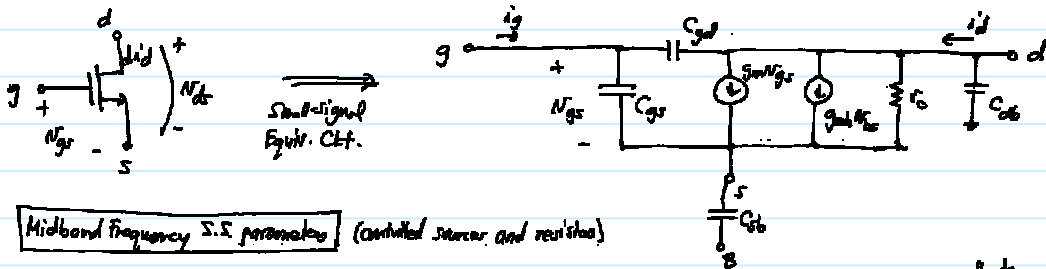


EE 140 MOS Small-Signal Model CTN 18

MOS Small-Signal Model (for NMOS) in saturation



Midband Frequency S.S. parameters (omitted sources and resistors)

Transconductance, gm:

$$g_m = \frac{\partial i_d}{\partial v_{gs}} = \frac{\partial I_D}{\partial v_{gs}} \Big|_{\text{opt}} = \frac{\partial}{\partial v_{gs}} \left(\frac{1}{2} \mu_n C_{ox} \frac{W}{L} (v_{gs} - v_{th})^2 \right) \Big|_{\text{opt}} = \mu_n C_{ox} \frac{W}{L} (v_{gs} - v_{th}) \Big|_{v_{gs} = v_{gs, \text{opt}}}$$

$$g_m = \mu_n C_{ox} \frac{W}{L} (v_{gs} - v_{th}) = \sqrt{2 \mu_n C_{ox} \frac{W}{L} I_D}$$

$$g_{mb} = \frac{\partial i_d}{\partial v_{bs}} = - \frac{\partial I_D}{\partial v_{bs}} = - \left(\frac{\partial I_D}{\partial v_{th}} \cdot \frac{\partial v_{th}}{\partial v_{bs}} \right) \Big|_{\text{opt}}$$

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (v_{gs} - v_{th})^2 \rightarrow (v_{gs} - v_{th}) = \sqrt{\frac{2 I_D}{\mu_n C_{ox} \frac{W}{L}}}$$

$$\frac{\partial I_D}{\partial v_{th}} \Big|_{\text{opt}} = - \frac{\partial I_D}{\partial v_{gs}} = -g_m \quad ; \quad \frac{\partial v_{th}}{\partial v_{bs}} \Big|_{\text{opt}} = \frac{\partial}{\partial v_{bs}} \left[v_{th} + \gamma \left(\sqrt{v_{bs} + 2\phi_f} - \sqrt{2\phi_f} \right) \right] = \frac{\gamma}{2\sqrt{v_{bs} + 2\phi_f}} = \eta$$

$$g_{mb} = \eta g_m$$

Note: $v_{bs} \uparrow \rightarrow v_{th} \uparrow \rightarrow \eta \downarrow \rightarrow I_D \downarrow$
often neglected! g_{mb} is minimized by maximizing γ !

Output Resistance, r_o : ($= \frac{1}{g_{ds}}$)

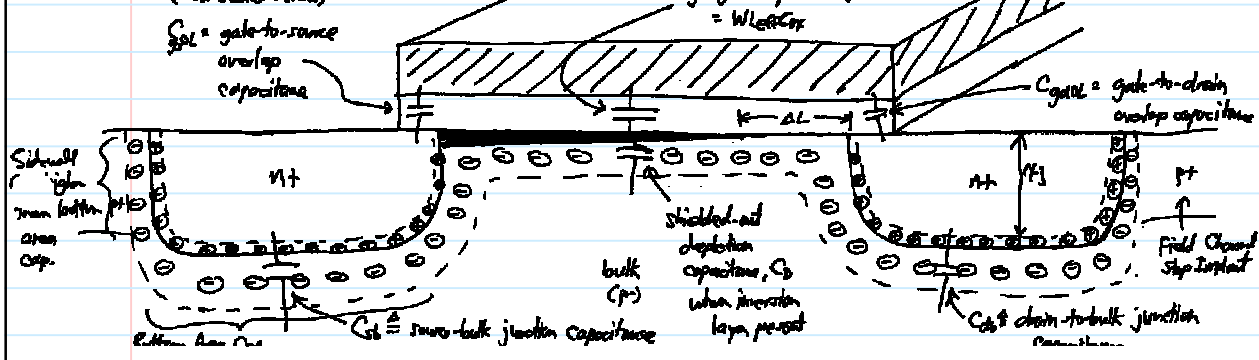
$$\Rightarrow \text{output conductance } g_{ds} = \frac{\partial i_d}{\partial v_{ds}} = \frac{\partial I_D}{\partial v_{ds}} \Big|_{\text{opt}} = \frac{\partial}{\partial v_{ds}} \left(\frac{1}{2} \mu_n C_{ox} \frac{W}{L} (v_{gs} - v_{th})^2 (1 + \lambda v_{ds}) \right) \Big|_{\text{opt}}$$

$$= \lambda I_{D, \text{sat}} = \frac{\lambda I_D}{1 + \lambda v_{ds}} \approx \lambda I_D = g_{ds}$$

