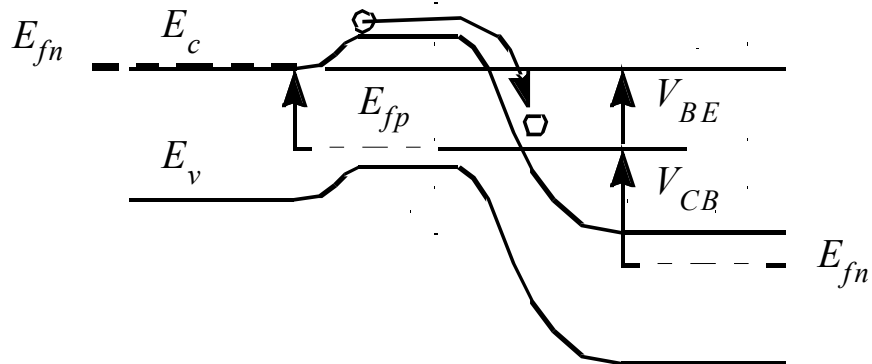
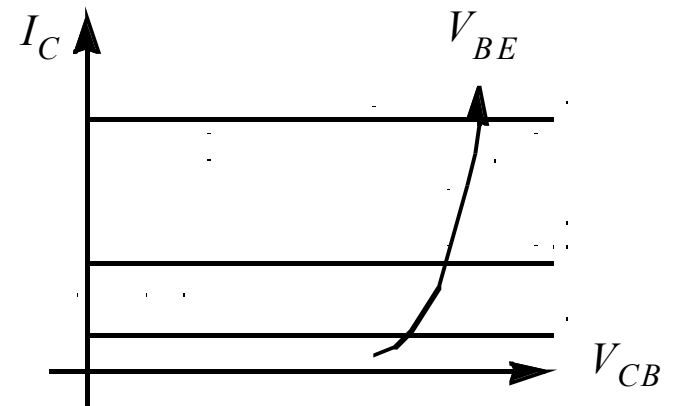
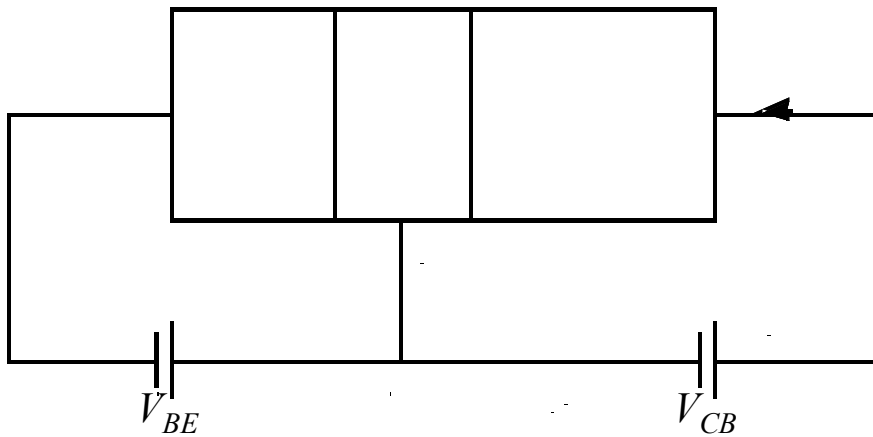


# *Chapter 8 Bipolar Junction Transistors*

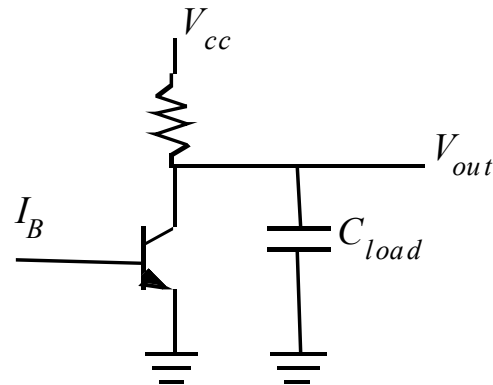
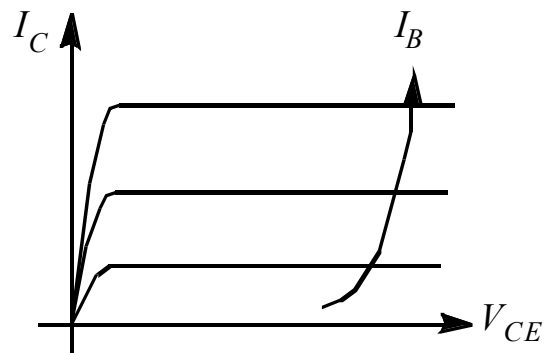
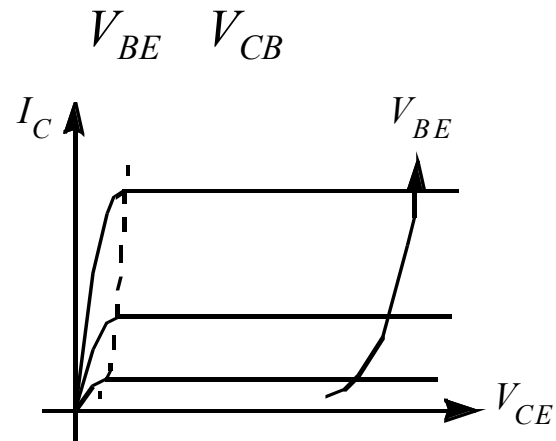
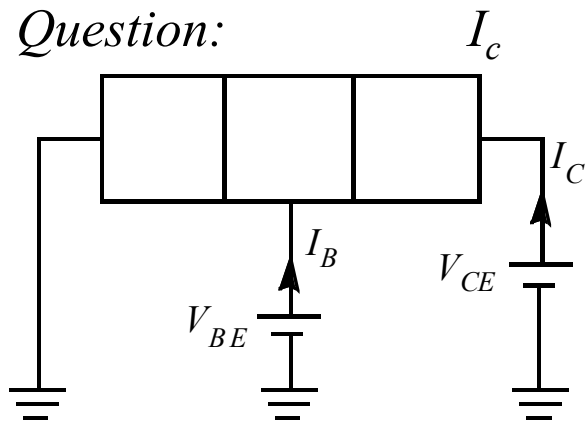
*Question*

## 8.1 Introduction to the BJT



# Common-Emitter Configuration

Question:

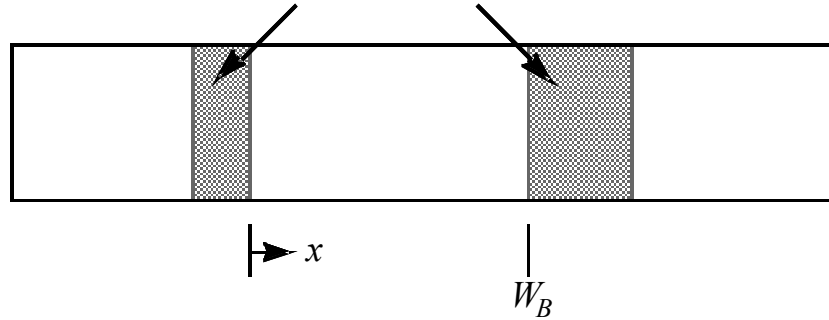


Question

$I_B$

$V_{BE}$

## 8.2 Collector Current



$$\frac{d n'}{dx} = \frac{n'}{L_B}$$

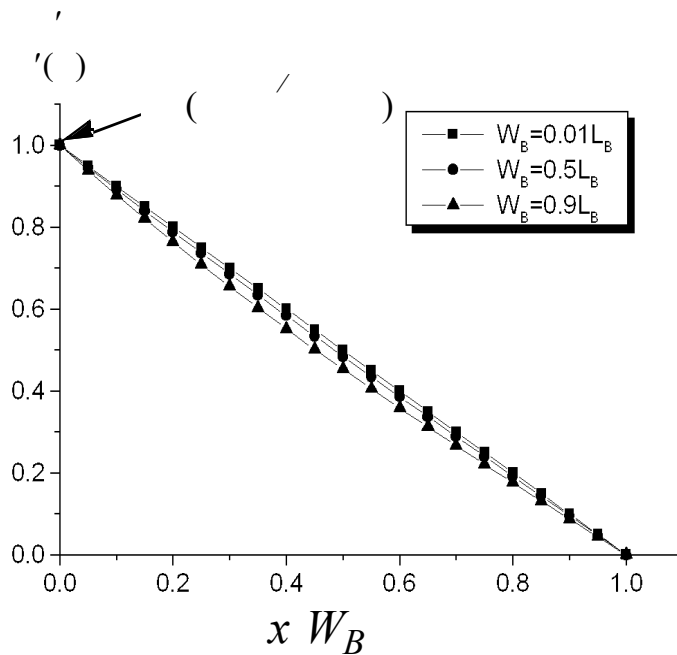
$$L_B \equiv \sqrt{\tau_B D_B}$$

$$n' = n_B e^{qV_{BE} / kT} -$$

$$n' W_B = n_B e^{qV_{BC} / kT} - \approx -n_B \approx$$

## 8.2 Collector Current

$$n' x = n_B e^{qV_{BE}/kT} - \frac{\left(\frac{W_B - x}{L_B}\right)}{(W_B/L_B)}$$



$$\begin{aligned} n' x &= n' - x W_B \\ &= \frac{n_{iB}}{N_B} e^{qV_{BE}/kT} - x W_B \end{aligned}$$

