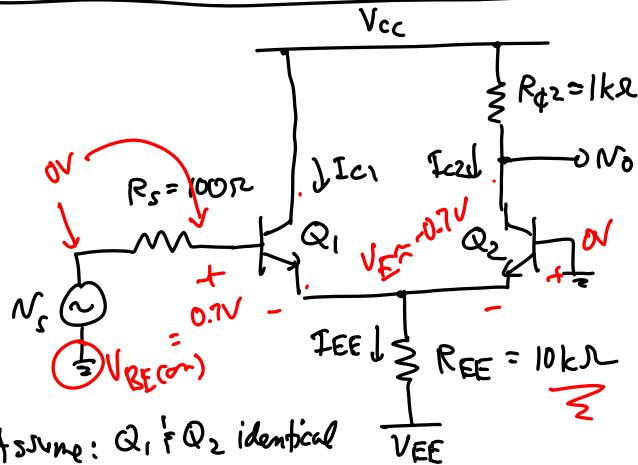


Lecture 5: MOS Inspection Analysis

- Announcements:
- Make-up lecture: Saturday, 2/5, 3:30-5 p.m., in 213 Wheeler (this room) → **no longer true! Watch email for update to time and place (if no email, then nothing over the weekend)**
- Lab#1 is online (and hardcopies were handed out in class today)
- HW#2 has been online since Tuesday and is due next Tuesday, at 5 p.m.
- Lecture Topics:
 - ↳ Multi-Tx Amplifier Examples
 - ↳ MOS Inspection Analysis

Inspection Analysis on a Multitransistor Ckt.



Assume: Q_1 & Q_2 identical

Do small-signal analysis to get: $R_i, R_o, A_v = \frac{V_o}{V_s}$

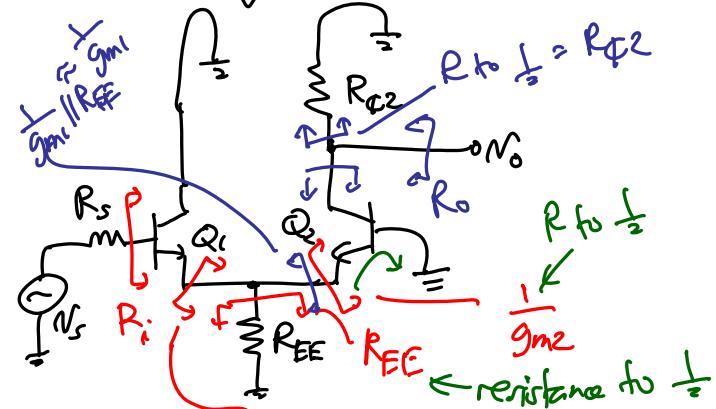
First: Get the DC operating pt.

$$I_D = I_{D1} = I_{D2} = \frac{I_{EE}}{2} \rightarrow \text{determine S.S. parameter}$$

$$\rightarrow r_{\pi 1} \approx r_{\pi 2} = r_{\pi} = \frac{\beta}{g_m}$$

$$r_{o1} = r_{o2} = r_o = \frac{V_A}{I_D} \quad g_{m1} \approx g_{m2} = g_m = \frac{I_D}{V_T}$$

Convert to AC def.



