

# Lecture 8: Active Loads

## Announcements:

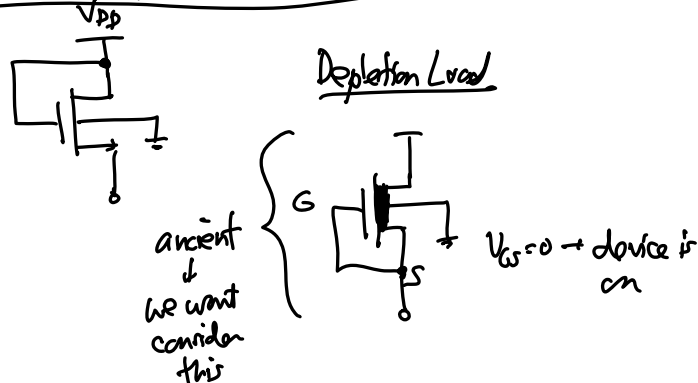
- No Prof. Nguyen Office Hours this coming Monday (on travel)
- But there WILL BE lecture Tuesday

## Lecture Topics:

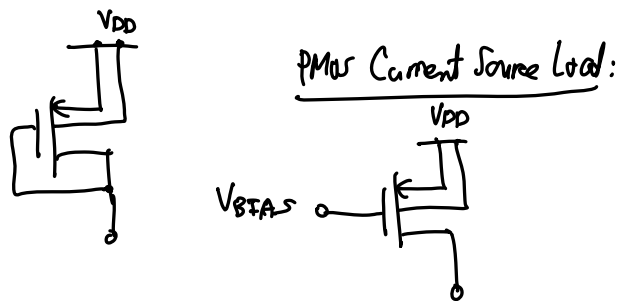
- Types of Active (Transistor) Loads
- Analysis of actively loaded circuits
- Current Sources

## Last Time:

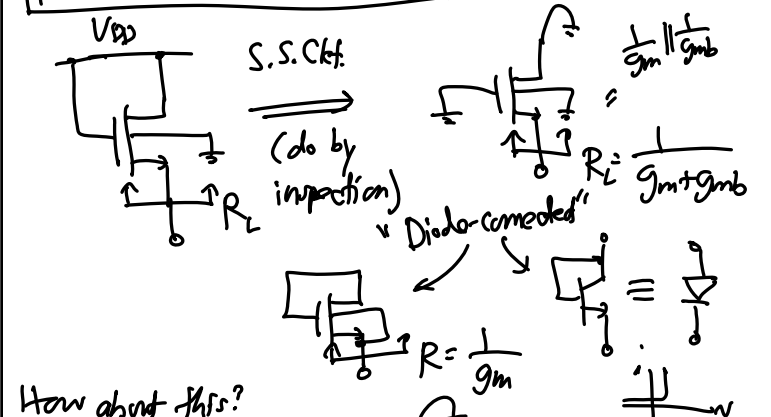
### Diode-Connected Enhancement Load



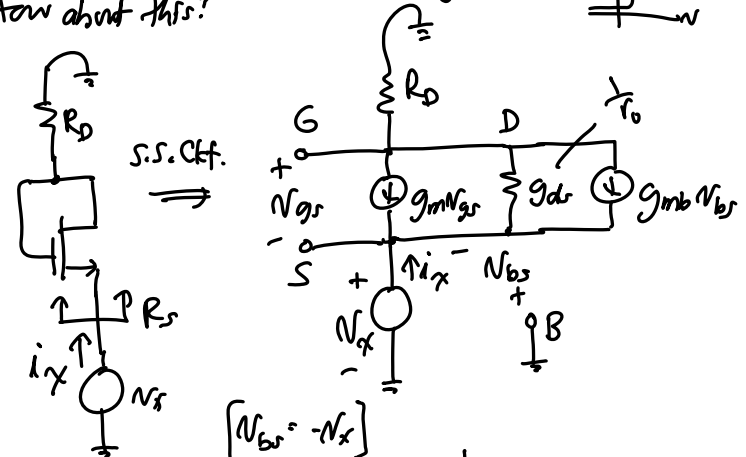
### Diode-Connected PMOS Load:



### Diode-Connected Enhancement Load



How about this?



$$i_x = -g_m V_{gs} + g_{ds} (-V_{gs}) - g_{mb} V_{bs} \quad \eta = \frac{g_{mb}}{g_m}$$

$$= g_m (V_x - i_x R_D) + g_{mb} V_x$$

$$R_D = \frac{V_x}{i_x} = \frac{1 + g_m R_D}{g_m + g_{mb}} = \frac{1}{g_m + g_{mb}} + \frac{R_D}{1 + \eta}$$

$$R_D \approx \frac{1}{g_m + g_{mb}}$$

... and from the top:

S.S. Ckt.

do the analysis

$$R_d = \frac{v_x}{i_x} = \frac{1}{g_m} + (1+\eta)R_S \approx \frac{1}{g_m} + R_S$$

Thus:

from top      from bottom

Apply to C.S. Ckt.

