

EE243 Advanced Electromagnetic Theory

Lec # 13: Waveguides and sources

- **Source Free Region: Vector Potentials A and F**
- **Single direction component of A and F**
 - **Give TM and TE**
 - **Are Adequate**
- **Perfectly Electrically Conducting Guides**
- **Source Excitation via Reciprocity**

Reading: Jackson Ch 8.2-8.4, 8.12

Harrington 3.2, 3.12

Collin 4.10

Overview

- A very general TE/TM separation into two scalar problems is first developed as a working tool.
- This TE/TM separation with respect to the z (propagation) direction is applied to perfectly electrically conducting waveguides.
- The waveguide modes, phase and group velocities are then derived.
- General representations for fields in waveguides are then developed.
- Reciprocity is then used to determine the excitation of a given waveguide mode.

Overview: TE/TM Separation

- In a homogeneous source free region, it is adequate in general to independently solve for **TWO SCALAR FUNCTIONS** instead of 6 components simultaneously (3 components of E and 3 components of B).
- These scalar functions are the components of the vector potentials A and F in a common direction.
- Under the Lorenz Gauge these scalar functions satisfy the wave equation and their boundary conditions generally differ.
- The scalar component of A gives fields that are transverse magnetic and the scalar component of F gives the fields that are transverse magnetic (both with respect to the common direction).

Magnetic/Electric Duality

Harrington 3.2

Electric Sources

Magnetic Sources

$$\nabla \times \bar{H} = -i\omega\epsilon\bar{E} + \bar{J}$$

$$\nabla \times \bar{E} = i\omega\mu\bar{H} - \bar{M}$$

$$\nabla \times \bar{E} = i\omega\mu\bar{H}$$

$$\nabla \times \bar{H} = -i\omega\epsilon\bar{E}$$

$$\bar{H} = \nabla \times \bar{A}$$

$$\bar{E} = -\nabla \times \bar{F}$$

$$\bar{A} = \frac{1}{4\pi} \int_V \frac{\bar{J} e^{ik|\bar{x}-\bar{x}'|}}{|\bar{x}-\bar{x}'|} d^3x'$$

$$\bar{F} = \frac{1}{4\pi} \int_V \frac{\bar{M} e^{ik|\bar{x}-\bar{x}'|}}{|\bar{x}-\bar{x}'|} d^3x'$$

- Dual equations for problems in which only an electric source \bar{J} or only a magnetic source \bar{M} are present.

Simultaneous Electric and Magnetic Sources

$$\bar{E} = -\nabla \times \bar{F} + \frac{1}{i\omega\epsilon} (\nabla \times \nabla \times \bar{A} - \bar{J})$$

$$\bar{H} = \nabla \times \bar{A} + \frac{1}{i\omega\mu} (\nabla \times \nabla \times \bar{F} - \bar{M})$$

$$\bar{A} = \frac{1}{4\pi} \int_V \frac{\bar{J} e^{ik|\bar{x}-\bar{x}'|}}{|\bar{x}-\bar{x}'|} d^3x'$$

$$\bar{F} = \frac{1}{4\pi} \int_V \frac{\bar{M} e^{ik|\bar{x}-\bar{x}'|}}{|\bar{x}-\bar{x}'|} d^3x'$$

- Superimpose contributions for the two source types.

Source Free Region

Harrington 3.12

$$\bar{E} = -\nabla \times \bar{F} + \frac{1}{i\omega\epsilon} (\nabla \times \nabla \times \bar{A})$$

$$\bar{H} = \nabla \times \bar{A} + \frac{1}{i\omega\mu} (\nabla \times \nabla \times \bar{F})$$

- Representation is still valid in a source free regions (A and F are viewed as being produced by sources outside of the region).

- With the Lorenz gauge A and F satisfy the wave equation and the fields are give by

$$\nabla^2 \bar{A} + k^2 \bar{A} = 0 \quad \bar{E} = -\nabla \times \bar{F} + i\omega\mu \bar{A} + \frac{1}{i\omega\epsilon} \nabla(\nabla \cdot \bar{A})$$

$$\nabla^2 \bar{F} + k^2 \bar{F} = 0 \quad \bar{H} = \nabla \times \bar{A} + i\omega \bar{F} + \frac{1}{i\omega\mu} \nabla(\nabla \cdot \bar{F})$$