$$I_C = \left| A_E q D_B \frac{dn}{dx} \right|$$

$$= A_E q \frac{D_B}{W_B} \frac{n_{iB}}{N_B} e^{qV_{BE}/kT}$$

$$I_C = I_S e^{qV_{BE}/kT}$$

$$I_C = A_E \frac{qn_i}{G_B} e^{qV_{BE}/kT}$$

$$G_B \equiv \int_0^{W_B} \frac{n_i}{n_{iB}} \frac{p}{D_B} dx$$

$G_B$

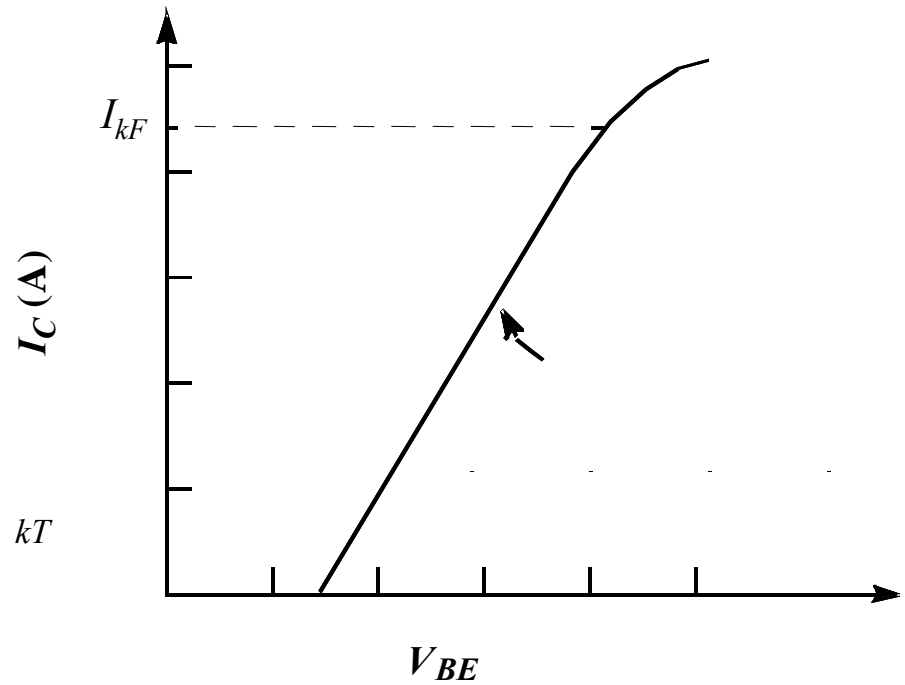
*base Gummel number*

# Gummel Plot

$p \quad N_B,$

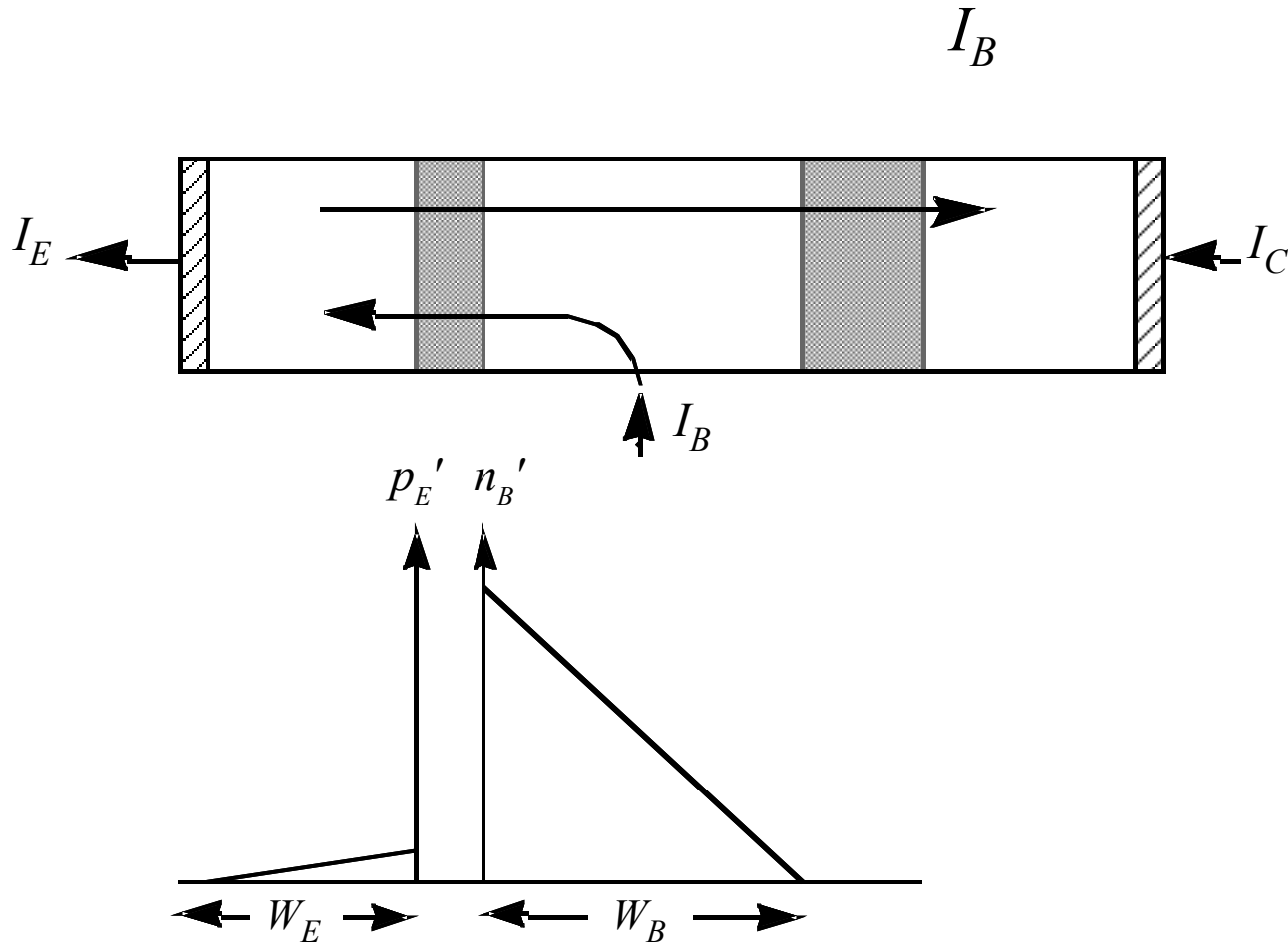
$$I_C \propto e^{qV_{BE}/kT}$$

$I_C$

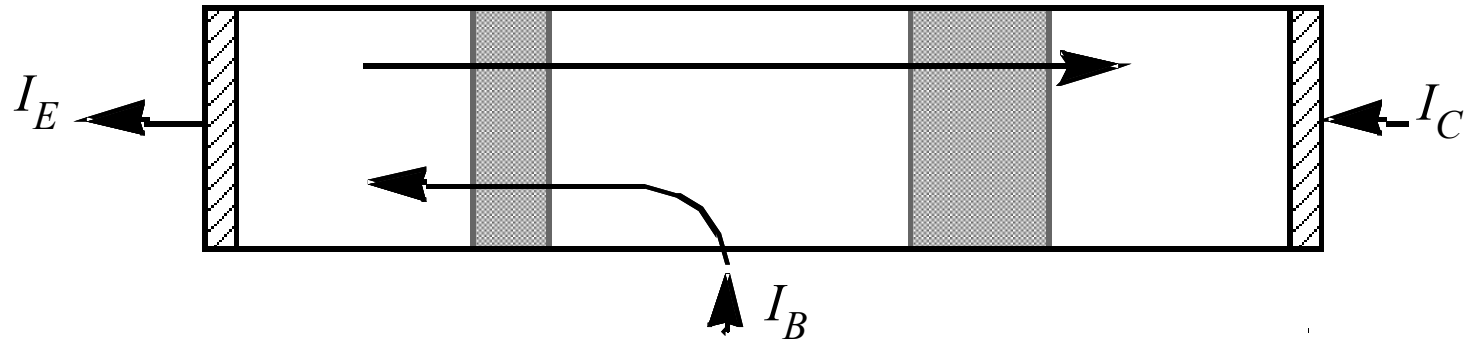


$V_{BE}$

## 8.3 Base Current



## 8.3 Base Current



$$I_B = A_E \frac{qn_i}{G_E} e^{qV_{BE}/kT} -$$

$$G_E \equiv \int_{-W_E}^{W_E} \frac{n_i}{n_{iE}} \frac{n}{D_E} dx$$

$$I_B = A_E q \frac{D_E n_{iE}}{W_E N_E} e^{qV_{BE}/kT} -$$

Question

$I_B$



## 8.4 Current Gain

$$\beta_F$$

$$\beta_F \equiv \frac{I_C}{I_B}$$

$$I_C = \alpha_F I_E$$

$$\alpha_F \equiv \frac{I_C}{I_E} = \frac{I_C}{I_B + I_C} = \frac{I_C}{I_C} \frac{I_B}{I_B + I_C} = \frac{\beta_F}{1 + \beta_F}$$

$$\beta_F = \frac{\alpha_F}{1 - \alpha_F}$$

$$\beta_F = \frac{G_E}{G_B} = \frac{D_B W_E N_E n_{iB}}{D_E W_B N_B n_{iE}}$$

$$\beta_F$$

## ***EXAMPLE: Current Gain***

*A BJT has  $I_C = 1 \text{ mA}$  and  $I_B = 10 \text{ }\mu\text{A}$ . What are  $I_E$ ,  $\beta_F$  and  $\alpha_F$ ?*

