

2 stage

Miller comp.
RHP zero
mirror doublet

Common mode gain

stewing

add $C_c \rightarrow$

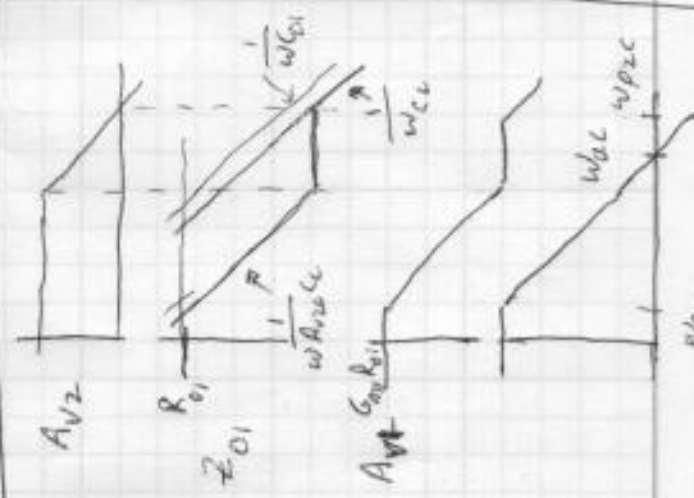
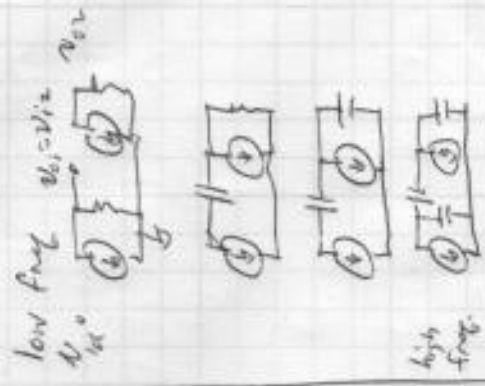
$$\omega_{p1} = \frac{1}{R_{o1}C_{o1}}$$

$$\omega_{p2} = \frac{1}{R_{o2}C_{o2}}$$

$$\omega_{pic} \approx \frac{1}{G_m R_{o1} R_{o2} C_c}$$

$$\omega_{pzc} = ?$$

$$\omega_{uc} = ?$$



$$\omega_{pzc} = \frac{G_{m2}}{C_1 + C_2 + \frac{C_1 C_2}{C_c}}$$

$$\approx \frac{G_{m2}}{C_1 + C_2}$$

iff $C_c \gg C_1$
or $C_c \gg C_2$

$$\omega_{uc} = \omega_{pic} (A_{v10} A_{v20})$$

$$= \frac{G_{m1} R_{o1} G_{m2} R_{o2}}{G_{m2} R_{o2} R_{o1} C_c}$$

$$= \frac{G_{m1}}{C_c}$$

for $PM > 45^\circ$ need $\omega_{uc} < \omega_{pzc}$
in unity gain

$$\frac{G_{m1}}{C_c} < \frac{G_{m2}}{C_1 + C_2 + \frac{C_1 C_2}{C_c}} \approx \frac{G_{m2}}{C_1 + C_2}$$

Rough sizes of C_c :

- 1) Extra calc how much poles need to split (\neq low freq gain)
- 2) make $C_c = C_c$ need $G_{m1} R_{o1} C_c \approx \sqrt{\text{split } C_{o1}}$

Other frequency (phase) trouble

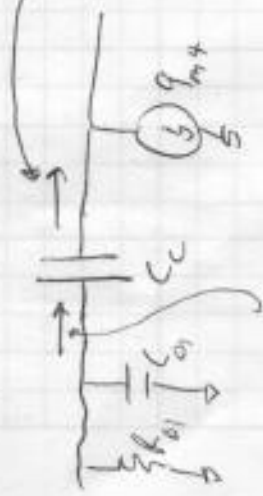
C_c gives RHP zero



G_m calc: $i_o = g_{m4} N_{o1} + s C_c (v_{o2} - v_{o1})$
 $= (g_{m4} - s C_c) N_{o1}$

$G_{m2} = \frac{s C_c}{\omega_{o1}} = g_{m4} (1 + s/\omega_z)$ $\omega_z = \frac{g_{m4}}{C_c}$

OR get rid of that feedforward current



want to get rid of this one to avoid RHP zero

Many options. On HW.

need thirone for Miller comp

if $I_{m4} = 10 I_{m1}$, not a problem

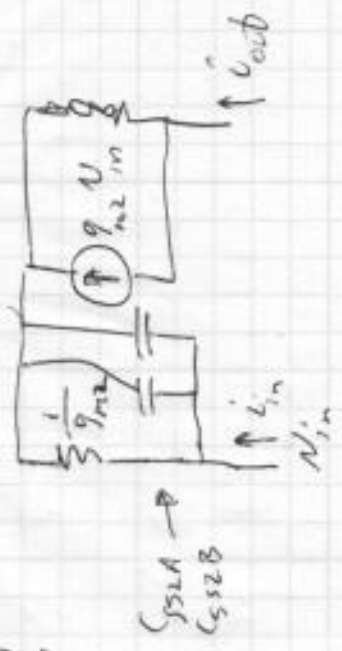
$\omega_{uc} = \frac{g_{m1}}{C_c}$ $\omega_z = \frac{g_{m4}}{C_c}$

$\Rightarrow \leq 60^\circ$ negative phase at unity gain
 or if $f \leq 0.1$, s_{m1} and $g_{m1} = s_{m4}$, something. otherwise, need to fix phase.