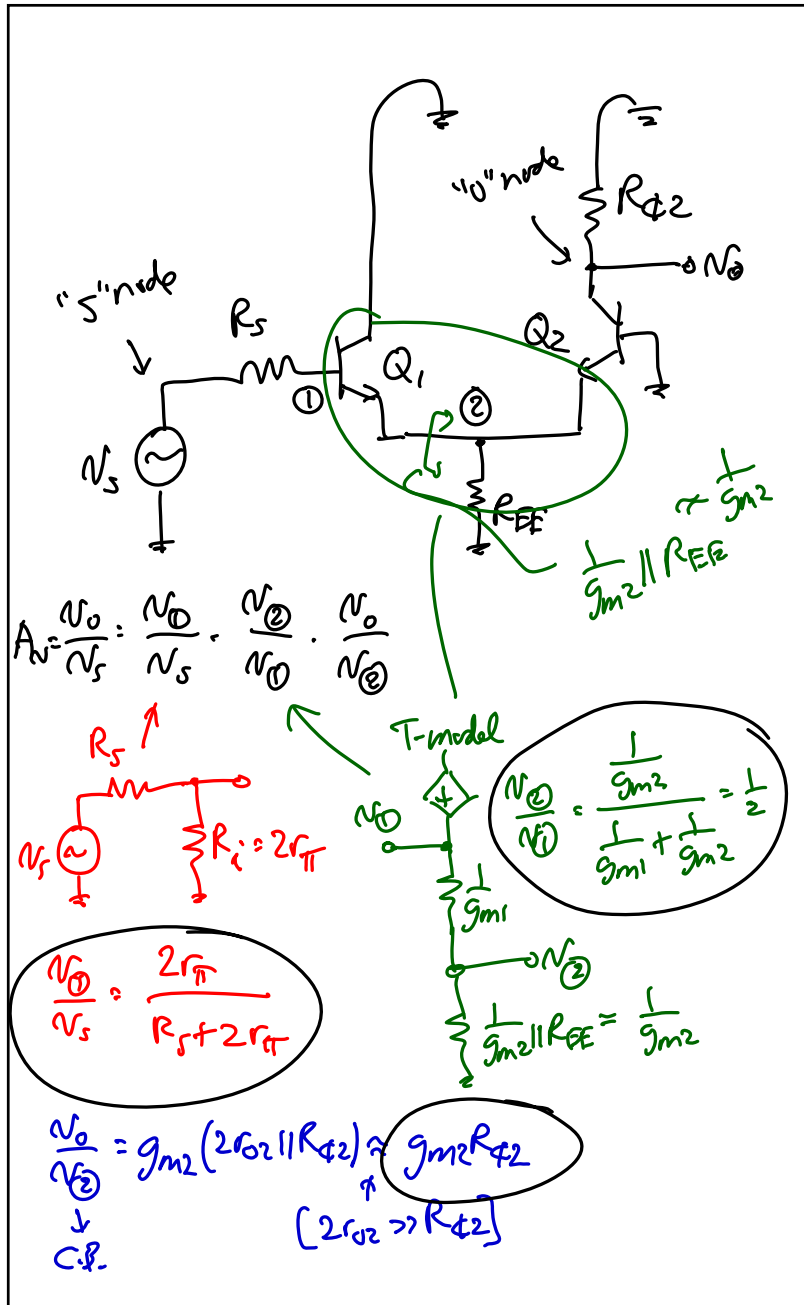
$$R_i = r_{\pi 1} + (\beta + 1)(?) = r_{\pi 1} + (\beta + 1) \frac{1}{g_{m2}} = 2r_{\pi} = R_i$$

$$\frac{1}{g_{m2}} \parallel R_{EE} \approx \frac{1}{g_{m2}} \quad r_{\pi 2} + \frac{R_s}{\beta + 1} \approx \frac{1}{g_{m1}}$$

$$R_o = R_{D2} \parallel r_{o2} \left(1 + \frac{g_{m2} \left(\frac{1}{g_{m1}} \right)}{1 + 0} \right) = (2r_{o2}) \parallel R_{D2}$$

$R_B = 0$

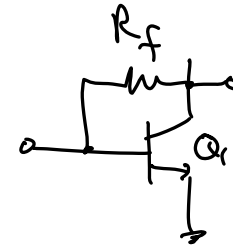
$[r_{o2} \gg R_{D2}]$
 $\approx R_{D2}$



$$A_v = \frac{V_o}{V_s} = \left(\frac{2r_{\pi}}{2r_{\pi} + R_s} \right) \left(\frac{1}{2} \right) g_{m2} R_{D2}$$

Inspection analysis doesn't always work!