### ***Solution***

$$I_E = I_C + I_B = \quad + \quad =$$

$$\beta_F = I_C / I_B = \quad =$$

$$\alpha_F = I_C / I_E = \quad =$$

*We can confirm*

$$\alpha_F = \frac{\beta_F}{1 + \beta_F} \qquad \beta_F = \frac{\alpha_F}{1 - \alpha_F}$$

## 8.4.1 Emitter Bandgap Narrowing

$$\beta \propto \frac{N_E}{N_B} \frac{n_{iB}}{n_{iE}}$$

$$\beta_F \propto \frac{N_E}{N_B}$$

$$N_E$$

$$n_{iE} > n_i$$

$$n_i = N_C N_V e^{-E_g / kT}$$

$$n_i$$

$$E_g$$

$$n_{iE} = n_i e^{\Delta E_{gE} / kT}$$

$$\Delta E_{gE}$$

$$N_E$$

$$\beta_F$$

## 8.4.2 Narrow-Bandgap (SiGe) Base

$$\beta \propto \frac{N_E}{N_B} \frac{n_{iB}}{n_{iE}}$$

$$\beta_F$$

$$n_{iB}$$

$$\eta \quad \eta$$

$$\eta$$

$$E_{gB}$$

$$n_{iE}$$

## ***EXAMPLE: Emitter Bandgap Narrowing and SiGe Base***

Assume  $D_B = 3D_E$ ,  $W_E = 3W_B$ ,  $N_B = 10^{18} \text{ cm}^{-3}$ , and  $n_{iB}^2 = n_i^2$ . What is  $\beta_F$  for (a)  $N_E = 10^{19} \text{ cm}^{-3}$ , (b)  $N_E = 10^{20} \text{ cm}^{-3}$ , and (c)  $N_E = 10^{20} \text{ cm}^{-3}$  and a SiGe base with  $\Delta E_{gB} = 60 \text{ meV}$ ?

(a) At  $N_E = 10^{19} \text{ cm}^{-3}$ ,  $\Delta E_{gE} \approx 50 \text{ meV}$ ,

$$n_{iE} = n_i e^{\frac{\Delta E_{gE}}{kT}} = n_i e = n_i$$

$$\beta_F = \frac{D_B W_E}{D_E W_B} \cdot \frac{N_E n_i}{N_B n_{iE}} = \frac{3 \cdot 10^{19} \cdot n_i}{10^{18} \cdot n_i} = 3$$

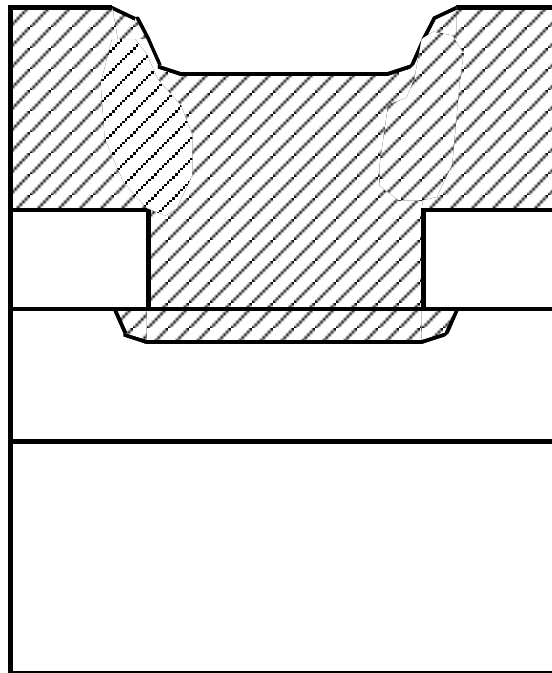
(b) At  $N_E = 10^{20} \text{ cm}^{-3}$ ,  $\Delta E_{gE} \approx 95 \text{ meV}$

$$n_{iE} = n_i e^{\frac{\Delta E_{gE}}{kT}} = n_i e^{1.8} \approx 6.05 n_i$$

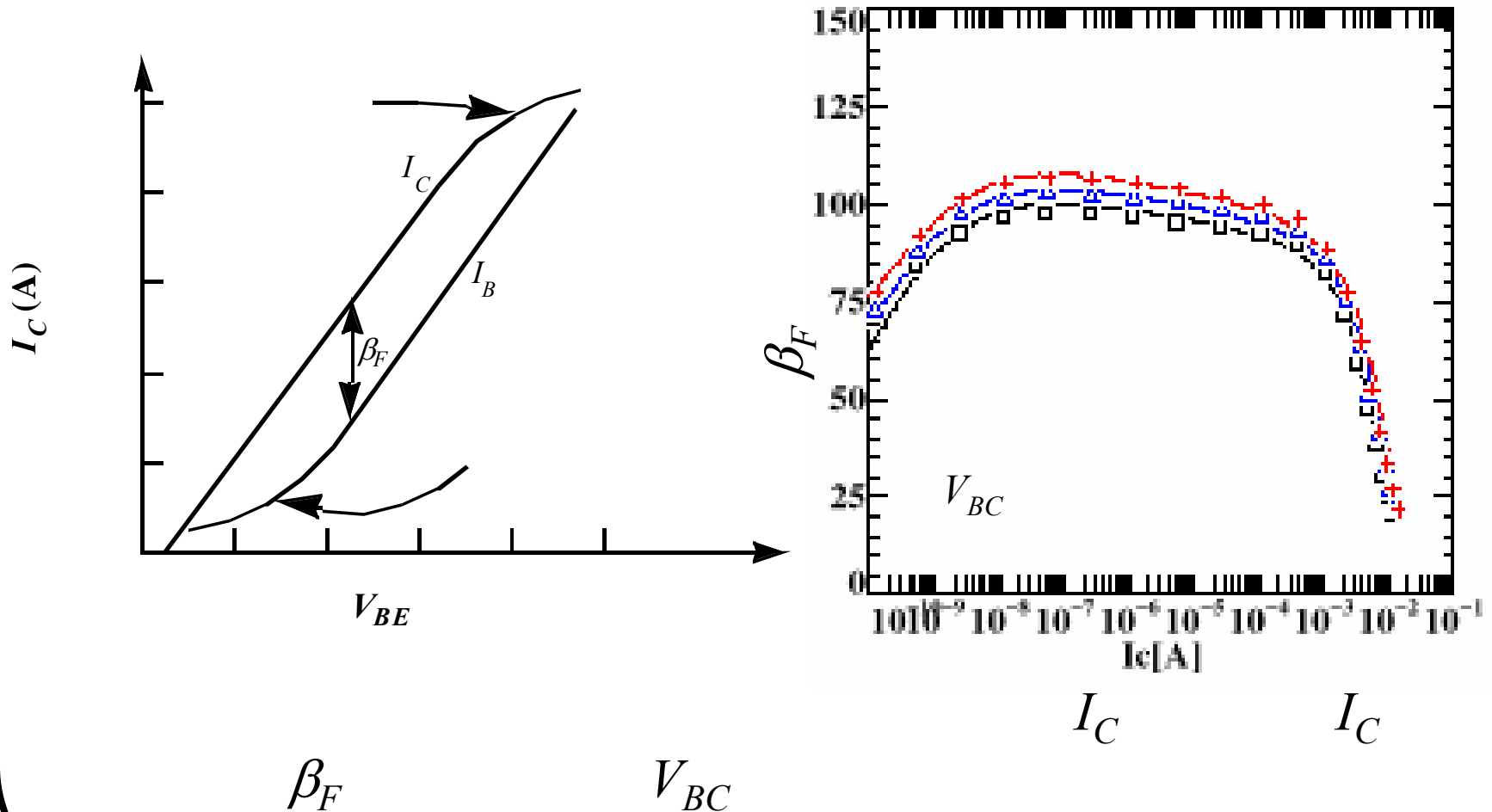
$$\beta_F =$$

(c)  $n_{iB} = n_i e^{\frac{\Delta E_{gB}}{kT}} = n_i e^{1.0} = n_i e$   $\beta_F =$

