

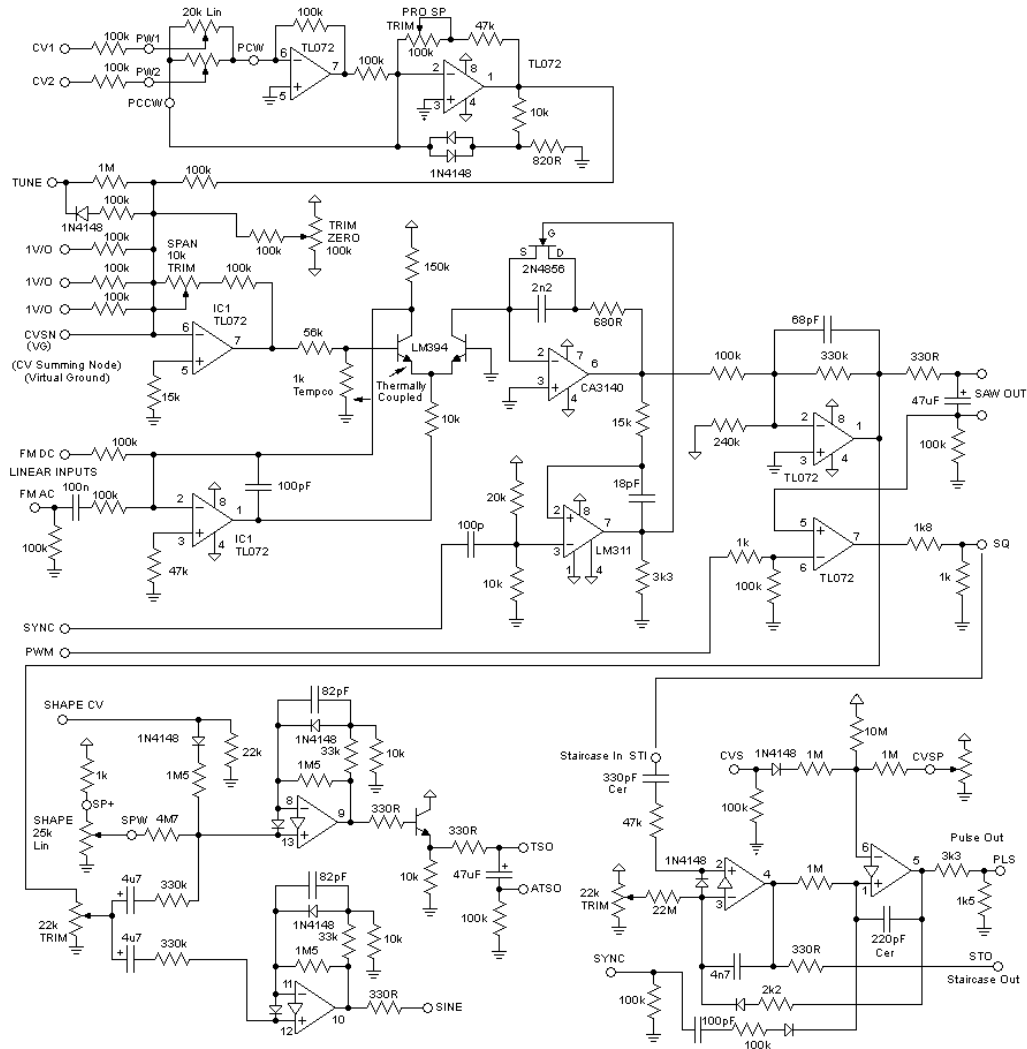
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Op Amps Are Everywhere

CTN

1

- Op amps are everywhere in practical circuits: (e.g., for solid-state guitar amplifiers, instrumentation, measurement tools, etc.)



- Op amps that can be used to build practical board-level circuits are often implemented via bipolar junction transistor technology