Active Load

Driver

negl.

$$A_v = \frac{v_O}{v_i} = - \frac{g_{m1}}{g_{m2} + g_{mb2}}$$

$$= - \frac{1}{(\eta+1)} \frac{g_{m1}}{g_{m2}}$$

$$A_v = - \frac{1}{\eta+1} \sqrt{\frac{\mu_n C_{ox} (\frac{W}{L})_1}{\mu_p C_{ox} (\frac{W}{L})_2}} \frac{V_{DD}}{V_{DD}} = - \frac{1}{\eta+1} \sqrt{\frac{(W/L)_1}{(W/L)_2}} = A_v$$

Diode-Connected PMOS Load

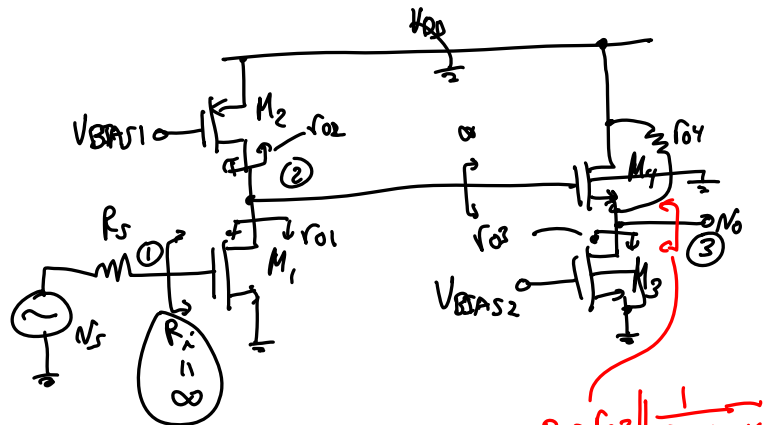
$$A_v = - \frac{g_{m1}}{g_{m2}} = - \sqrt{\frac{\mu_n (W/L)_1}{\mu_p (W/L)_2}}$$

PMOS Current Source Load

$$A_v = \frac{v_O}{v_i} = - \frac{g_{m1}}{g_{ds1} + g_{ds2}} = - g_{m1} (r_{o1} || r_{o2})$$

$\Rightarrow$  gain is huge! ( $r_o$  is huge)  
 $\Rightarrow$  but requires  $V_{bias}$

Ex. Multi-Stage Actively-Loaded MOS Ckt.



$$a_v = \frac{v_0}{v_s} = \frac{v_1}{v_s} \cdot \frac{v_2}{v_1} \cdot \frac{v_3}{v_2}$$

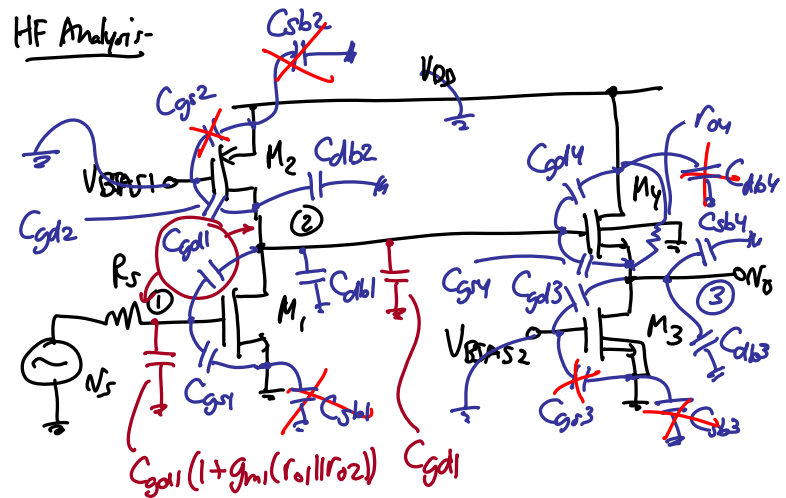
$$= (1)(-g_{m1}(r_{o1} || r_{o2}))$$

$$a_v = -g_{m1}(r_{o1} || r_{o2}) \left( \frac{g_{m4}}{g_{m4} + g_{mb4}} \right)$$