Ex. Feedback, e.g.,



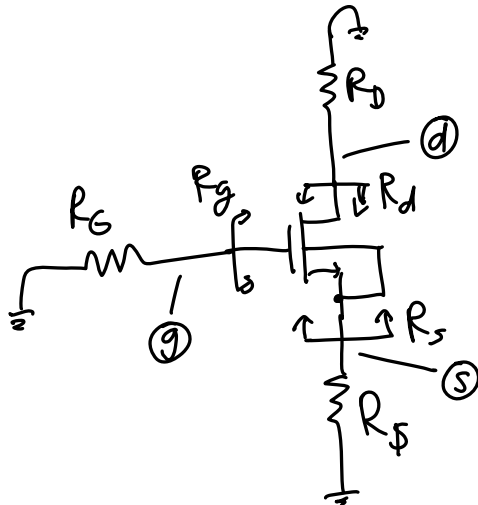
achieved when source tied to bulk

Mos Xsistor Clot!

⇒ for now, ignore Body effect (i.e., ignore g_{mb})

use same inspection formulas as bipolar,

but use $\beta \rightarrow \infty$, $r_{\pi} = \frac{\beta}{g_m} \rightarrow \infty$



⇒ referring to the "inspection formula sheet":

Bipolar

MOS

$$R_b = \left(\frac{1}{g_m} + R_E \right) (\beta + 1) \xrightarrow{\beta \rightarrow \infty} R_g = \infty$$

$$R_e = \frac{1}{g_m} + \frac{R_B}{\beta + 1} \xrightarrow{\beta \rightarrow \infty} R_s = \frac{1}{g_m}$$

$$R_c = r_o \left[1 + \frac{g_m R_E}{1 + R_B/r_{\pi}} \right] \xrightarrow{\beta \rightarrow \infty} R_d = r_o [1 + g_m R_s]$$

↑
∞

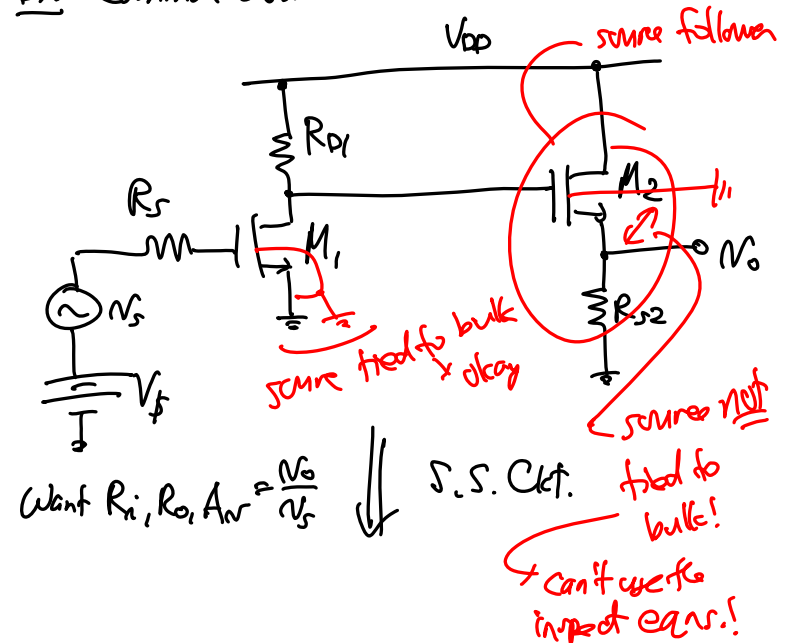
$$\frac{v_d}{v_g} = -G_m R_d, \quad G_m = \frac{g_m}{1 + g_m R_s}$$