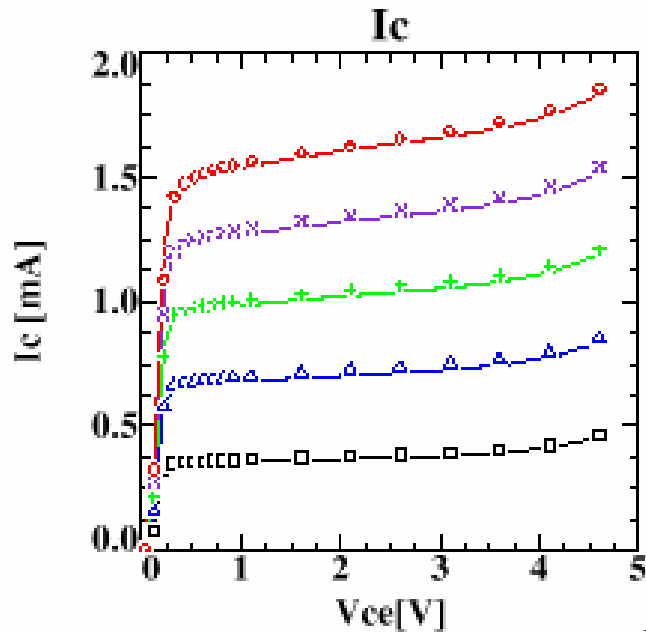
### 8.4.3 Poly-Silicon Emitter

 $\beta_F$  $W_E$ 

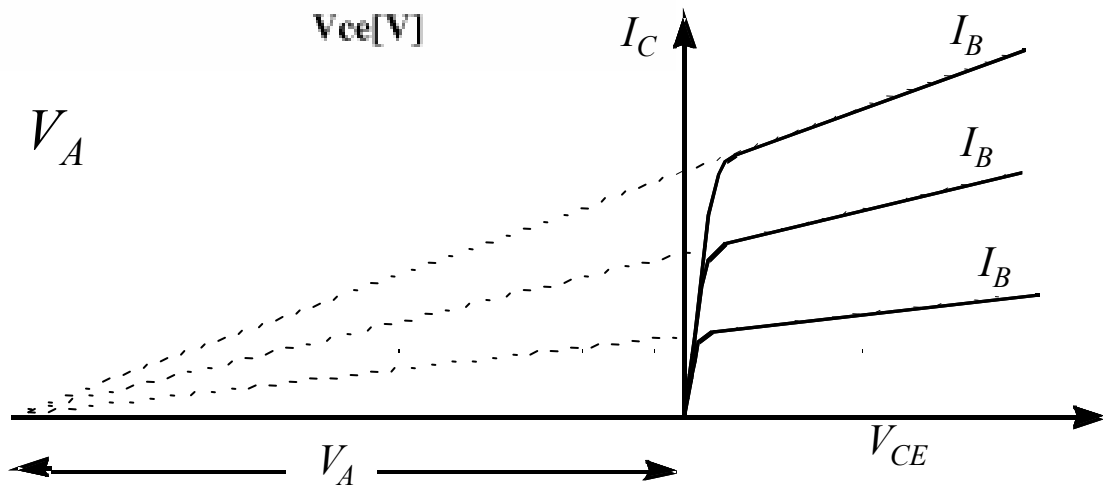
### 8.4.4 Gummel Plot and $\beta_F$ Fall-off at High and Low $I_c$



## 8.5 Base-Width Modulation by Collector Voltage



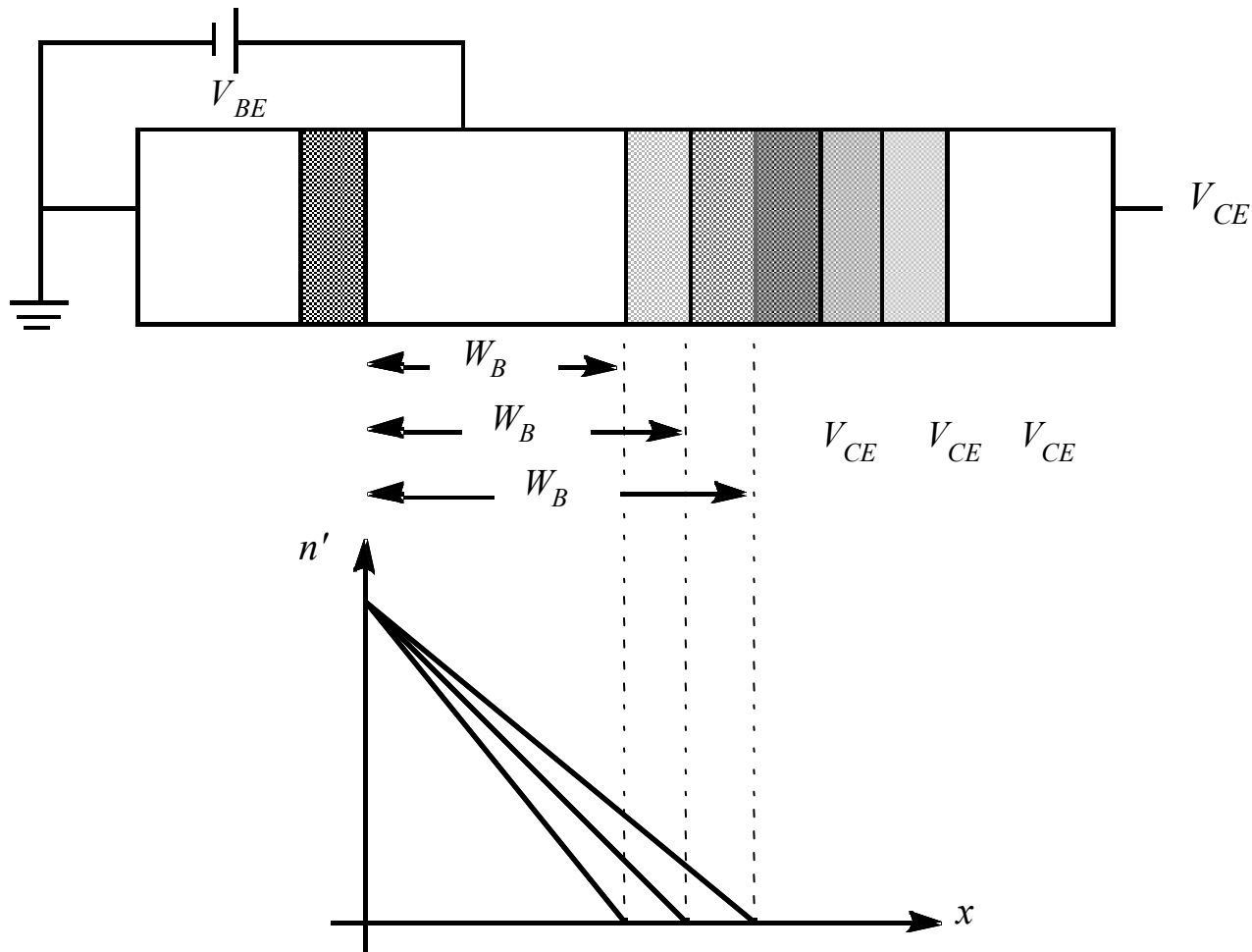
$$r \equiv \left( \frac{\partial I_C}{\partial V_{CE}} \right)^{-1} = \frac{V_A}{I_C}$$



