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# ***Active Filters***

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# Active Lowpass Filter

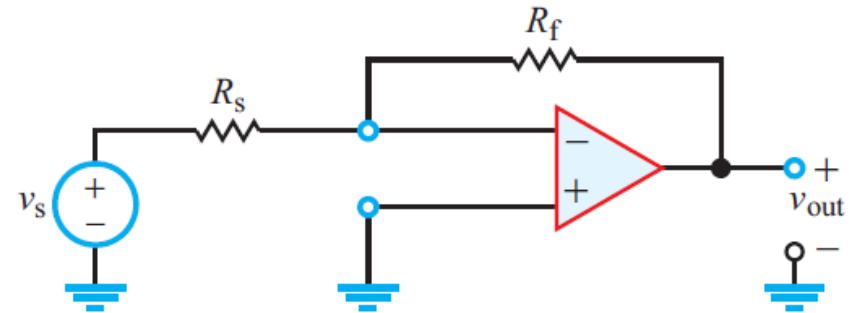
$$\mathbf{V}_{\text{out}} = -\frac{\mathbf{Z}_f}{\mathbf{Z}_s} \mathbf{V}_s$$

$$\mathbf{Z}_f = R_f \parallel \left( \frac{1}{j\omega C_f} \right) = \frac{R_f}{1 + j\omega R_f C_f}$$

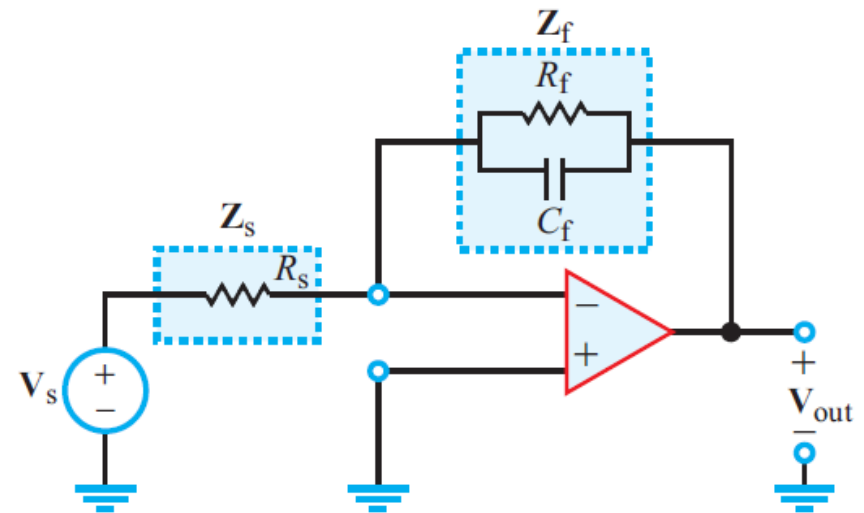
$$\begin{aligned} \mathbf{H}_{\text{LP}}(\omega) &= \frac{\mathbf{V}_{\text{out}}}{\mathbf{V}_s} = -\frac{\mathbf{Z}_f}{\mathbf{Z}_s} = -\frac{R_f}{R_s} \left( \frac{1}{1 + j\omega R_f C_f} \right) \\ &= G_{\text{LP}} \left( \frac{1}{1 + j\omega/\omega_{\text{LP}}} \right), \end{aligned}$$

where

$$G_{\text{LP}} = -\frac{R_f}{R_s}, \quad \omega_{\text{LP}} = \frac{1}{R_f C_f}$$