$R_o = r_{o3} || \frac{1}{g_{m4} + g_{mb4}}$   
 $R_o \approx \frac{1}{g_{m4} + g_{mb4}}$

$\frac{g_{m4}(r_{o3} || r_{o4})}{1 + (g_{m4} + g_{mb4})R_o}$   
 $\frac{g_{m4}R_o}{1 + (g_{m4} + g_{mb4})R_o}$

HF Analysis



$$\tau_1 = [C_{gs1} + C_{gd1}(1 + g_{m1}(r_{o1} || r_{o2}))]R_s$$

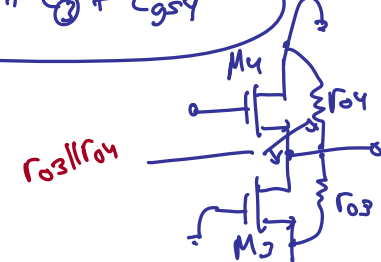
$$\tau_2 = (C_{gd1} + C_{db1} + C_{db2} + C_{gd2} + C_{gd4})(r_{o1} || r_{o2})$$

$$\tau_3 = (C_{gd3} + C_{db3} + C_{sb4})\left(\frac{1}{g_{m4} + g_{mb4}}\right)$$

$$\tau_{g4} = C_{gs4} \left( \frac{(r_{o1} || r_{o2}) + (r_{o3} || r_{o4})}{g_{m4} + g_{mb4}} \right) \approx C_{gs4} \left( \frac{2}{g_{m4} + g_{mb4}} \right)$$

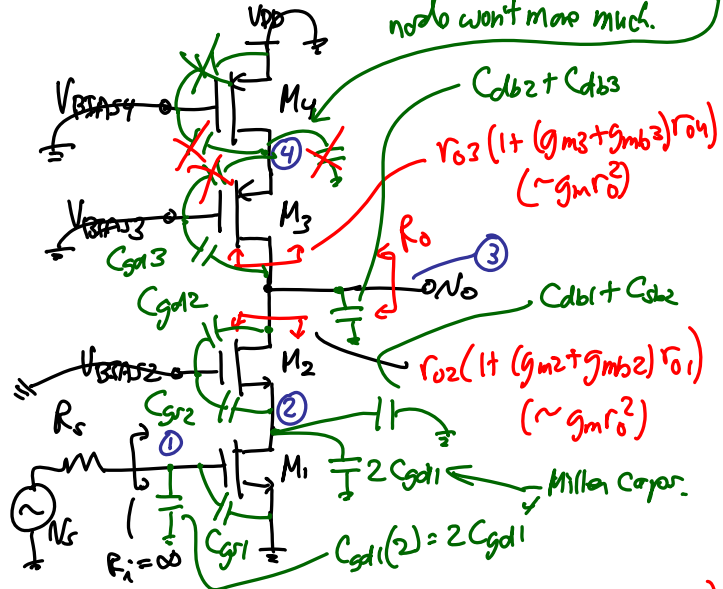
small

$$\omega_H = \frac{1}{\tau_1 + \tau_2 + \tau_3 + \tau_{g4}}$$



Ex. Cascode Drive + Load

For reason to be discussed, this node won't move much.



$$R_o = r_{o2}(1 + (g_{m2} + g_{mb2})r_{o1}) \parallel r_{o3}(1 + (g_{m3} + g_{mb3})r_{o4})$$

$$A_v = \frac{v_o}{v_s} = \frac{v_o}{v_1} \cdot \frac{v_2}{v_o} \cdot \frac{v_o}{v_2} \approx -1$$

$$= (1) \left( -g_{m1} \left( \frac{1}{g_{m2} + g_{mb2}} \right) \right) (g_{m2} + g_{mb2}) R_o$$

$$\therefore A_v = -g_{m1} R_o$$

Get the dominant pole: (use OCTC analysis)

$$\tau_{D1} = (2C_{gd1} + C_{gs1})R_s$$

$$\tau_{D2} = (2C_{gd1} + C_{gs2} + C_{db1} + C_{db2}) \left( \frac{1}{g_{m2} + g_{mb2}} \right)$$

$$\tau_{D3} = (C_{gd2} + C_{db2} + C_{db3} + C_{gd3})R_o \leftarrow \text{hugest}$$

$$\omega_H = \frac{1}{\tau_{D1} + \tau_{D2} + \tau_{D3}}$$

$\Rightarrow$  this is accurate enough... but... can we be a bit smarter?