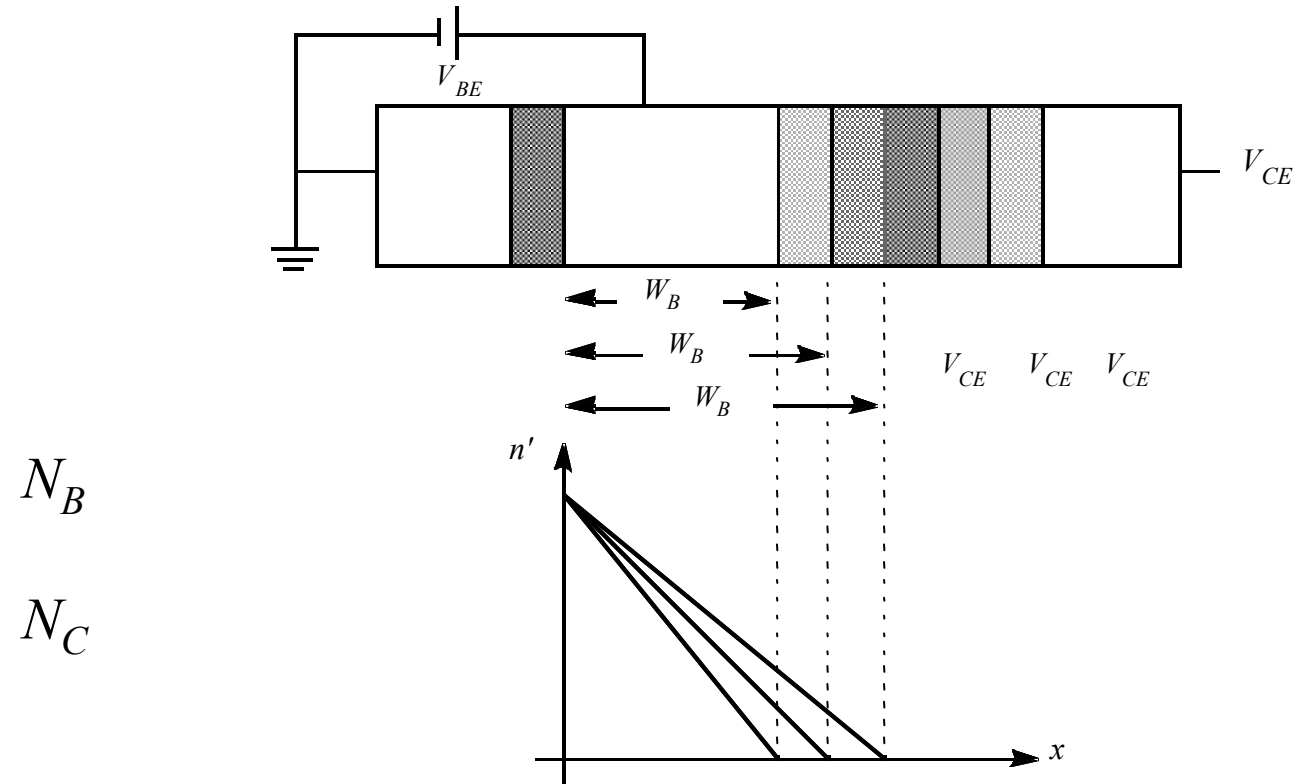
$$r_o = \frac{V_A}{I_C}$$



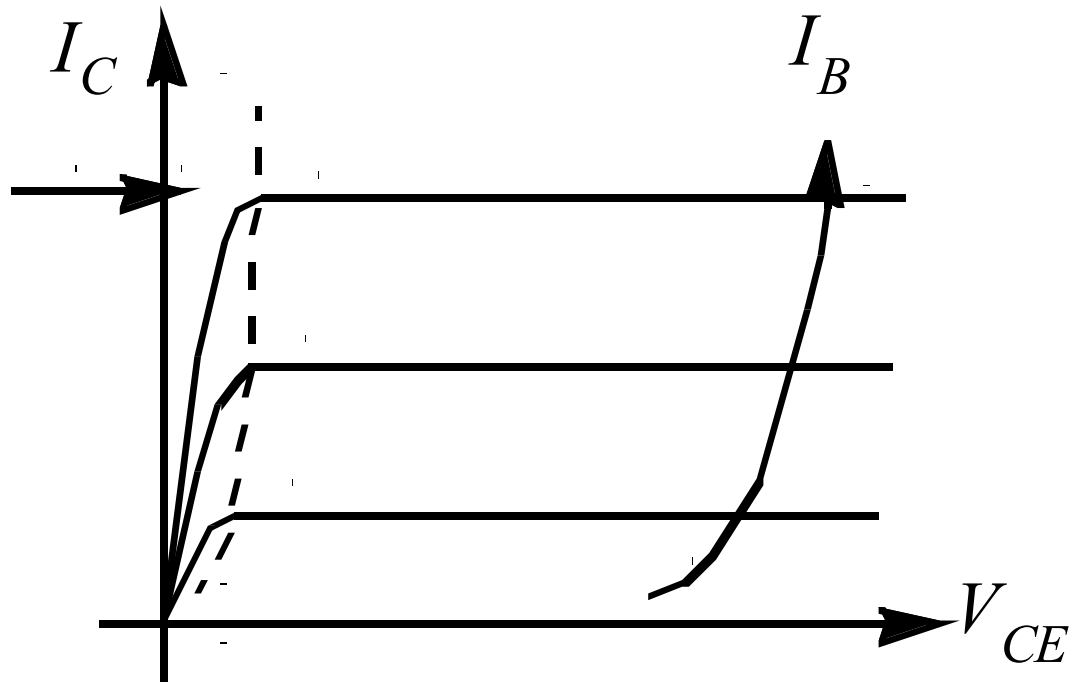
## 8.5 *Base-Width Modulation by Collector Voltage*



## 8.5 *Base-Width Modulation by Collector Voltage*



## 8.6 Ebers-Moll Model



## 8.6 Ebers-Moll Model

$I_C$

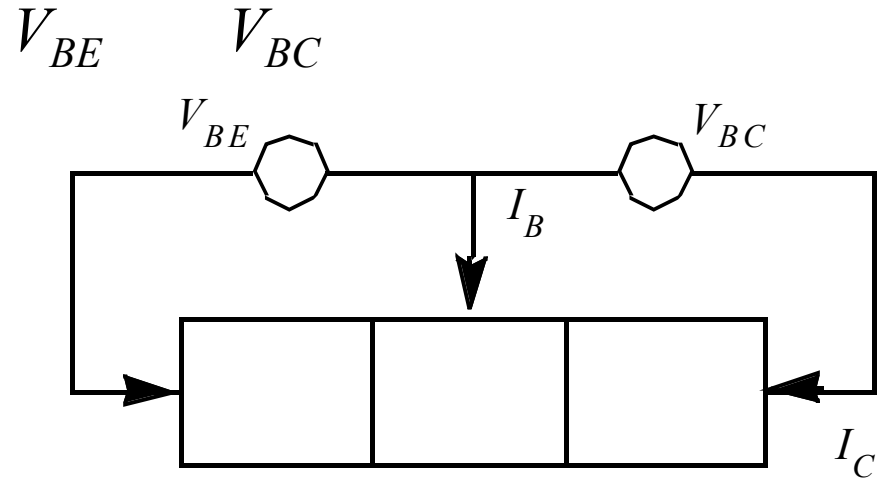
$$I_C = I_S e^{\frac{qV_{BE}}{kT}} - \frac{I_S}{\beta_F} e^{\frac{qV_{BE}}{kT}}$$

$$I_B = \frac{I_S}{\beta_F} e^{\frac{qV_{BE}}{kT}} - \frac{I_S}{\beta_R} e^{\frac{qV_{BC}}{kT}}$$

$$I_E = I_S e^{\frac{qV_{BC}}{kT}} - \frac{I_S}{\beta_R} e^{\frac{qV_{BC}}{kT}}$$

$$I_B = \frac{I_S}{\beta_R} e^{\frac{qV_{BC}}{kT}} - \frac{I_S}{\beta_F} e^{\frac{qV_{BE}}{kT}}$$

$$I_C = -I_E - I_B = -I_S + \frac{I_S}{\beta_R} e^{\frac{qV_{BC}}{kT}} - \frac{I_S}{\beta_F} e^{\frac{qV_{BE}}{kT}}$$



$\beta_R$   
 $\beta_F$

## 8.6 Ebers-Moll Model

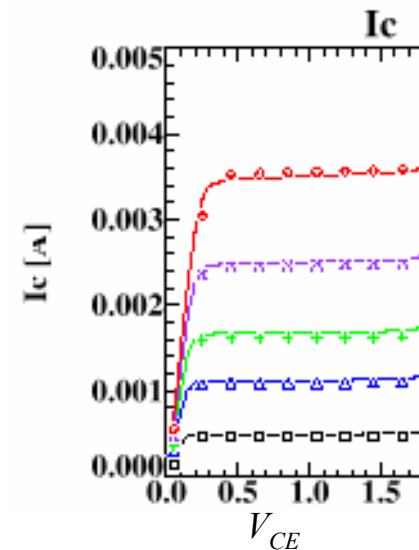
$$I_C = I_S e^{\frac{qV_{BE}}{kT}} - \frac{I_S}{\beta_R} e^{\frac{qV_{BC}}{kT}}$$

$$I_B = \frac{I_S}{\beta_F} e^{\frac{qV_{BE}}{kT}} + \frac{I_S}{\beta_F} e^{\frac{qV_{BC}}{kT}}$$

$V_{BC}$

$I_B$

$I_C$



## *8.7 Transit Time and Charge Storage*

$Q_F$

$$\tau_F \equiv \frac{Q_F}{I_C}$$

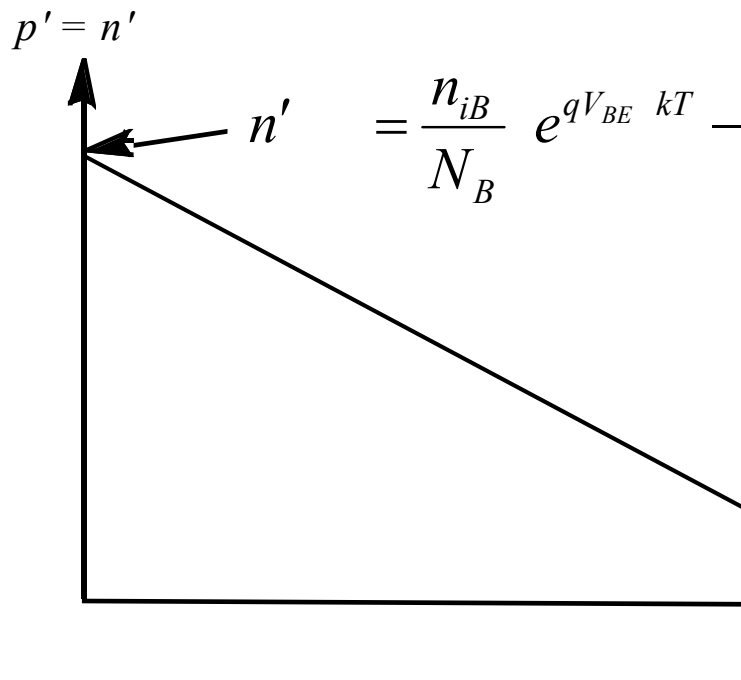
$\tau_F$

*$\tau_F$  determines the high-frequency limit of BJT operation.*

## 8.7.1 Base Charge Storage and Base Transit Time

$$Q_{FB} = qA_E n' W_B$$

$$\frac{Q_{FB}}{I_C} \equiv \tau_{FB} = \frac{W_B}{D_B}$$



### ***EXAMPLE: Base Transit Time***

*What is  $\tau_{FB}$  if  $W_B = 70 \text{ nm}$  and  $D_B = 10 \text{ cm}^2/\text{s}$ ?*

***Answer:***

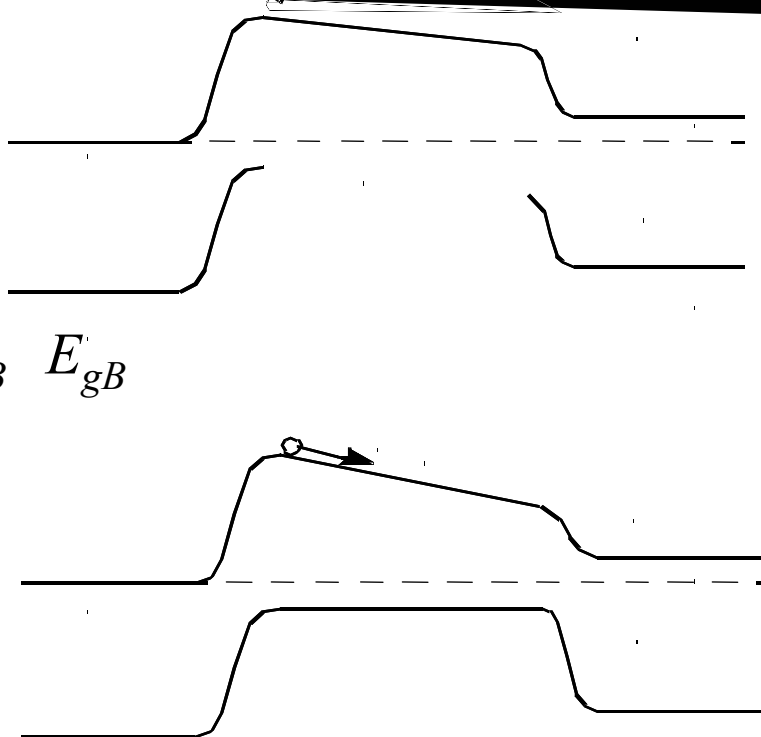
$$\tau_{FB} = \frac{W_B}{D_B} = \frac{70 \times 10^{-9} \text{ m}}{10 \times 10^{-4} \text{ m}^2/\text{s}} = 7 \times 10^{-6} \text{ s} = 7 \text{ } \mu\text{s}$$

