

Single pole response

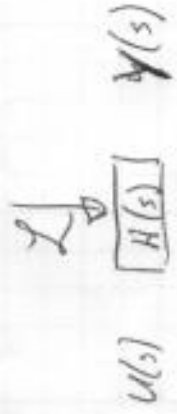
very common effect at $s_n, f_n, \tau_n, \omega_n$

poles & zeros, ODEs

time domain simulation, settling time

CS amp design

Poles, Zeros?



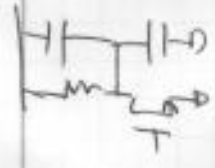
circuit designers are lazy, and use some small signal variables for time and freq.

$$y(t) + a \frac{dy}{dt} = u(t)$$

$$Y + a s Y = U$$

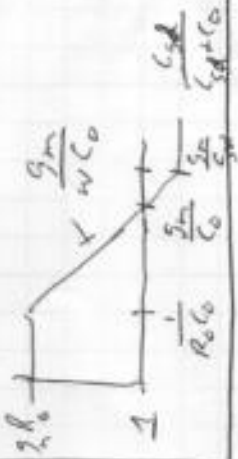
$$H(s) = \frac{Y}{U} = \frac{1}{1 + as} = \frac{1}{1 + s/\omega_p} \quad \omega_p = \frac{1}{a}$$

Last time



is more if driving w/ voltage source (why?)

distortion
smaller parasitic input current source load active load



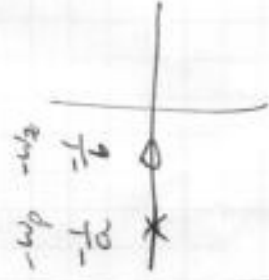
$$y(t) + a \frac{dy}{dt} = u(t) + b \frac{du}{dt}$$

$$(1 + as)Y = (1 + bs)U$$

$$H(s) = \frac{Y}{U} = \frac{1 + bs}{1 + as} = \frac{1 + s/\omega_z}{1 + s/\omega_p}$$

$$\omega_z = \frac{1}{b}$$

$$\omega_p = \frac{1}{a}$$



a zero means ≥ 2 paths from the input to the output



complex plane

poles & zeros

140/240A

19 FA W4L1

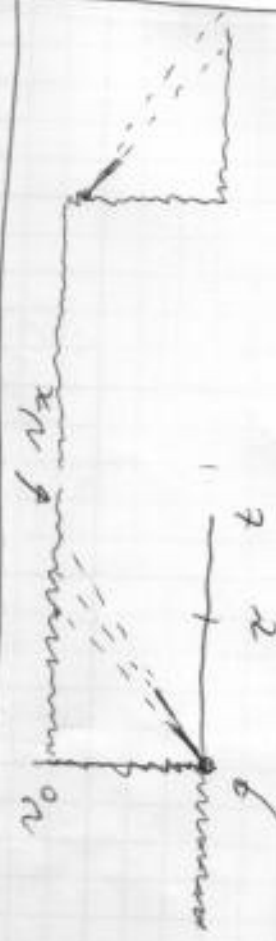
time domain

$$A \sin(\omega t) \rightarrow [H(s)] \rightarrow |H(j\omega)| A \sin(\omega t + \angle H(j\omega))$$

$$\sum A_i \sin(\omega_i t + \phi_i) \rightarrow [H(s)] \rightarrow \sum |H(j\omega_i)| A_i \sin(\omega_i t + \phi_i + \angle H(j\omega_i))$$

So knowing $|H(j\omega)|$ and $\angle H(j\omega)$ is important

⇒ Bode Plot



$$\frac{dv_x}{dt} = \frac{v_x - v_0}{\tau} = \frac{v_x}{\tau}$$

$$v_x (1 - e^{-t/\tau})$$

$$\text{error} = v_x e^{-t/\tau}$$

Step response v_x



theorem



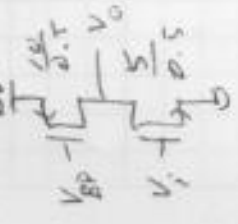
$$v_x \rightarrow v_0 \quad \frac{dv_0}{dt} = \frac{v_i}{C_0} \rightarrow \frac{v_x - v_0}{R C_0}$$

$$i = \frac{v_x - v_0}{R} \quad \frac{dv_0}{dt} = \frac{v_x - v_0}{\tau}$$

settling time $-t/\tau$

t	error = e
τ	$e^{-1} = 37\%$
2τ	$\frac{1}{e^2} = 14\%$
3τ	5%
4τ	1%
5τ	0.1%
6τ	0.01%
14τ	1 ppm