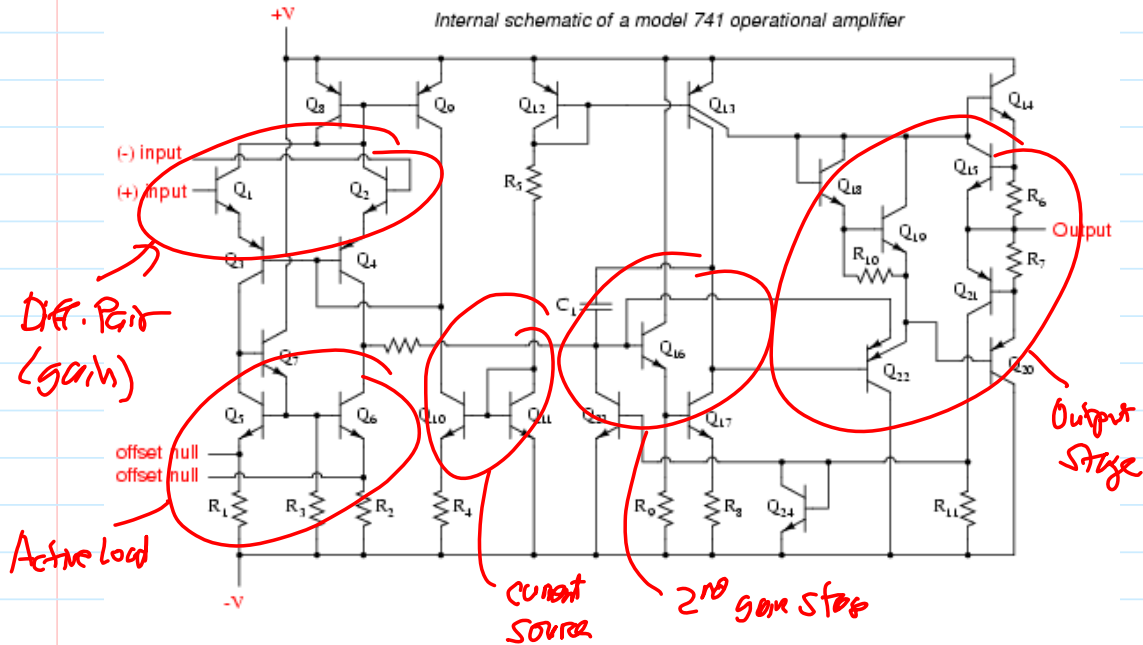
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Op Amps Are Everywhere

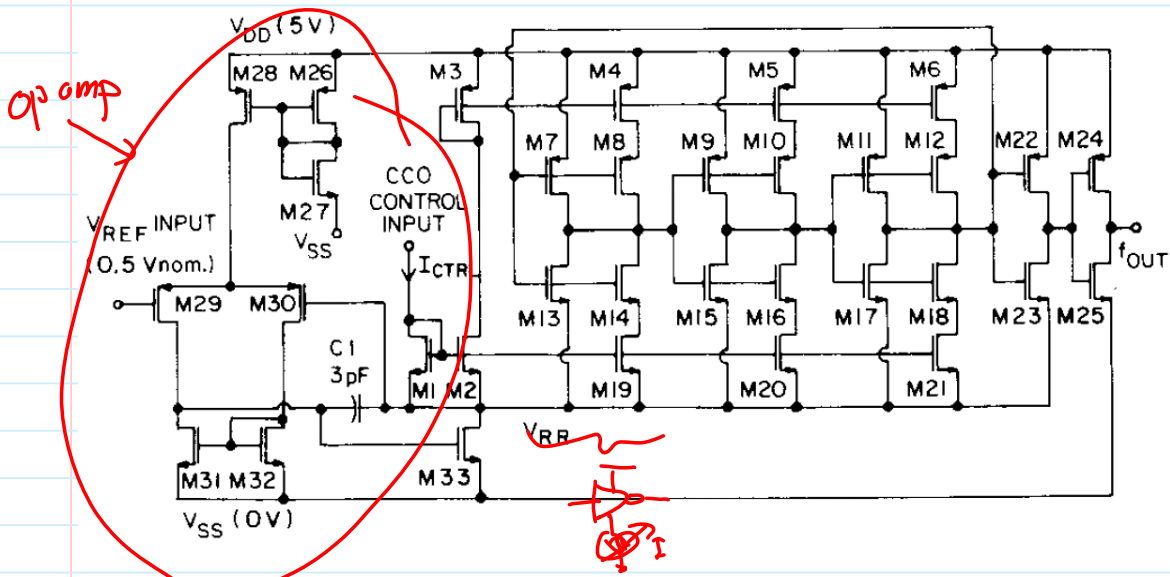
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2

- e.g., the 741 op amp, which has been a workhorse instrumentation op amp for decades



- Today, application specific integrated circuits (ASICs) for mixed analog/digital signal applications (e.g., A/D converters) utilize many op amps on the die level
 - ↳ such ASICs generally utilize CMOS op amps