*2.5 ps is a very short time. Since light speed is  $3 \times 10^8 \text{ m/s}$ , light travels only 1.5 mm in 5 ps.*

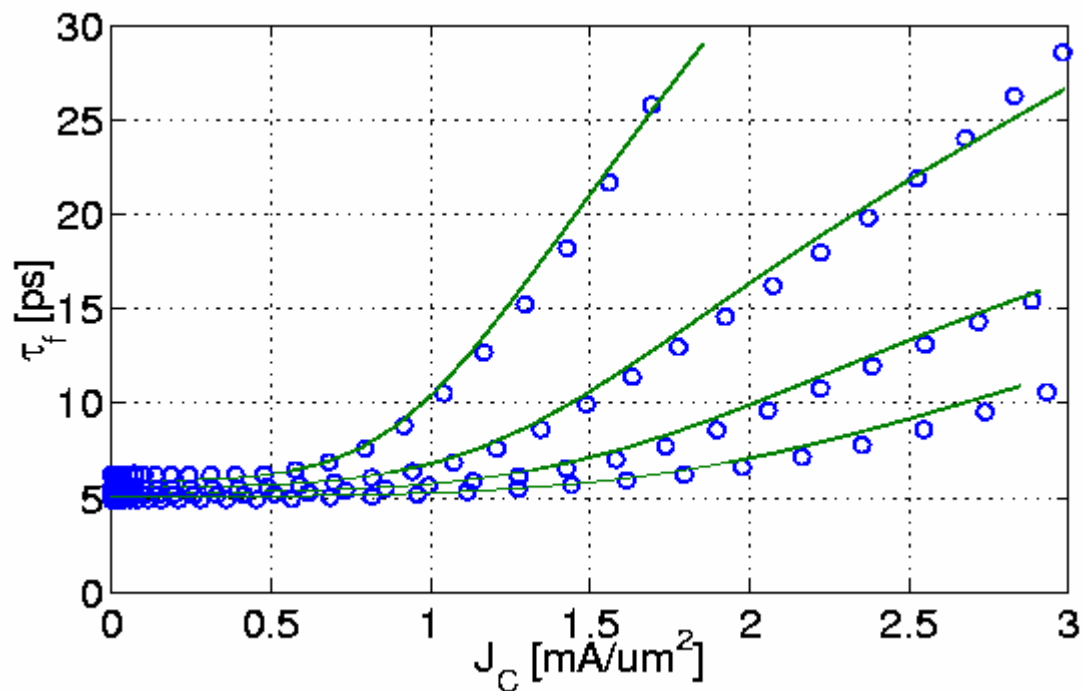


$E_{gB}$   $N_B$

$N_B$   $E_{gB}$



### 8.7.3 Emitter-to-Collector Transit Time and Kirk Effect



$n \quad N_C$

$\tau_F$

$V_{CE}$

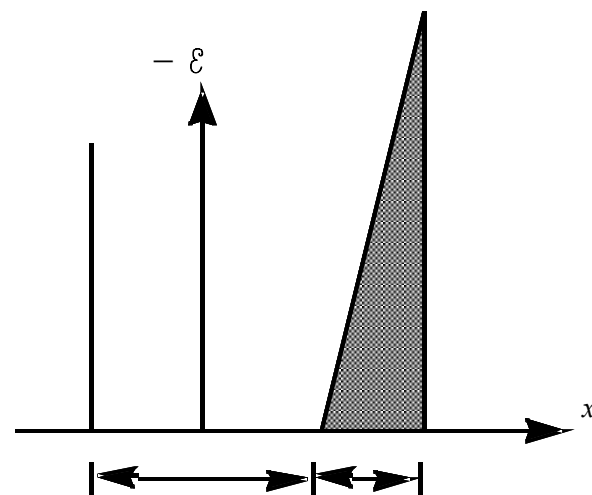
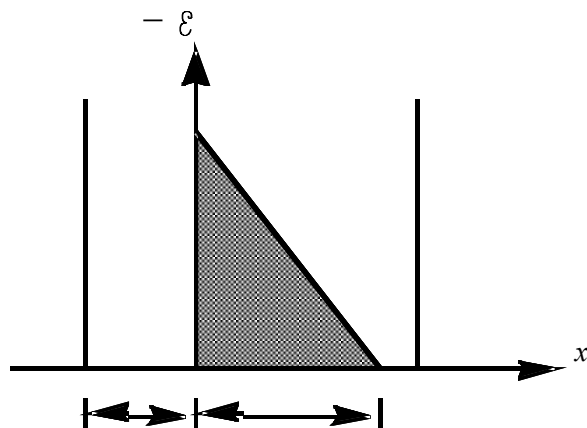
## *Base Widening at Large $I_c$*

$$I_C = A_E q n v_{sat}$$

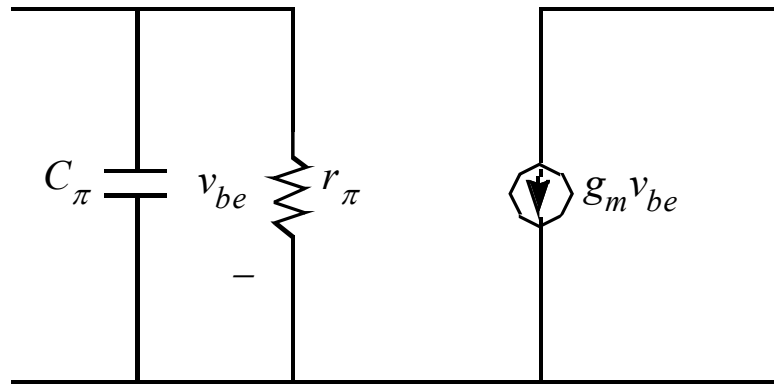
$$\rho = qN_C - qn$$

$$= qN_C - \frac{I_C}{A_E v_{sat}}$$

$$\frac{d\mathcal{E}}{dx} = \rho \quad \epsilon_s$$



## 8.8 Small-Signal Model



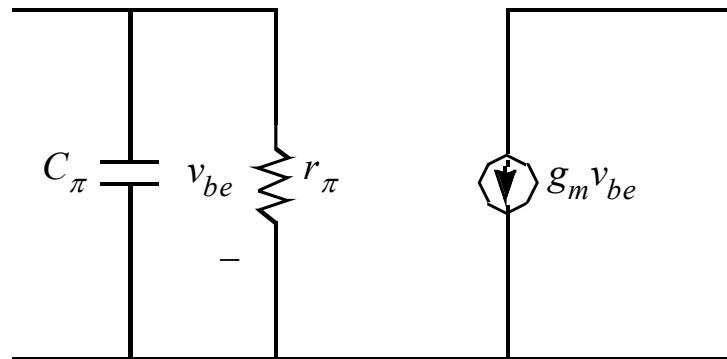
$$I_C = I_S e^{qV_{BE}/kT}$$

$$\begin{aligned} g_m &\equiv \frac{dI_C}{dV_{BE}} = \frac{d}{dV_{BE}} I_S e^{qV_{BE}/kT} \\ &= \frac{q}{kT} I_S e^{qV_{BE}/kT} = I_C \frac{q}{kT} \end{aligned}$$

$$g_m = I_C \frac{q}{kT}$$

$$g_m = I_C /$$

## 8.8 Small-Signal Model



$$\frac{1}{r_\pi} = \frac{dI_B}{dV_{BE}} = \frac{1}{\beta_F} \frac{dI_C}{dV_{BE}} = \frac{g_m}{\beta_F} \quad r_\pi = \beta_F \frac{1}{g_m}$$

