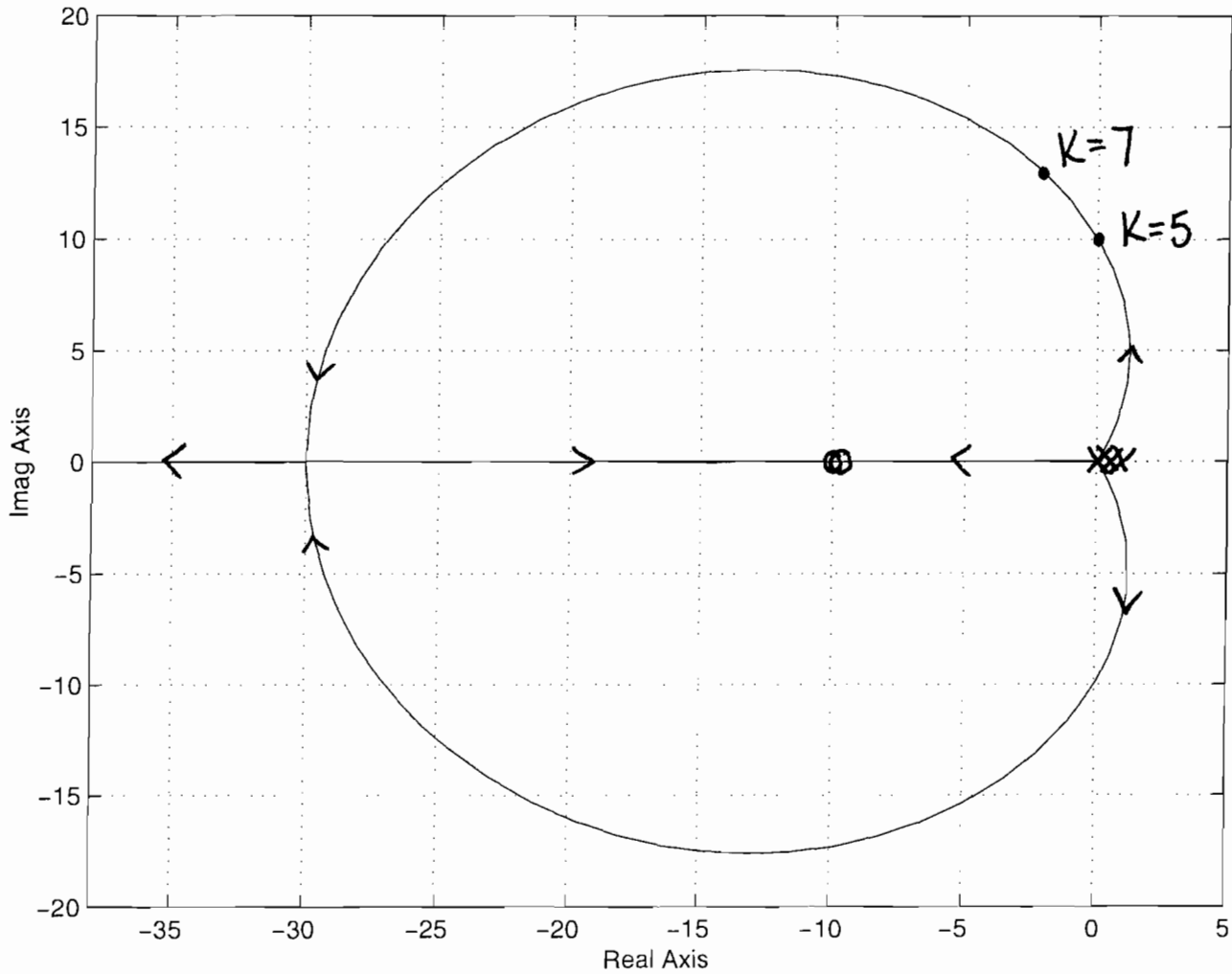
Choose  $K=7$  and plot Bode:

Bode Diagrams



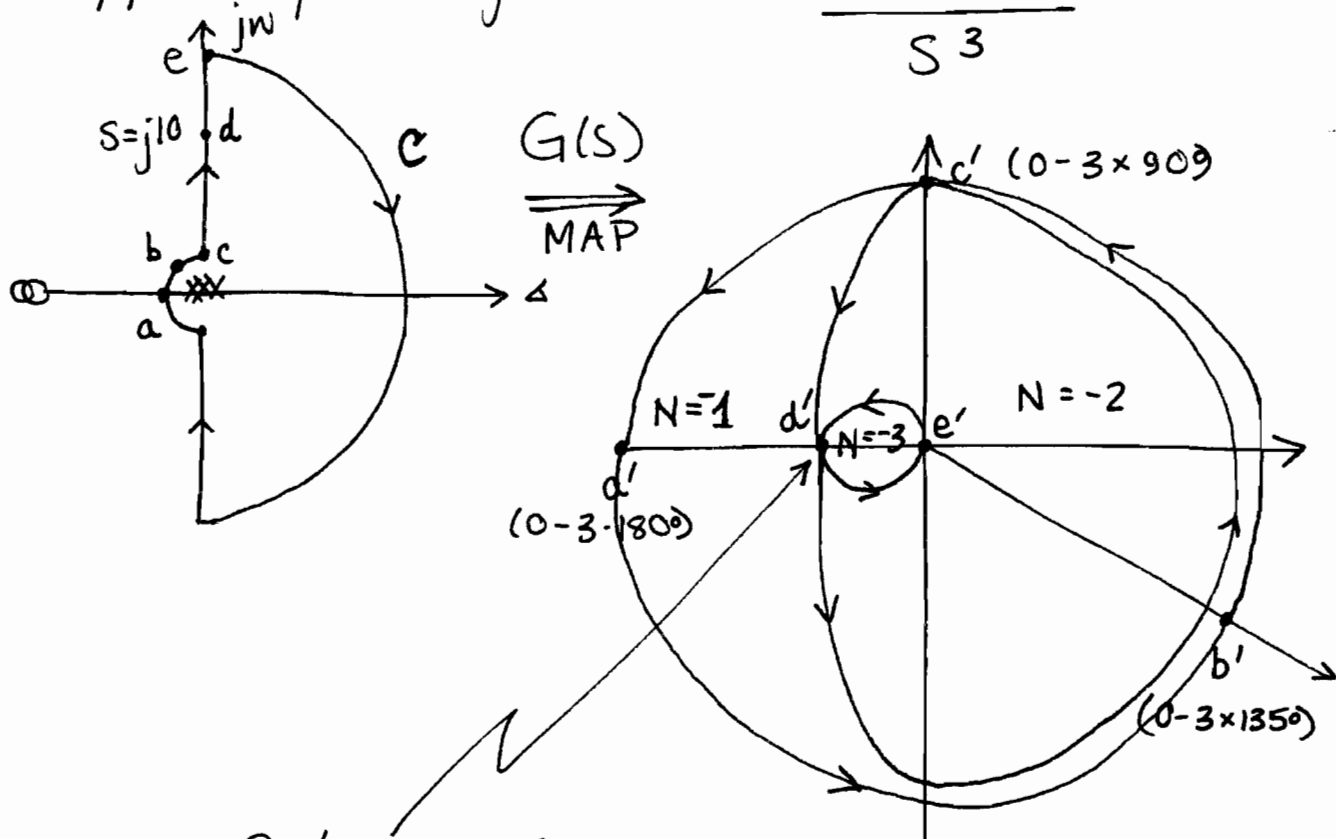
$GM = 0.7$ $PM = 10^\circ$	??
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Root locus of  $\frac{(s+10)^2}{s^3}$



- root locus indicates  
absolute stability  
• margins ??