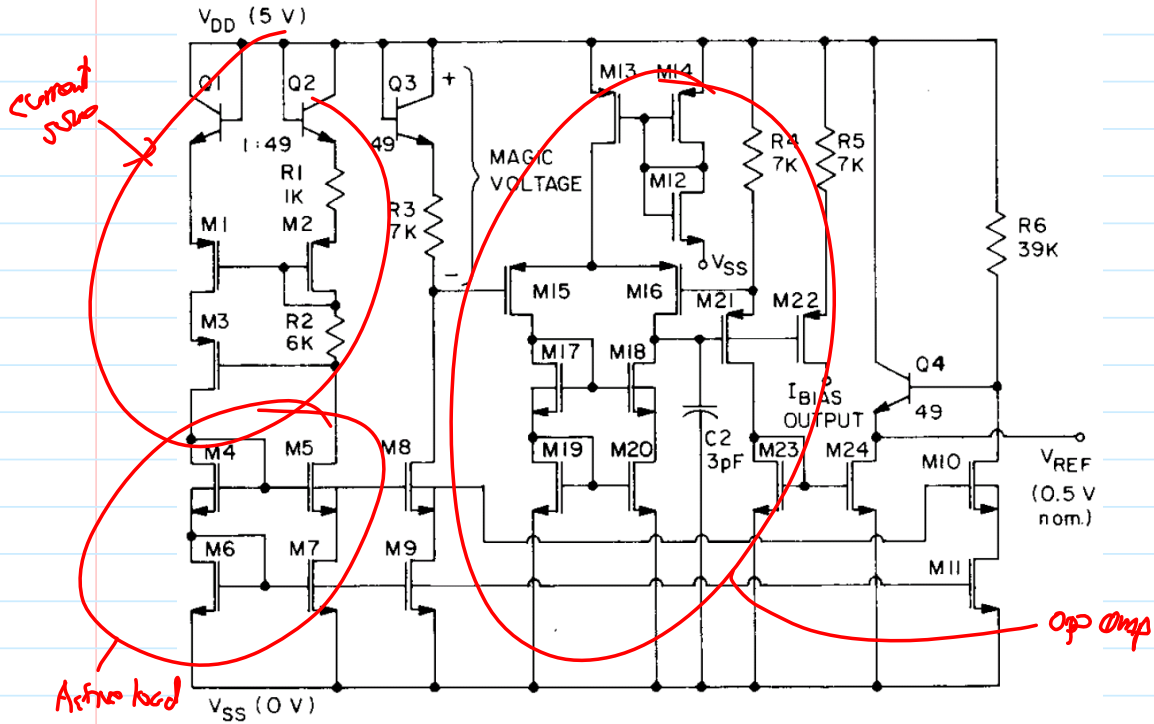
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Op Amps Are Everywhere

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3

• Below: bandgap reference using a CMOS op amp



- Again, this course will focus mainly on the innards of op amps
- Focus: CMOS, with some BJT coverage so you can work with practical board-level circuits, as well
- The first step towards analyzing and designing op amps is to understand the transistor technologies upon which they are based

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BJT Modeling

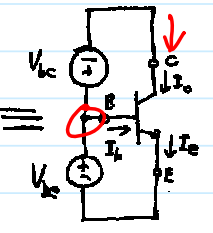
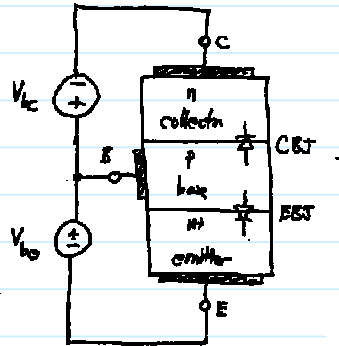
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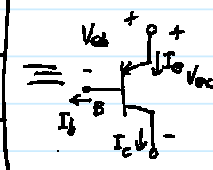
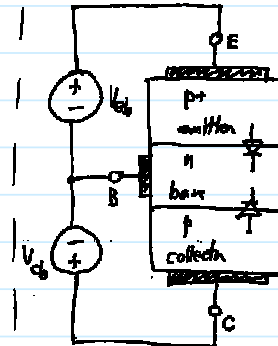
Modeling the Bipolar Junction Transistor (BJT)

→ physically, BJTs are just back-to-back pn junctions

npn bipolar Xistor



ppn bipolar Xistor



Regions of Bipolar Xistor Operation

EBJ

CBJ

Key: R = reverse-biased
F = forward-biased

R

R

Cut-off (both diodes off)

F

R

Forward Active (widely used in analog amplifier ckt)

R

F

Reverse Active

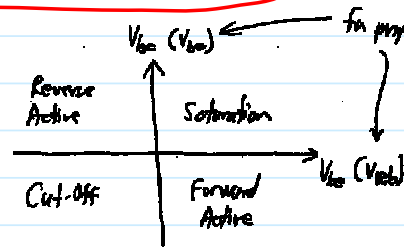
F

F

Saturation

⇒ can also think of this in a convenient graphical sense:

→ for npn (ppn):