CS amplifier



$$V_D = 0.6V$$

$$V_{GS} = V_{GS} = 0.5V$$

$$I_{DQ} = \left(\frac{100\mu A}{V^2}\right)(60)(0.5)^2(1 + \lambda V_{DS}) = 100\mu A \left(1 + \frac{V_{DS}}{10V}\right)$$

what if $V_D = 0.82V$

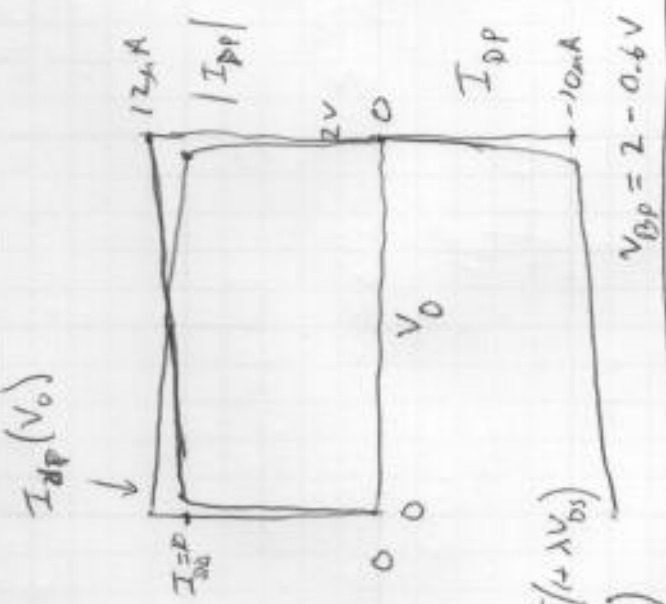
$$I_D = \left(\frac{200\mu A}{V^2}\right)(60)(0.5)^2(1 + \lambda V_{DS}) = 100\mu A$$

$$g_m = \frac{2I_D}{V_{GS}} = \frac{200\mu A}{0.5V} = 600\mu A/V$$

$$r_o = \frac{1}{\lambda I_D} = \frac{10V}{100\mu A} = 100k\Omega$$

$$R_D = 50k\Omega$$

$$A_v = g_m R_D = 30$$



$$V_{DD} = 2 - 0.6V$$

$$V_{OV} = 0.32V$$

$$V_{OV}^2 = 0.1V^2$$

$$V_{GT} = 2 - 0.82V = 1.18$$

find $g_m, R_D, (V_{O, min}, V_{O, max}) = \text{output swing}$.

$$A_v = \frac{2I_D}{V_{OV}} = \frac{2(100\mu A)}{0.1V} = 200\mu A/V$$

$$r_o = \frac{1}{\lambda I_D} = \frac{10V}{100\mu A} = 100k\Omega$$

$$R_D = \frac{1}{2} r_o = 50k\Omega$$

$$A_v = (200\mu A/V)(50k\Omega) = 100$$

$$v_i = 10mV \Rightarrow i_d = (200\mu A/V)(10mV) = 2\mu A, V_O < 0.1V$$

$$v_i = -10mV \Rightarrow i_d = -2\mu A, V_O > 1.9V$$

output swing $\approx (0.1, 1.9V)$

what if $V_D = 0.5V$? $V_{OV} \approx 0 < 10mV$

Sub- V_T Say equal at 10mV Say $n=2$

$$I_D \approx \frac{10mV}{V_T} \left(\frac{10}{V_T}\right)^2 = 0.1\mu A$$

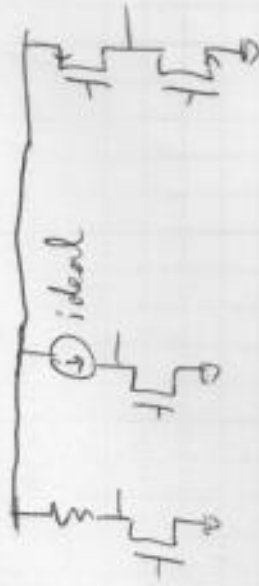
$$I_D \approx 0.05\mu A \approx 0.05\mu A$$

$$r_o = \frac{1}{\lambda I_D} = \frac{10V}{0.05\mu A} = 200k\Omega$$

$$g_m = \frac{I_D}{nV_T} = \frac{80\mu A}{50mV} = 1.6 \times 10^{-6} S$$

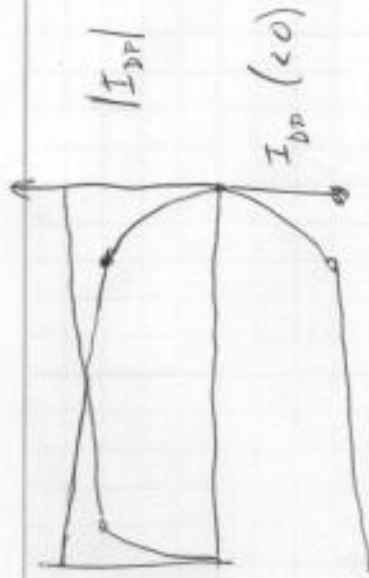
$$A_v \approx 169 = 80 A_v = \frac{I_D}{nV_T} \frac{1}{\lambda I_D} = \frac{V_A}{nV_T} = \frac{10V}{4V_T} = \frac{10V}{50mV}$$

Back to circuits



$R_L \ll \infty, A_v \approx g_m r_o$

$R_L \gg r_o, A_v \approx g_m R_L$



$r_{in} = r_{oq} \quad R_o = \frac{r_{oq}}{2} \quad A_v = \frac{g_m r_o}{2}$

active load usually gives better gain than resistive load (when $|A_v| > V_{DD}$)