(a) Inverting amplifier

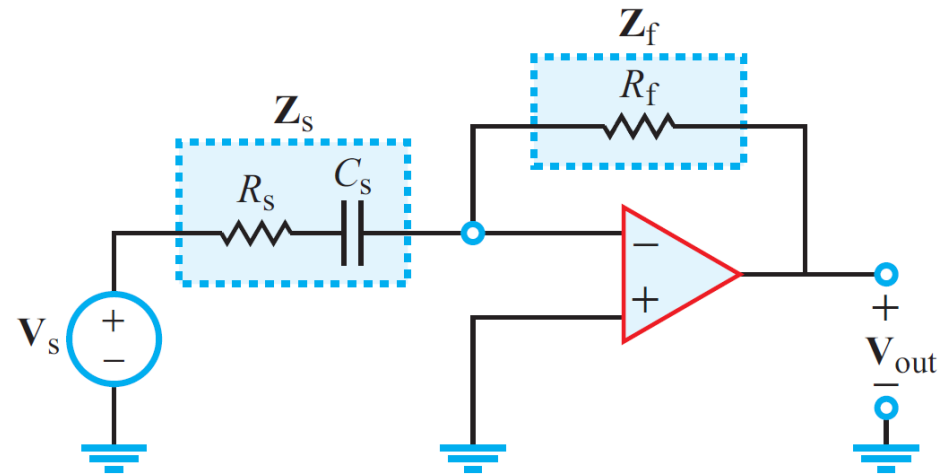


(b) Phasor domain with impedances

# Active Highpass Filter

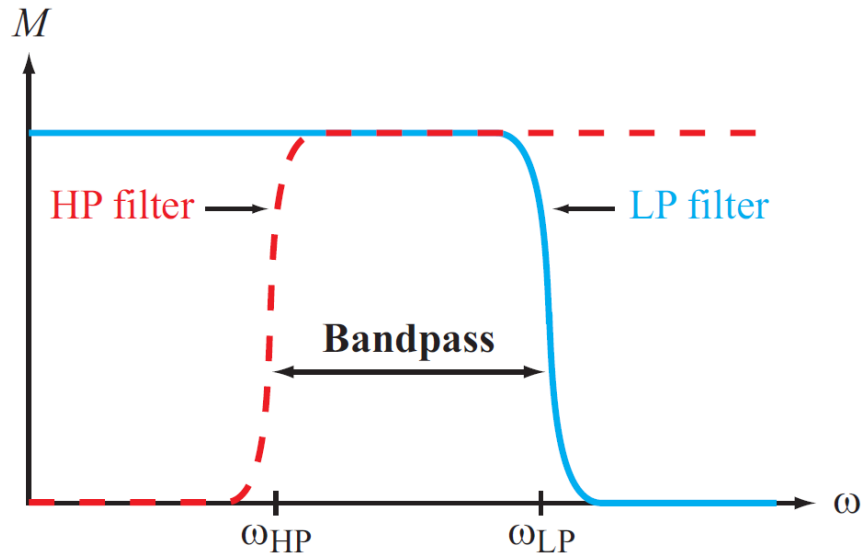
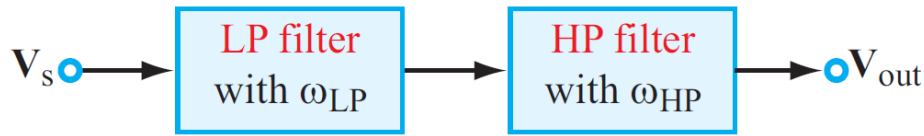
$$\mathbf{Z}_s = R_s - \frac{j}{\omega C_s} \quad \text{and} \quad \mathbf{Z}_f = R_f,$$

$$\begin{aligned} \mathbf{H}_{\text{HP}}(\omega) &= \frac{\mathbf{V}_{\text{out}}}{\mathbf{V}_s} = -\frac{\mathbf{Z}_f}{\mathbf{Z}_s} = -\frac{R_f}{R_s - j/\omega C_s} \\ &= G_{\text{HP}} \left[ \frac{j\omega/\omega_{\text{HP}}}{1 + j\omega/\omega_{\text{HP}}} \right], \end{aligned}$$