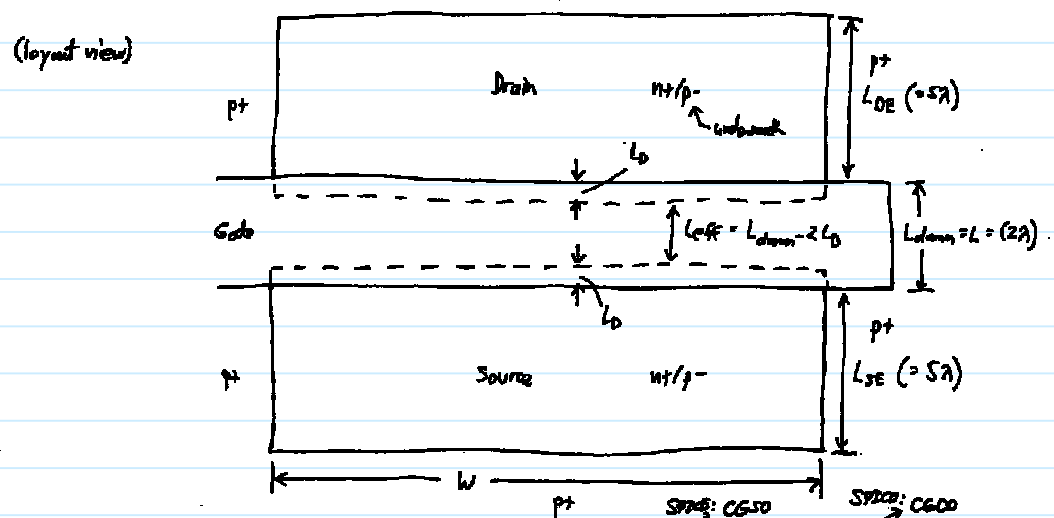
if v_{ds} is very large

$$r_o = g_{ds}^{-1} = \frac{1}{\lambda I_D} = \frac{1}{\lambda} \frac{v_{ds}}{I_D}$$

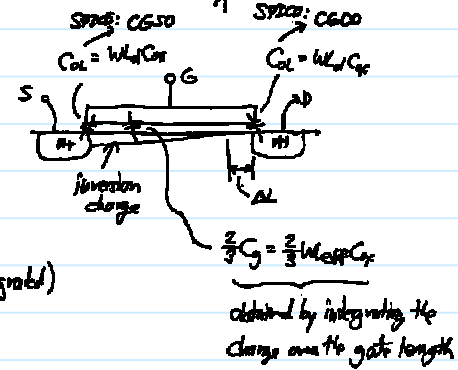
High Frequency S.S. Parameters (capacitors)



EE 140 MOS High Frequency SS Parameters CTN 19



(still considering saturation region)
In saturation, the inversion charge is not present near the drain:



Gate-to-Source Capacitor, C_{gs} :

$$C_{gs} = C_G \rightarrow \frac{2}{3}WLCCox \quad (\text{inversion charge integrated})$$

Gate-to-Drain Capacitor, C_{gd} :

$$C_{gd} = C_G \quad (\text{no inversion charge near the drain in saturation})$$

Source/Drain Junction Capacitance, C_{sb} & C_{db} : (must include these in SPICE simulations)

- ⇒ there are depletion capacitance associated with the drain-to-bulk and source-to-bulk pn junctions
- ⇒ bottom-side capacitance per unit area is different from that at sidewalls due to higher doping at the sidewalls (there is higher doping in the field areas to prevent channels from forming under interconnect wires)

⇒ take drain capacitance as an example:

$$C_{db} = \frac{C_{db0}}{\sqrt{1 + \frac{V_{DS}}{V_0}}}, \quad C_{db0} \triangleq \text{depletion capacitance with } V_{DS} = 0V$$

SPICE: CS

$$C_{j0} = \sqrt{\frac{q\epsilon_s N_A N_D}{216\pi}} \rightarrow \left(\frac{q\epsilon_s N_A N_D}{216\pi}\right)^{1/2}$$

depl. cap. per unit area @ bottom-side w/ $V_{DS} = 0V$

bulk doping level