① $\frac{v_{out}}{v_{in}} \approx \frac{1}{R_2 C_c} \omega_z = \frac{1}{C_c (\frac{1}{g_{m4}} - R_2)}$

push zero to higher freq, \rightarrow infinity \rightarrow LHP!
 cancel a LHP pole?!

Mirror freq response



$i_{out} = g_{m2} v_{in}$

Max $i_{in} = v_{in} [g_{m2} + s(C_{S2A} + s(2C_{S2B}))] = v_{in} g_{m2} [1 + \frac{s}{\omega_{pm}}]$

$v_{in} = i_{in} \frac{1}{g_{m2} (1 + \frac{s}{\omega_{pm}})}$ $\omega_{pm} = \frac{g_{m2}}{2 C_{S2B}} = \frac{1}{2} \omega_T$

$$i_{out} = i_{n2} v_{in} = \frac{g_{m2} i_{in}}{g_{m2}} \left(\frac{1 + \frac{s}{\omega_{pm}}}{1 + \frac{s}{\omega_{pm}}} \right) = i_{in} \left(1 + \frac{s}{\omega_{pm}} \right)$$



$G_{m1} = g_{m1}$ at low freq.
 but at high freq $G_{m1} \approx \frac{g_{m1}}{2}$

$$-i_o = g_{m1A} \frac{v_{id}}{2} \left(1 + \frac{s}{\omega_{pm}} \right) + g_{m1B} \frac{v_{id}}{2}$$

$$A_{v1} = \frac{i_o}{i_{in}} = -\frac{g_{m1}}{2} \left(1 + \frac{s}{\omega_{pm}} \right) = -\frac{g_{m1}}{2} \left(1 + \frac{s}{2\omega_{pm}} \right)$$

$$G_{m1} = \frac{i_o}{v_{id}} = -\frac{g_{m1}}{2} \left[1 + \frac{1}{1 + \frac{s}{\omega_{pm}}} \right]$$

$$= -\frac{g_{m1}}{2} \left[\frac{2 + \frac{s}{\omega_{pm}}}{1 + \frac{s}{\omega_{pm}}} \right]$$

$$= -g_{m1} \left[\frac{1 + \frac{s}{2\omega_{pm}}}{1 + \frac{s}{\omega_{pm}}} \right]$$

$$\omega_{pm} = \frac{g_{m2}}{2 C_{gs}}$$

$$\omega_{zpm} = 2\omega_{pm} = \frac{g_{m2}}{C_s} = \omega_T$$

"Doublet"

Summary

uncompensated

$$\omega_{p1} = \frac{1}{R_{o1} C_{o1}}$$

$$\omega_{p2} = \frac{1}{R_{o2} C_{o2}}$$

$$\omega_{z1} = ?$$

$$\omega_z = \frac{g_{m4}}{C_c}$$

$$\omega_{pm} = \frac{g_{m2}}{2 C_{gs}}$$

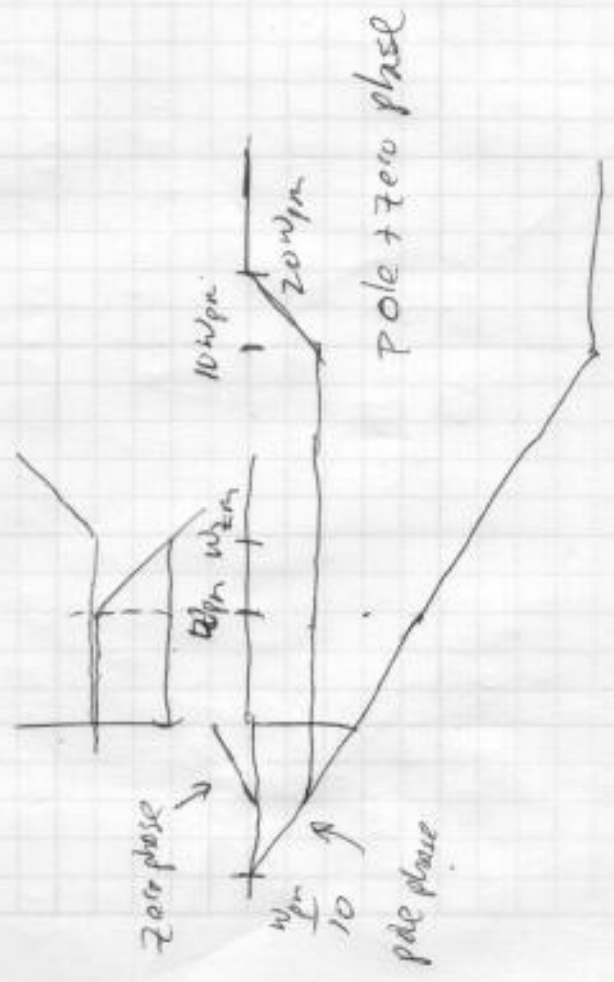
$$\omega_{zpm} = 2\omega_{pm}$$

compensated

$$\omega_{p1c} = \frac{1}{R_{o1} R_{o2} R_{o3} C_c}$$

$$\omega_{p2c} = \frac{g_{m4}}{C_1 + C_2 + \frac{C_{c1} C_2}{C_c}}$$

$$\omega_{zc} = \frac{g_{m4}}{C_c}$$



$$A_{v1} = -\frac{g_{m1}}{2} \left(1 + \frac{s}{2\omega_{pm}} \right)$$