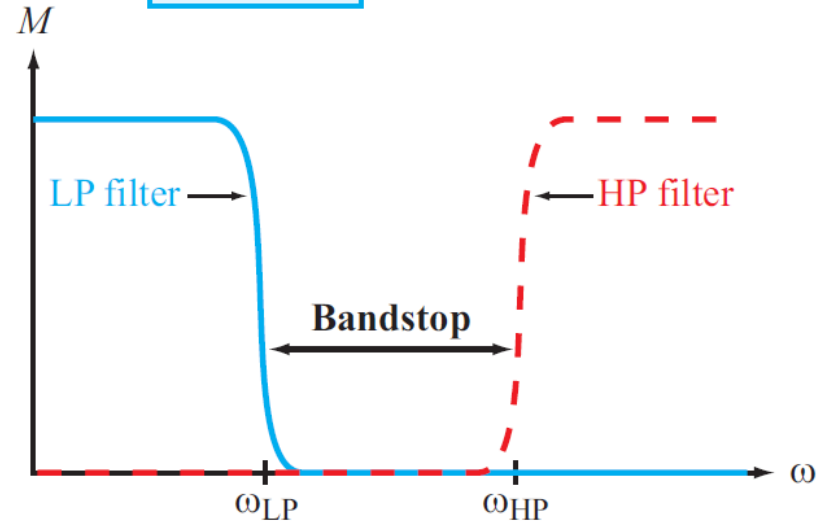
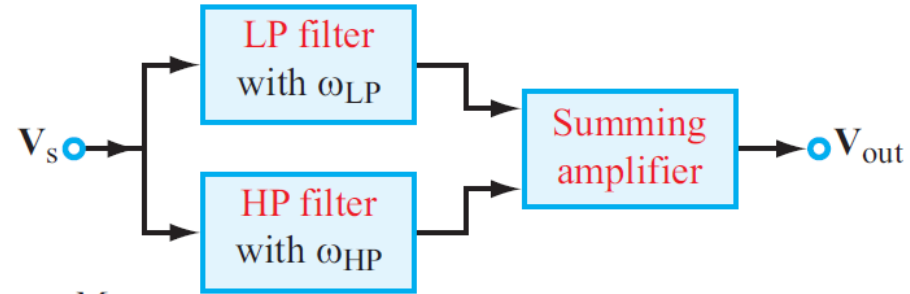


$$G_{\text{HP}} = -\frac{R_f}{R_s} \quad \text{and} \quad \omega_{\text{HP}} = \frac{1}{R_s C_s}.$$