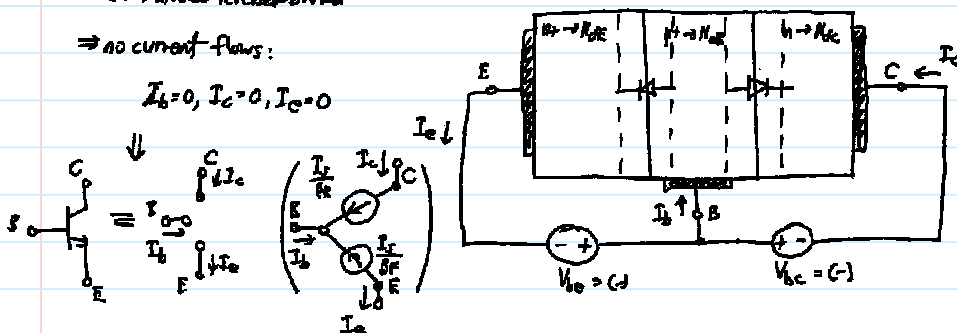


① Cut-off region - (npn transistor)

⇒ both diodes reverse-biased

⇒ no current flows:

$$I_B = 0, I_C = 0, I_E = 0$$



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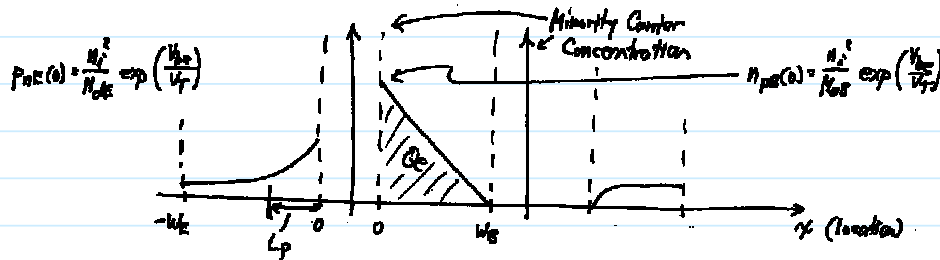
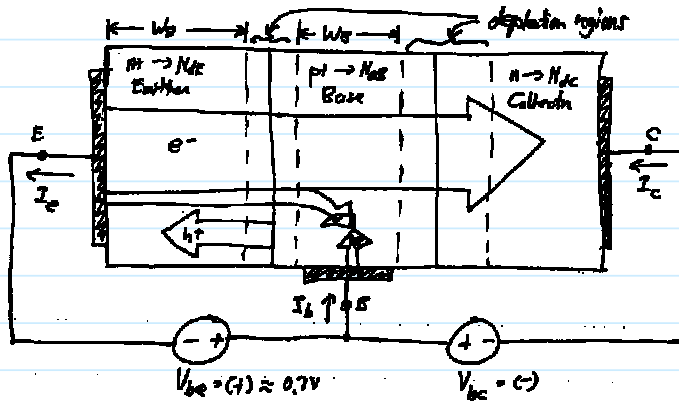
BJT Forward-Active

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② Forward-Active Region - (npn transistor)

⇒ BJT Forward-Biased (i.e., diode on), BJT Reverse-Biased (i.e., diode off)



Forward biasing of the BJT generates three current components:

- ① e⁻s injected from emitter to base: $I_{nE} = -A J_{nE}^{diff}$
 - ② h⁺s injected from base to emitter: $I_{pE} = A J_{pE}^{diff}$
 - ③ recombination of e⁻s & h⁺s in base: I_{rB}
- $I_C = I_{nE} = ①$
 $I_E = I_{nE} + I_{pE} + I_{rB} = ① + ② + ③$
 $I_B = I_{pE} + I_{rB} = ② + ③$

$$I_{nE} = -A J_{nE}^{diff} = -A q D_{nE} \frac{dn_p(x)}{dx} = -q A D_{nE} \frac{[n_{pE}(w_B) - n_{pE}(0)]}{w_B} = q A D_{nE} \frac{n_i^2}{N_B w_B} \exp\left(\frac{V_{BE}}{V_T}\right) = ① *$$

diffusion constant for e⁻s in E slope
 diffusion constant for h⁺s in E

$n_{pE}(w_B) = \frac{n_i^2}{N_B} \exp\left(\frac{V_{BC}}{V_T}\right) \approx 0$
 $n_{pE}(0) = \frac{n_i^2}{N_B} \exp\left(\frac{V_{BE}}{V_T}\right)$

$I_C = I_{nE} \exp\left(\frac{V_{BC}}{V_T}\right)$

$$I_{pE} = A J_{pE}^{diff} = A q D_{pE} \frac{dp_n(x)}{dx} = q A D_{pE} \frac{[p_{nE}(0) - p_{nE}(w_B)]}{w_E} = q A D_{pE} \frac{n_i^2}{N_E w_E} \exp\left(\frac{V_{BE}}{V_T}\right) = ② *$$

slope

$p_{nE}(0) = \frac{n_i^2}{N_E} \exp\left(\frac{V_{BE}}{V_T}\right)$
 $p_{nE}(w_B) \approx 0$

could also replace by diffusion length, L_p (for h⁺ in n-type material)