Nyquist plot of  $G(s) = \frac{K(s+10)^2}{s^3}$



@  $d \Rightarrow s = j10$

$\therefore d'$  is determined by:

$$G(j10) = \frac{(10+j10)^2}{(j10)^3} \therefore |G(j10)| = 0.2$$

$$N = Z - P \leftarrow 3$$

$\therefore N = -3$  for stability

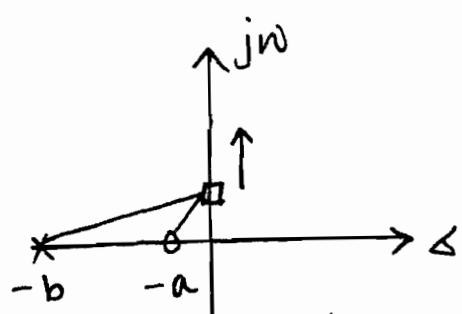
$\therefore$  stable for  $0 \leq -\frac{1}{K} \leq -0.2$

$\Rightarrow$  stable for  $K > 5$

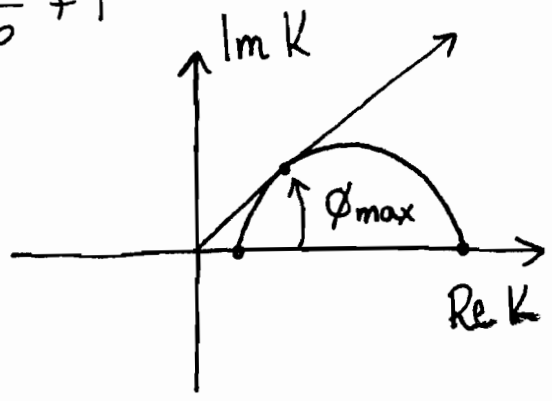
$\therefore$  Nyquist gives much more information...

Q: how does LEAD compensation affect a Nyquist plot?

$$K(s) = K_{lead} \frac{\frac{s}{a} + 1}{\frac{s}{b} + 1}$$

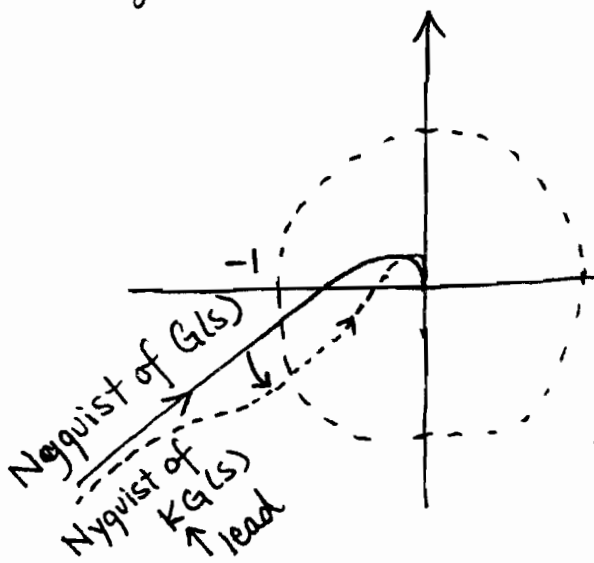


$K(s)$   
MAP



"LEAD": phase due to zero always leads phase due to pole.

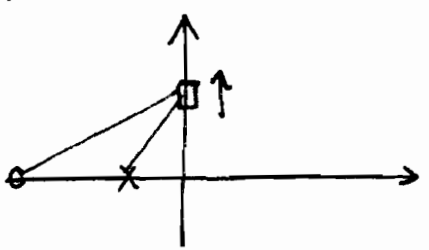
effect of LEAD on Nyquist of  $G(s)$ :



lead compensator has the effect of causing the Nyquist plot to swing away

from the  $-1 + j0$  point.  
 $\Rightarrow \uparrow$  stability.

how about LAG?



$K(s)$   
MAP