# Cascading Active Filters

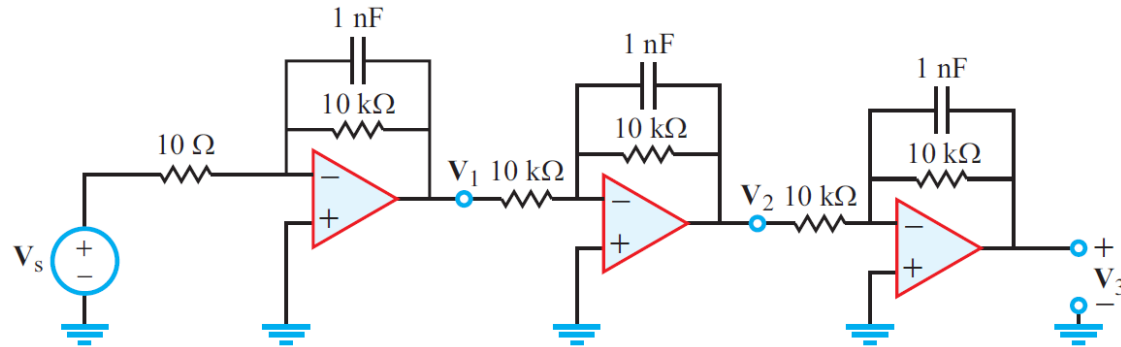


(a) Bandpass filter

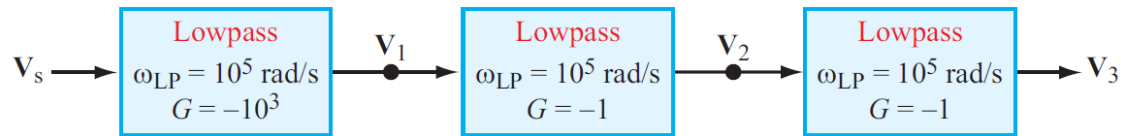


(b) Bandreject filter

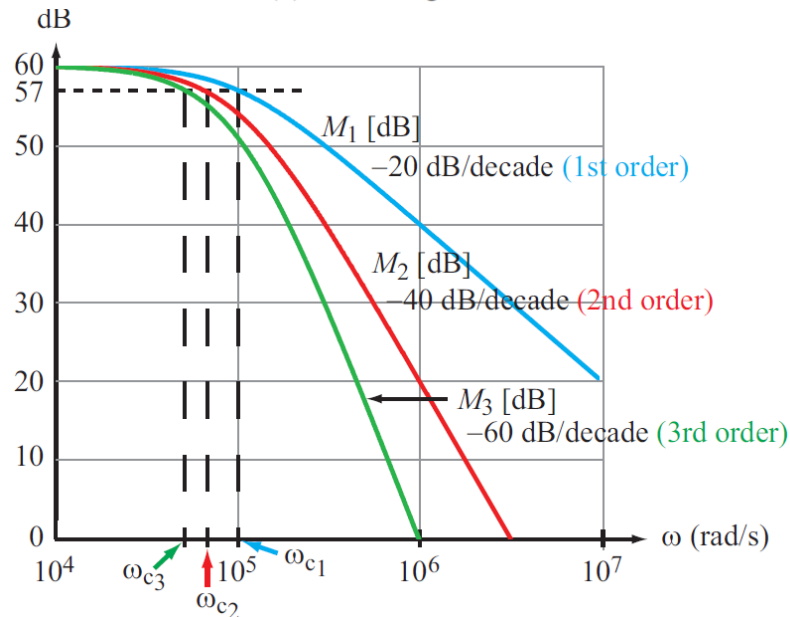
# Example: Third-Order Lowpass Filter



(a) Circuit diagram



(b) Block diagram



# Example: Bandreject Filter

Design a bandreject filter with the specifications:

(a) Gain = -50, (b) bandstop extends from 20 kHz to 40 kHz, and (c) gain roll-off rate = -40 dB/decade along both boundaries of the bandstop.

Somewhat arbitrarily, we select  $R = 1 \text{ k}\Omega$ . From

$$\omega_{LP} = 4\pi \times 10^4 = \frac{1}{RC_{LP}} \rightarrow C_{LP} = 7.96 \text{ nF} \simeq 8 \text{ nF},$$

$$\omega_{HP} = 8\pi \times 10^4 = \frac{1}{RC_{HP}} \rightarrow C_{HP} \simeq 4 \text{ nF}.$$

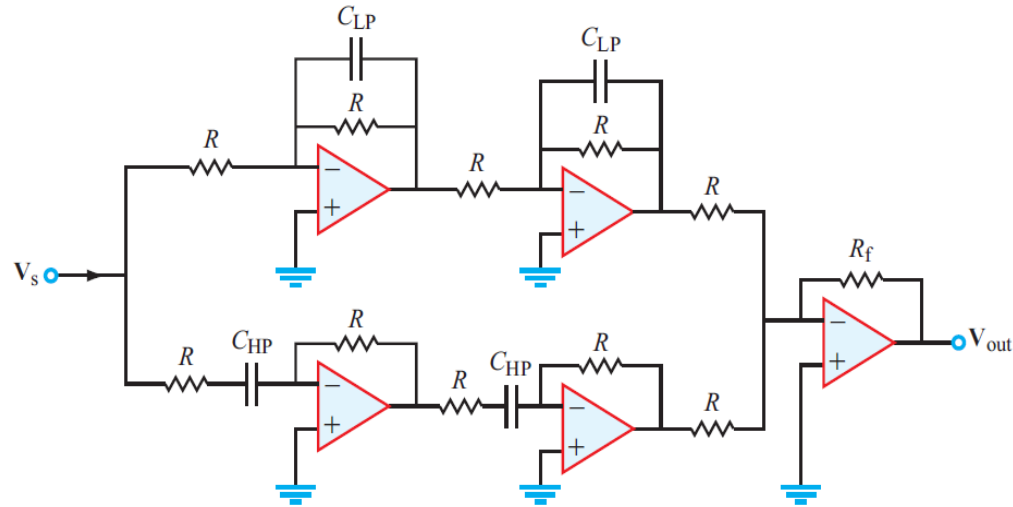
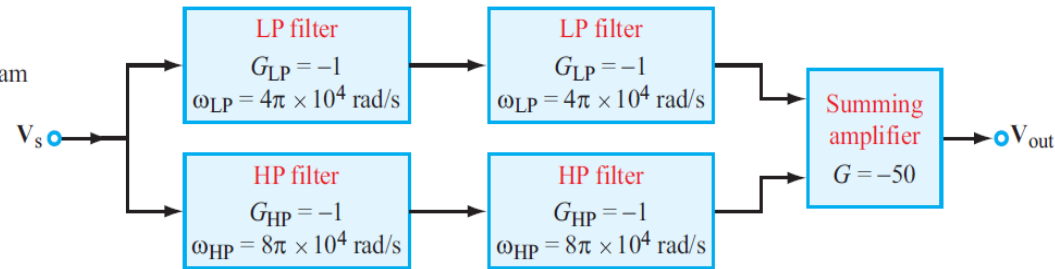
The value of  $R_f$  is specified by the gain of the summing amplifier as