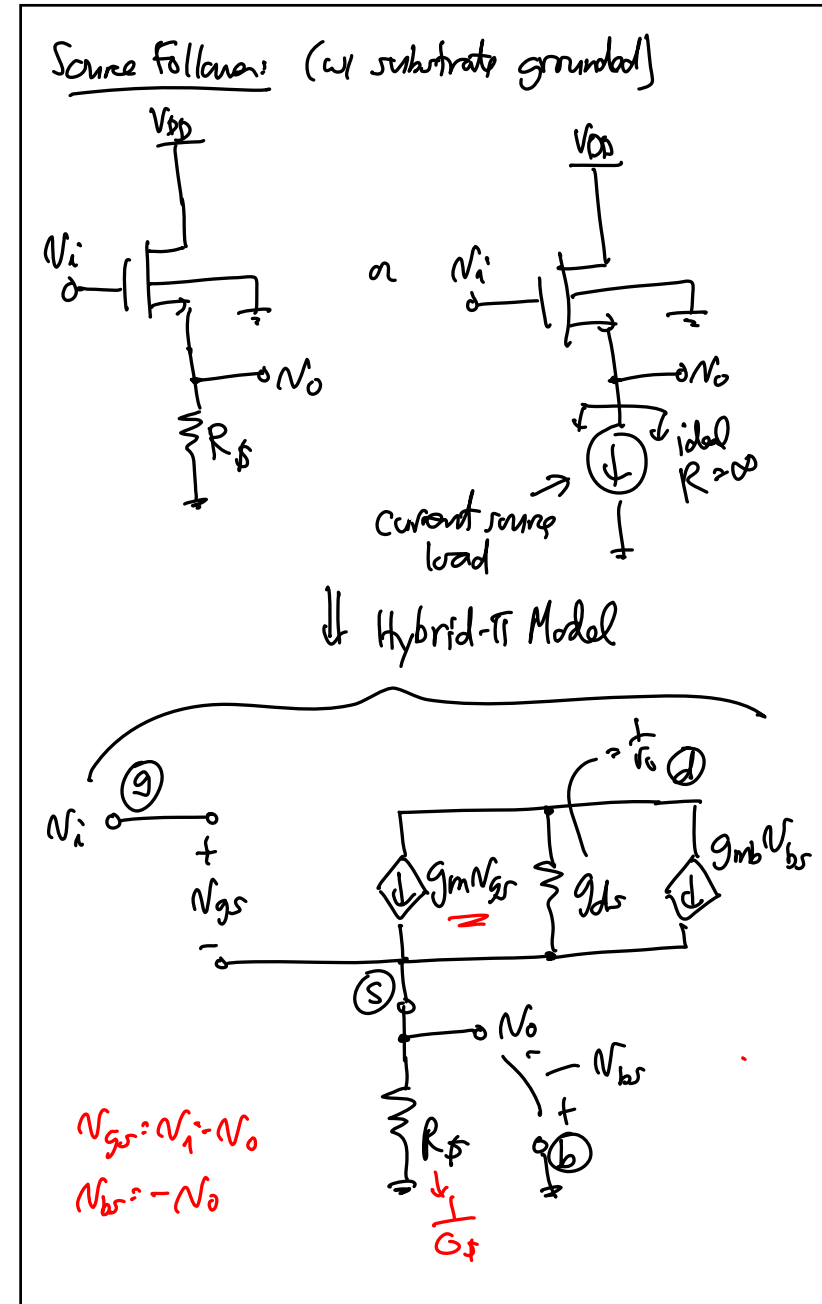
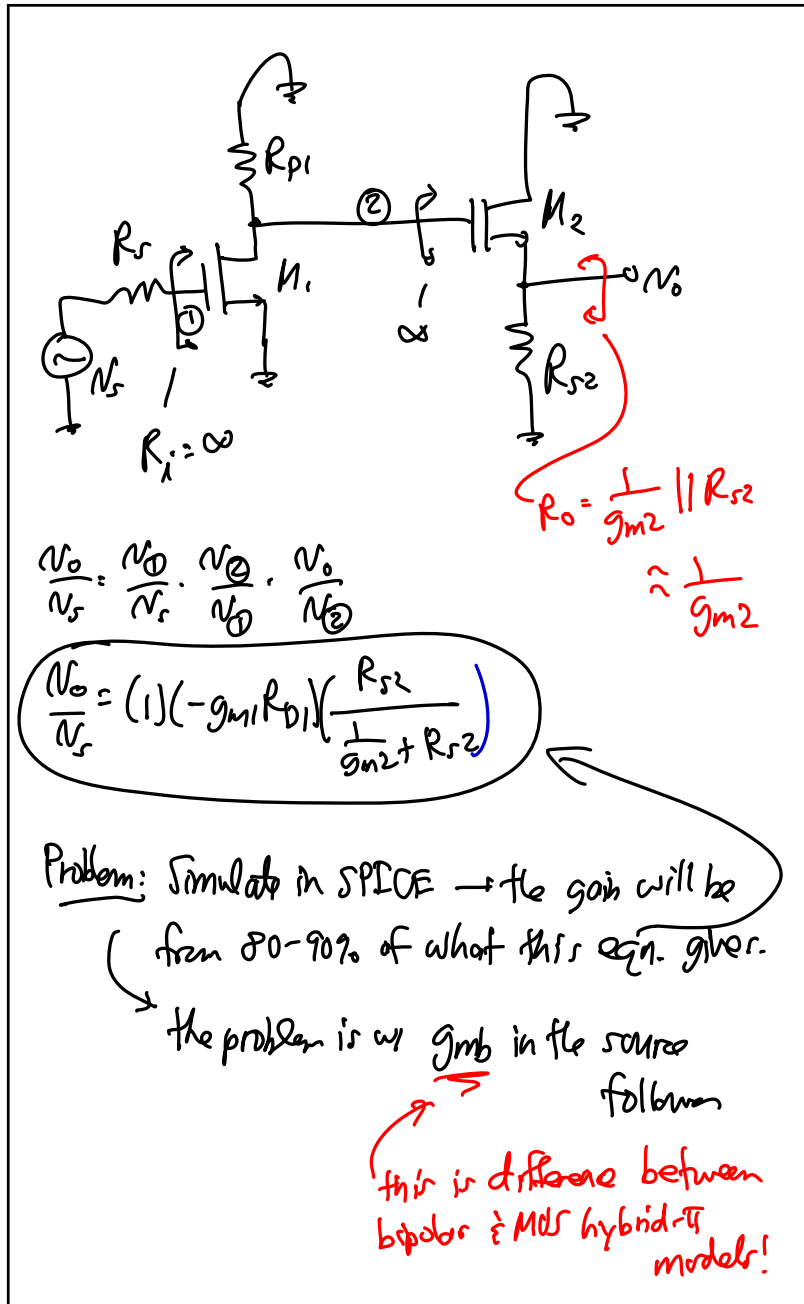
$$\frac{v_d}{v_s} = -G_m R_d, \quad G_m = -g_m$$

