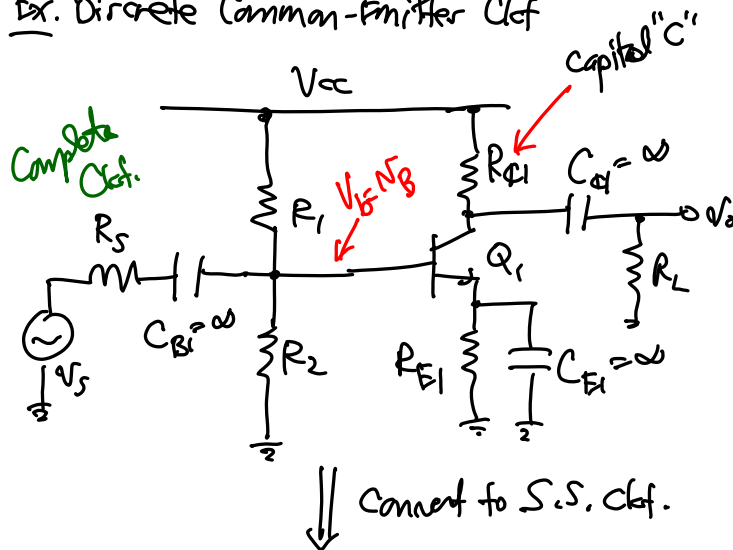


Lecture 4: Inspection Analysis

- Announcements:
- Course website has been up and running
 - ↳ Just point your browser to
<http://www-inst.eecs.berkeley.edu/~ee140/sp11/>
- I'm here today, but as your syllabus shows, will be traveling again next Tuesday, 2/1
 - ↳ Flying back next Tuesday, 2/1
 - ↳ Make-up lecture:
- -----
- Lecture Topics:
 - ↳ Procedure for Small Signal Analysis
 - ↳ Inspection Formulas
 - ↳ 1-Tx Amplifier Examples
- -----

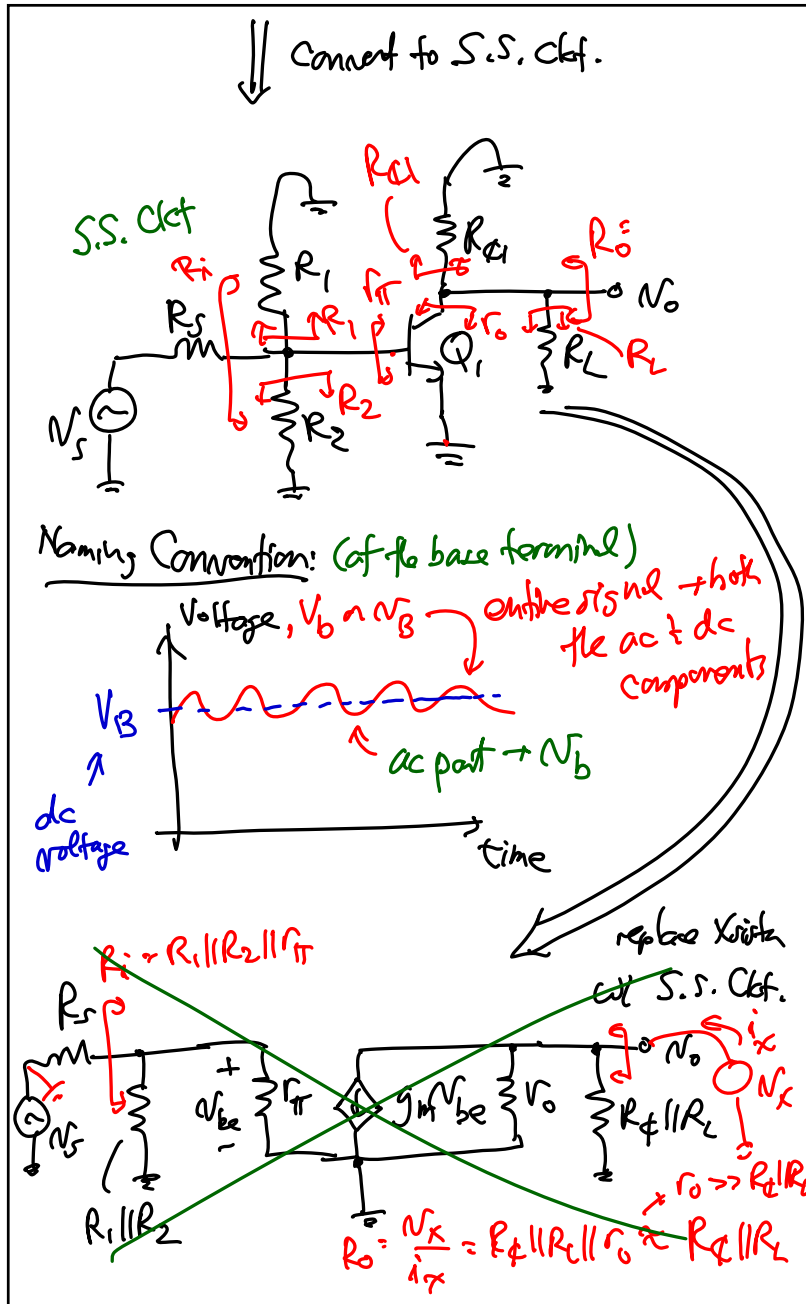
Procedure for Small-Signal Analysis

Ex. Discrete Common-Emitter Ckt



Procedure:

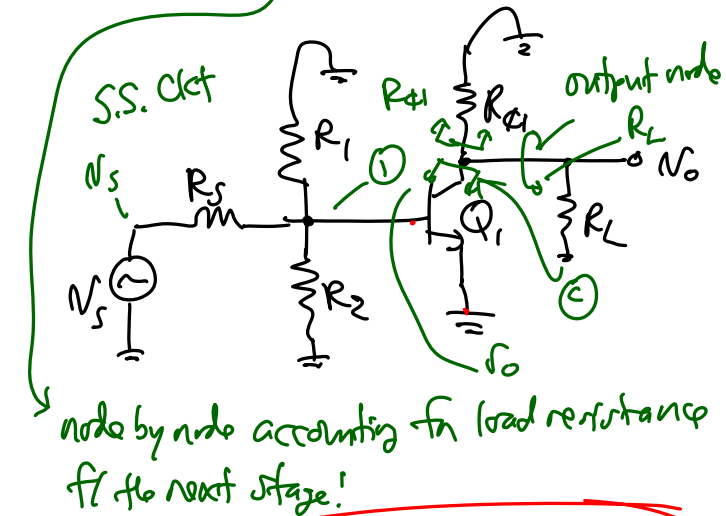
- ① Find the DC operating pt. → get the DC voltages & currents at all nodes & branches, respectively
 - ② Determine the small-signal (S.S.) parameter for devices in the signal path.
 - ③ Convert the full ckt. to the S.S. ckt.
 - ⇒ zero out the DC source
 - ⇒ short out large caps.
 - ④a If needed, replace the Xrista w/ its S.S. Ckt.
 - ⇒ this should not be NEEDED often!
 - ⇒ when is it needed? → generally, only in cases where there is feedback
 - ④b Analyze by inspection based on prior S.S. analysis experience!
- Go through Inspection Analysis handout
 - ↳ Best to commit the equations on this sheet to memory



$$R_i = R_1 \parallel R_2 \parallel r_{\pi}$$

$$R_o = R_{\pi} \parallel R_L \parallel r_o \approx R_{\pi} \parallel R_L$$

Get G_{oib1} (go node by node) $\rightarrow A_{v1}$



$$A_{v1} = \frac{V_{O1}}{V_S} \cdot \frac{V_O}{V_{O1}} = - \left(\frac{R_1 \parallel R_2 \parallel r_{\pi}}{R_1 \parallel R_2 \parallel r_{\pi} + R_S} \right) g_m (R_{\pi} \parallel R_L)$$

$$\frac{V_{O1}}{V_S} = \frac{R_1 \parallel R_2 \parallel r_{\pi}}{R_1 \parallel R_2 \parallel r_{\pi} + R_S}$$

$\frac{v_o}{v_i} = -G_m R_{\odot} = -g_m (R_{\odot} \parallel R_L \parallel r_o) \approx -g_m (R_{\odot} \parallel R_L)$
 $\uparrow \quad \uparrow$
 $\frac{g_m}{1 + g_m (0) R_E} = g_m$
 \uparrow
 R_E
 $R_{\odot} = R_L \parallel R_{\odot} \parallel r_o \approx R_L \parallel R_C$
 $@ 1 \text{mA} \approx 25 \Omega$

Ex. Common-Collector:

if $R_E \gg \frac{1}{g_m}$

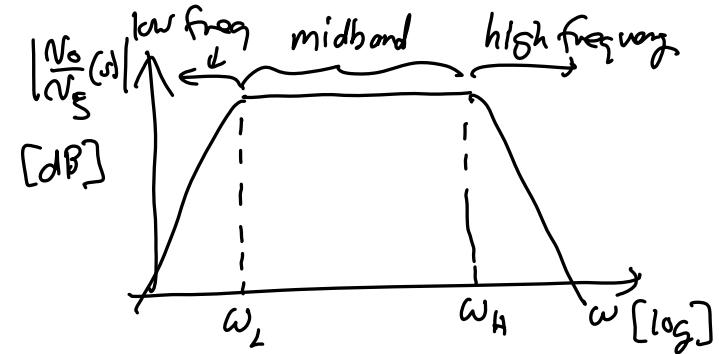
$R_o = \frac{1}{g_m} \parallel R_E \approx \frac{1}{g_m}$
 $\frac{v_o}{v_i} = \frac{R_E}{r_{\pi} + R_E} = \frac{(\beta + 1) R_E}{r_{\pi} + (\beta + 1) R_E}$
 $\uparrow \quad \uparrow$
 $\frac{1}{g_m} \rightarrow \frac{\beta}{g_m} = r_{\pi}$
 $R_i = r_{\pi} + (\beta + 1) R_E$
 \uparrow
 $(R_E \parallel r_o) \approx R_E$
 $R_o = r_o \parallel R_E \approx R_E$

Ex. Common-Base

$R_i = \frac{1}{g_m}$
 $\frac{v_o}{v_i} = g_m (r_o \parallel R_C) \approx g_m R_C$

⇒ so far, we've been talking about "midband" analysis

⇒ Bode Plot: (for the 1st amp we analyzed) C.E.



we want this!

use OCTC (open circ. time constant) analysis