$$C_\pi = \frac{dQ_F}{dV_{BE}} = \frac{d}{dV_{BE}} \tau_F I_C = \tau_F g_m$$

*diffusion capacitance*

$$C_\pi = \tau_F g_m + C_{dBE}$$

## ***EXAMPLE: Small-Signal Model Parameters***

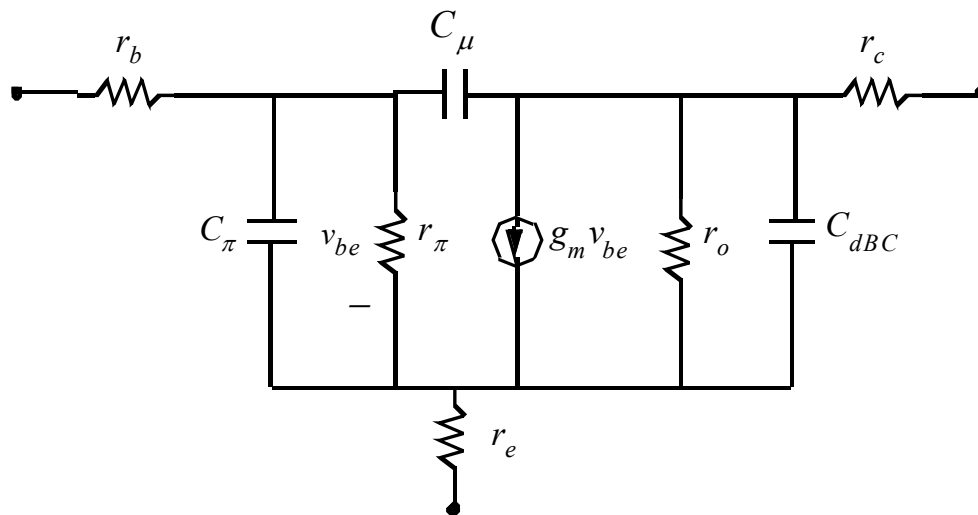
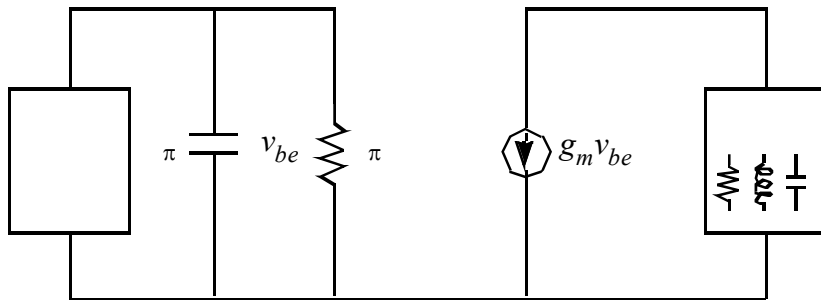
*A BJT is biased at  $I_C = 1 \text{ mA}$  and  $V_{CE} = 3 \text{ V}$ .  $\beta_F = 90$ ,  $\tau_F = 5 \text{ ps}$ , and  $T = 300 \text{ K}$ . Find (a)  $g_m$ , (b)  $r_\pi$ , (c)  $C_\pi$ .*

***Solution:***

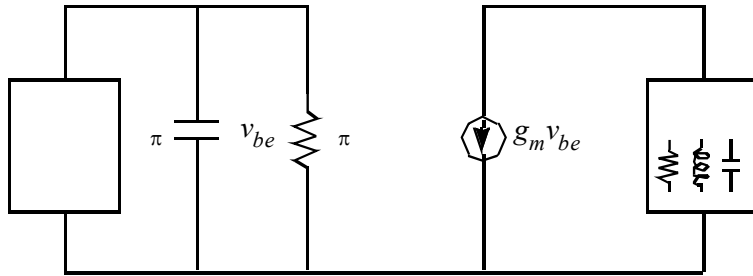
$$(a) \quad g_m = I_C \frac{q}{kT} = \frac{1 \text{ mA}}{26 \text{ mV}} = 38.5 \text{ mS} \quad (\text{milli siemens})$$

$$(b) \quad r_\pi = \beta_F / g_m = 90 / 38.5 \text{ mS} = 2.34 \text{ k}\Omega$$

$$(c) \quad C_\pi = \tau_F g_m = 5 \text{ ps} \times 38.5 \text{ mS} \approx 0.19 \text{ pF} = 190 \text{ fF} \quad (\text{femto farad})$$



## 8.9 Cutoff Frequency



$$\beta =$$

$$f_T = \frac{g_m}{\pi (\tau_F + C_{dBE} / g_m)} = \frac{q I_C}{\pi (\tau_F + C_{dBE} / g_m)}$$

$$\beta \equiv \frac{i_c}{i_b} \quad f$$

$$v_{be} = \frac{i_b}{\frac{1}{r_\pi} + j\omega C_\pi} = \frac{i_b}{r_\pi + j\omega C_\pi}$$

$$C_\pi = \tau_F g_m + C_{dBE}$$

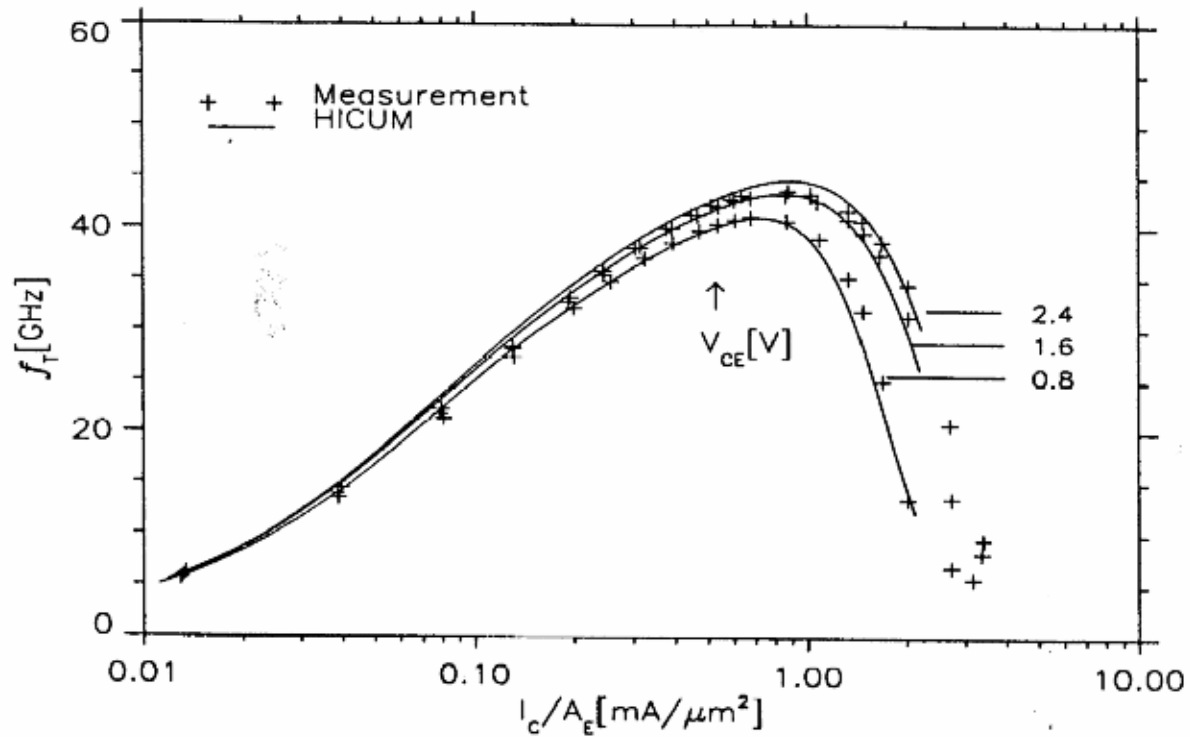
$$i_c = g_m v_{be}$$

$$\beta \omega = \left| \frac{i_c}{i_b} \right| = \left| \frac{g_m}{r_\pi + j\omega C_\pi} \right| = \left| \frac{\beta_F}{1 + j\omega \tau_F + j\omega C_{dBE} / g_m} \right|$$