$$\frac{v_s}{v_g} = \frac{g_m R_s}{1 + g_m R_s} = \frac{R_s}{\frac{1}{g_m} + R_s}$$

MOS Inspection Analysis

Ex Common-Source Common-Drain Cascode





Apply KCL:

$$g_m(N_i - N_o) = N_o(g_{mb} + g_{dr} + G_s)$$

$$\Rightarrow A_v = \frac{N_o}{N_i} = \frac{g_m}{g_m + g_{mb} + g_{dr} + G_s}$$

$$\left[R_s \rightarrow \infty \rightarrow G_s \rightarrow 0 \right]$$

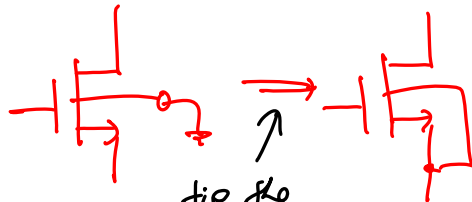
$$g_{dr} \ll g_m + g_{mb}$$

Body factor

$$A_v \approx \frac{g_m}{g_m + g_{mb}} = \frac{1}{1 + \eta}, \quad \eta = \frac{\gamma}{2\sqrt{V_{SB} + 2\phi_f}}$$

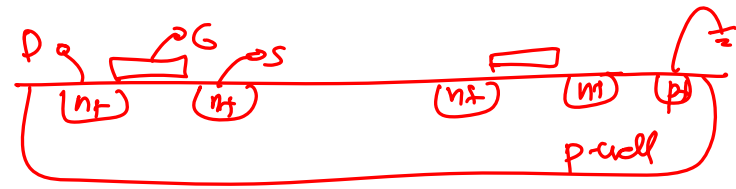
$\neq 1$ even when $R_s \rightarrow \infty$.

To eliminate g_{mb} , do this:

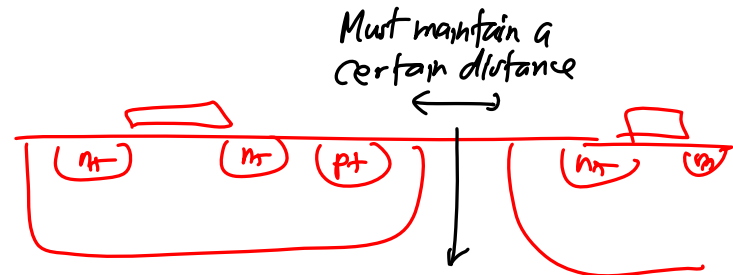


tie the bulk to the source \rightarrow Unfortunately, can't do this all the time:

\Rightarrow usually, have many MOS devices sharing a single well:

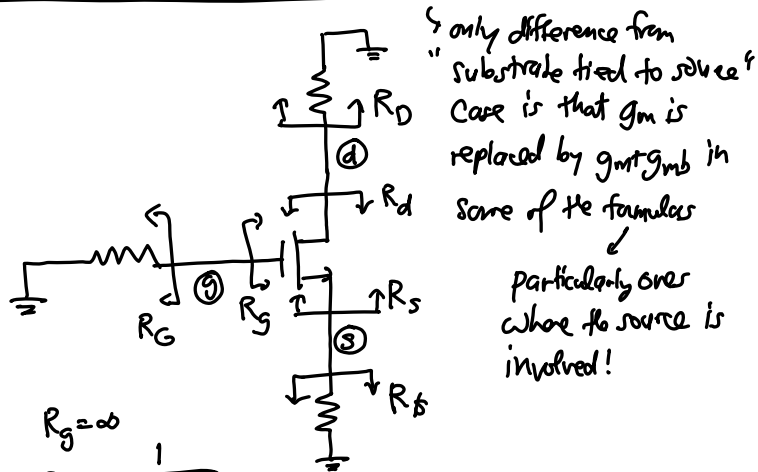


\Rightarrow to tie bulk to source for a given device, the device would require its own well:



Lot more area!
(and this is not good for cost!)

MOS Inspection Formulas w/ Substrate Grounded



$$R_g = \infty$$

$$R_s = \frac{1}{g_m + g_{mb}}$$

$$R_d = r_o [1 + (g_m + g_{mb}) R_s]$$

$$\frac{N_d}{N_g} = -G_m R_d, \quad G_m = \frac{g_m}{1 + (g_m + g_{mb}) R_s}$$

$$\frac{N_d}{N_s} = -G_m R_d, \quad G_m = -(g_m + g_{mb})$$

$$\frac{N_s}{N_0} = \frac{g_m R_s}{1 + (g_m + g_{mb}) R_s}$$

Remark When the substrate is tied to the source, $g_{mb} = 0$.