$$G = -50 = -\frac{R_f}{R} \rightarrow R_f = 50 \text{ k}\Omega.$$

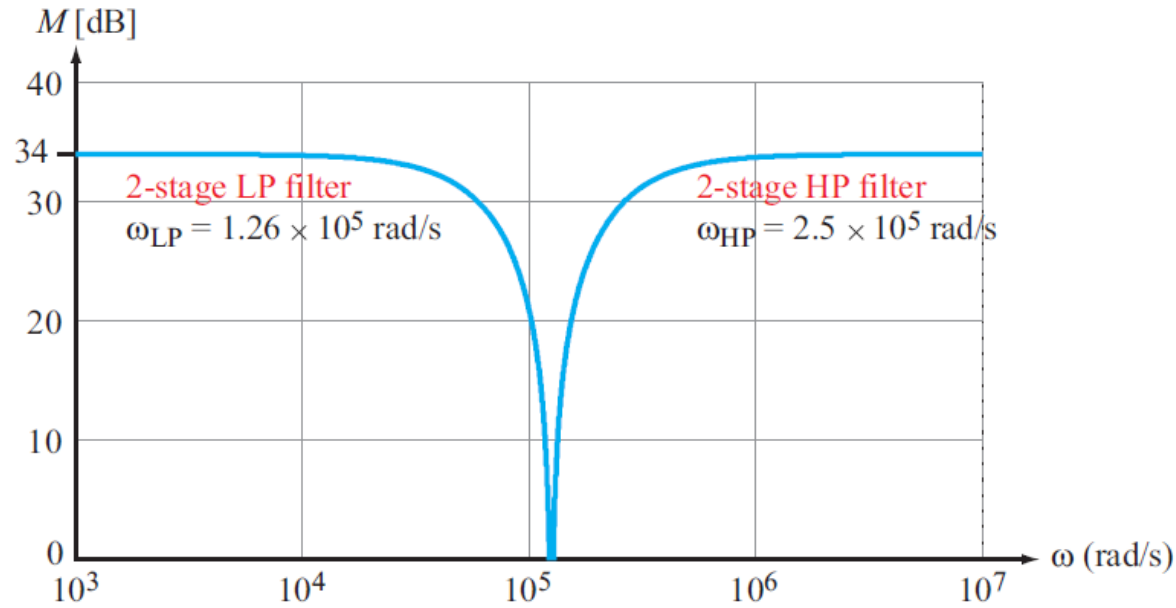
The transfer function of the bandreject filter is given by

$$\begin{aligned} \mathbf{H}(\omega) &= G[\mathbf{H}_{LP}^2 + \mathbf{H}_{HP}^2] \\ &= -50 \left[ \left( \frac{1}{1 + j\omega RC_{LP}} \right)^2 + \left( \frac{j\omega RC_{HP}}{1 + j\omega RC_{HP}} \right)^2 \right] \\ &= -50 \left[ \left( \frac{1}{1 + j\omega/4\pi \times 10^4} \right)^2 + \left( \frac{j\omega/8\pi \times 10^4}{1 + j\omega/8\pi \times 10^4} \right)^2 \right]. \end{aligned}$$

(a) Block diagram



# Example: Bandreject Filter



$$G = -50 = -\frac{R_f}{R} \quad \rightarrow \quad R_f = 50 \text{ k}\Omega.$$

The transfer function of the bandreject filter is given by

$$\begin{aligned} \mathbf{H}(\omega) &= G[\mathbf{H}_{LP}^2 + \mathbf{H}_{HP}^2] \\ &= -50 \left[ \left( \frac{1}{1 + j\omega RC_{LP}} \right)^2 + \left( \frac{j\omega RC_{HP}}{1 + j\omega RC_{HP}} \right)^2 \right] \\ &= -50 \left[ \left( \frac{1}{1 + j\omega/4\pi \times 10^4} \right)^2 + \left( \frac{j\omega/8\pi \times 10^4}{1 + j\omega/8\pi \times 10^4} \right)^2 \right]. \end{aligned}$$