## 8.9 Cutoff Frequency

$$f_T \propto \frac{1}{\tau_F + C_{dBE} \frac{kT}{qI_C}}$$



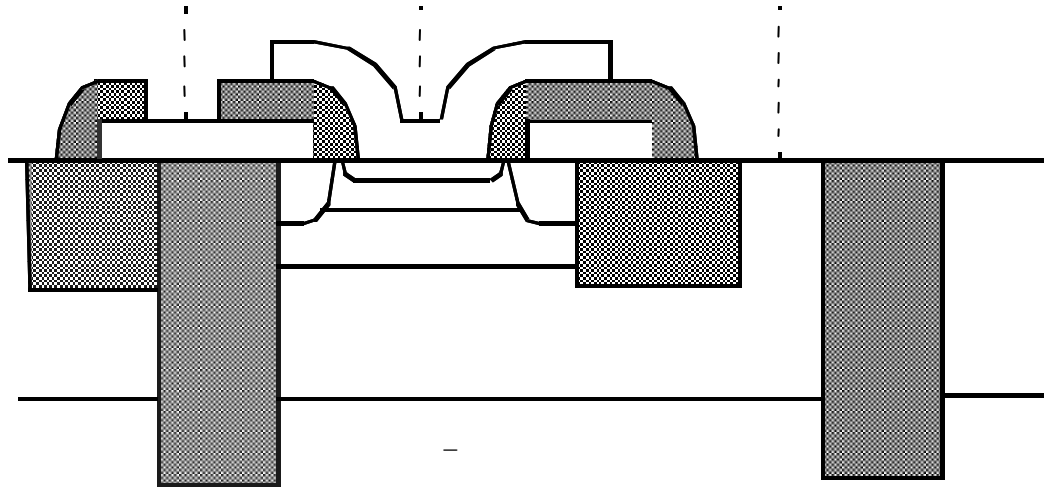
$f_T$

$f_T$   
 $f_T$

$I_C$

$I_C$

## *BJT Structure for Minimum Parasitics and High Speed*



**isolation**

## 8.10 Charge Control Model

$$I_B = I_C + \frac{Q_F}{\tau_F \beta_F}$$

$$I_B$$

$$I_B$$

$$Q_F + \tau_F \beta_F$$

$$\frac{dQ_F}{dt} = I_B - \frac{Q_F}{\tau_F \beta_F}$$

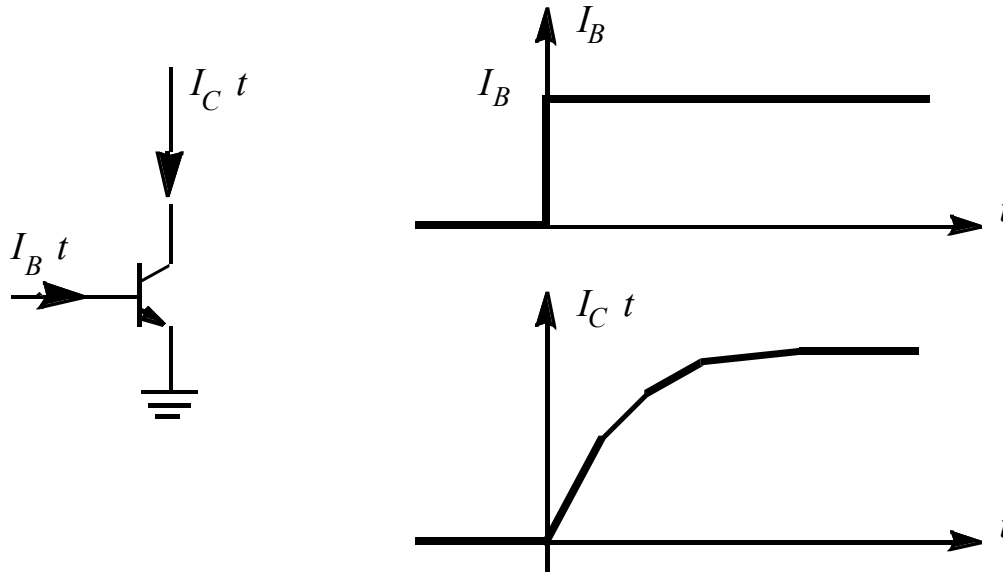
$$Q_F + \tau_F$$

$$I_B + \tau_F$$

$$I_C + \tau_F$$

$$I_C + \tau_F$$

**EXAMPLE : Find  $I_C(t)$  for a Step  $I_B(t)$**

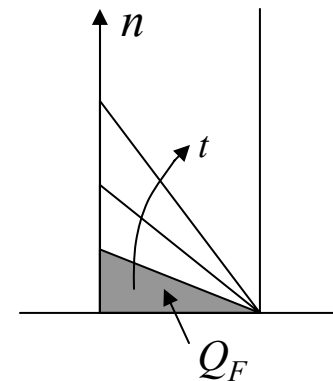


$$\frac{dQ_F}{dt} = I_B - \frac{Q_F}{\tau_F \beta_F}$$

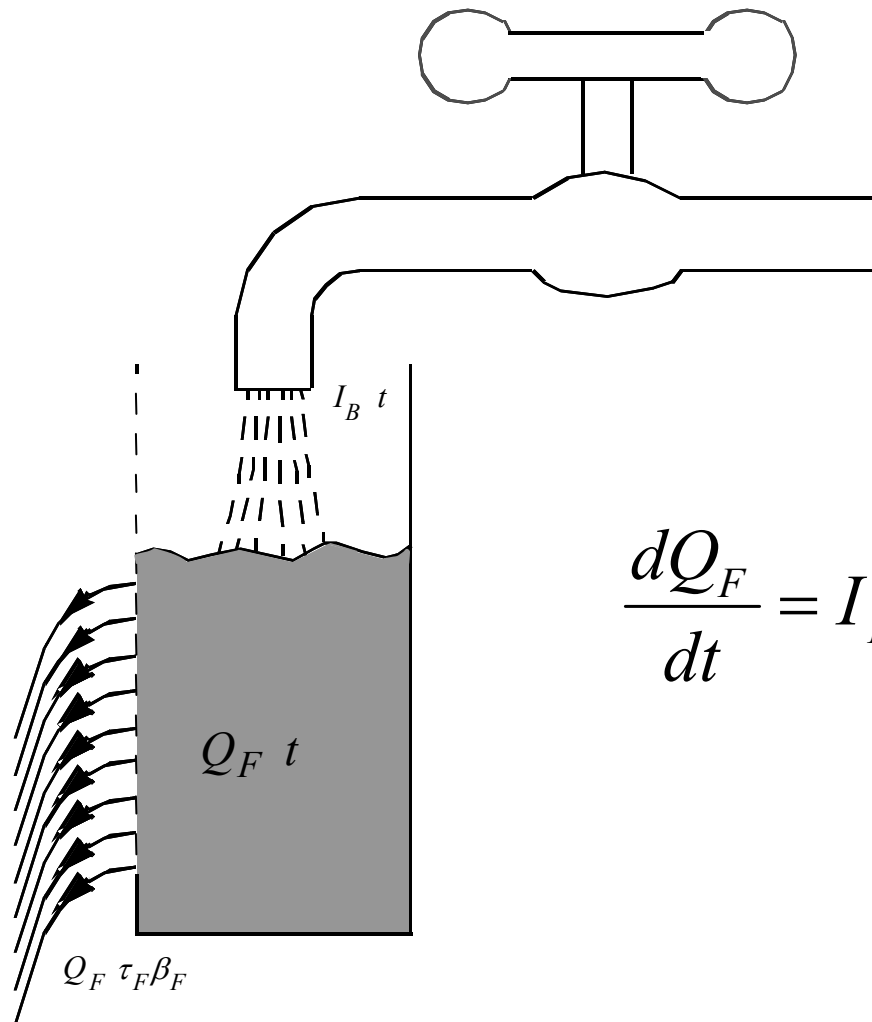
$$Q_F = \tau_F \beta_F I_B \left( 1 - e^{-t / (\tau_F \beta_F)} \right)$$

$$I_C(t) = Q_F(t) = \tau_F \beta_F I_B \left( 1 - e^{-t / (\tau_F \beta_F)} \right)$$

$$I_B \propto Q_F \quad Q_F \propto I_C$$

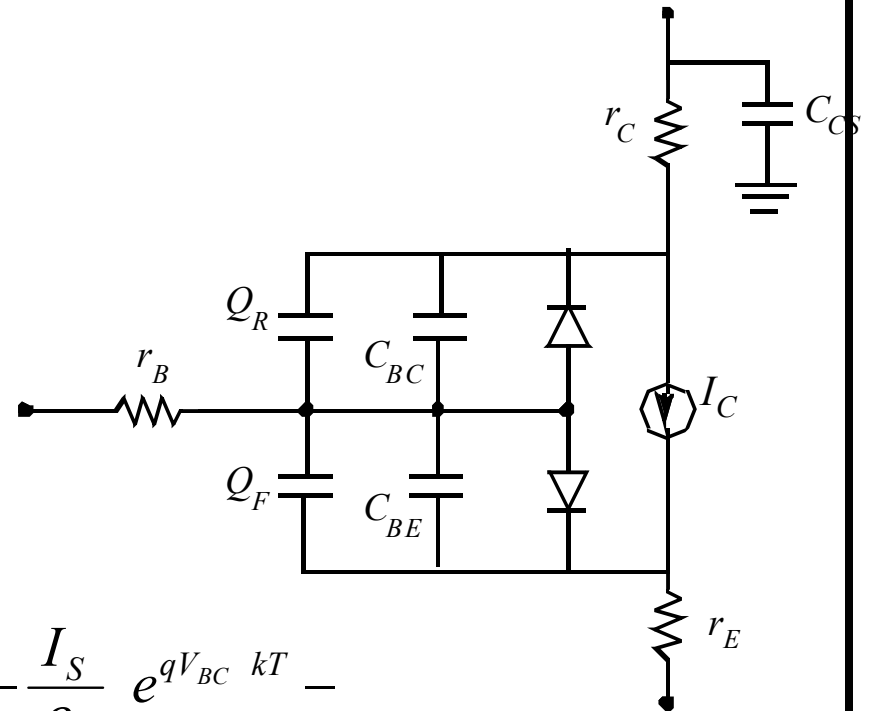


## *Visualization of $Q_F(t)$*



$$\frac{dQ_F}{dt} = I_B t - \frac{Q_F}{\tau_F \beta_F}$$

## 8.11 Model for Large-Signal Circuit Simulation



$$I_C = I_S' e^{qV_{BE}/kT} - e^{qV_{BC}/kT} \left( + \frac{V_{CB}}{V_A} \right) - \frac{I_S}{\beta_F} e^{qV_{BC}/kT} -$$

## ***8.11 Model for Large-Signal Circuit Simulation***

$I_C$

## 8.12 Chapter Summary

$I_C$

$V_{BE}$

$$I_C = A_E \frac{qn_i}{G_B} e^{qV_{BE}/kT} -$$

$$G_B \equiv \int_0^{W_B} \frac{n_i}{n_{iB}} \frac{p}{D_B} dx$$

$G_B$

$I_C$



## 8.12 Chapter Summary

$I_B$

$I_C$

$\beta_F$

$\alpha_F$

$$\beta_F = \frac{I_C}{I_B} \approx \frac{G_E}{G_B}$$

$$\alpha_F = \frac{I_C}{I_E} = \frac{\beta_F}{1 + \beta_F}$$

$\beta_F$

$I_C$

$I_C$

$V_{CB}$

$I_C$

$V_{CE}$

## 8.12 Chapter Summary

$$V_{BE}$$

$$Q_F$$

$$I_C$$

$$Q_F \equiv I_C \tau_F$$

$$\tau_F$$

$$\tau_F = \tau_{FB} = \frac{W_B}{D_B}$$

$$Q_F t$$

$$I_B t$$

$$I_C t$$

$$\frac{dQ_F}{dt} = I_B t - \frac{Q_F}{\tau_F \beta_F}$$

$$I_C t = Q_F t \quad \tau_F$$

## 8.12 Chapter Summary

$$g_m \equiv \frac{dI_C}{dV_{BE}} = I_C \frac{kT}{q}$$

$$C_\pi = \frac{dQ_F}{dV_{BE}} = \tau_F g_m$$

$$r_\pi = \frac{dV_{BE}}{dI_B} = \beta_F g_m$$