Only Electric Potential in z Direction

$$\bar{\mathbf{A}} = \psi \hat{\mathbf{z}}$$

$$E_x = \frac{1}{-i\omega\epsilon} \frac{\partial^2 \psi}{\partial x \partial z}$$

$$E_y = \frac{1}{-i\omega\epsilon} \frac{\partial^2 \psi}{\partial y \partial z}$$

$$E_z = \frac{1}{-i\omega\epsilon} \left(\frac{\partial^2}{\partial z^2} + k^2 \right) \psi$$

$$H_x = \frac{\partial \psi}{\partial y}$$

$$H_y = -\frac{\partial \psi}{\partial x}$$

$$H_z = 0$$

- This contribution is transverse magnetic (TM) to the z direction

Only Magnetic Potential in z Direction

$$\bar{F} = \psi \hat{z}$$

$$E_x = -\frac{\partial \psi}{\partial y}$$

$$E_y = \frac{\partial \psi}{\partial x}$$

$$E_z = 0$$

$$H_x = \frac{1}{-i\omega\mu} \frac{\partial^2 \psi}{\partial x \partial z}$$

$$H_y = \frac{1}{-i\omega\mu} \frac{\partial^2 \psi}{\partial y \partial z}$$

$$H_z = \frac{1}{-i\omega\mu} \left(\frac{\partial^2}{\partial z^2} + k^2 \right) \psi$$

- This contribution is transverse electric (TE) to the z direction

Total Solution

- The addition of the TM and TE solutions is sufficient to express any arbitrary field in a source free region.
- Further, the choice of the direction about which to make the TE/TM can be any direction.
 - In empty waveguides and on dielectric slabs the TE/TM separation is often the direction of propagation.
 - An exception is a partially filled waveguide where the separation directions is perpendicular to the dielectric filling.
- The scalar function describing the TE and TM solutions typically have different boundary conditions

- Perfect electric conductor

$$E_z |_S = 0$$

$$\frac{\partial B_z}{\partial n} |_S = 0$$

ME for Uniform Guided Waves

$$\nabla \phi = \frac{\partial \phi}{\partial x} \hat{x} + \frac{\partial \phi}{\partial y} \hat{y} + ik_z \phi \hat{z} \quad \text{Jackson 8.2}$$

$$\nabla \cdot \bar{V} = \frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} + ik_z V_z$$

$$\nabla \times \bar{V} = \left(\frac{\partial V_z}{\partial y} - ik_z V_y \right) \hat{x} + \left(ik_z V_x - \frac{\partial V_z}{\partial x} \right) \hat{y} + \left(\frac{\partial V_y}{\partial x} - \frac{\partial V_x}{\partial y} \right) \hat{z}$$

$$\nabla^2 \phi = \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} - k^2 \phi = (\nabla_t^2 - k^2) \phi$$

- Guided waves have a uniform longitudinal phase variation e^{ikz}
- Factor the differential operators into transverse operators and longitudinal algebraic multipliers.

ME for Uniform Guided Waves (Cont.)

$$\left[\nabla_t^2 + (\mu\varepsilon\omega^2 - k^2) \right] \bar{E} = 0 \quad \text{Jackson 8.2}$$

$$\bar{E} = E_z \hat{z} + \bar{E}_t$$

$$\bar{E}_t = \frac{1}{(\mu\varepsilon\omega^2 - k^2)} \left[k \nabla_t E_z - \omega \hat{z} \times \nabla_t B_z \right]$$

$$\bar{B}_t = \frac{1}{(\mu\varepsilon\omega^2 - k^2)} \left[k \nabla_t B_z + \mu\varepsilon\omega \hat{z} \times \nabla_t E_z \right]$$

- E and B satisfy wave equation with transverse operator and $-k^2$
- Break up E and B into longitudinal and transverse
- Transverse fields can be found from E_z and B_z .

TEM Degeneracy

- Occurs when both E_z and B_z are zero
- TEM Solution
 - $B_z = 0$ makes $\text{Curl}_t E_{\text{TEM}} = 0$
 - $E_z = 0$ makes $\text{Div}_t E_{\text{TEM}} = 0$
 - E_{TEM} is a solution to an electrostatic problem in 2D.
- Consequences
 - Propagates with k of plane wave in free space
 - B_{TEM} and E_{TEM} are related as in plane wave in free space
 - Can only exist with more than one conductor

Boundary Conditions

$$n \times E = 0$$

$$\Rightarrow E_z |_S = 0$$

$$n \cdot B = 0$$

$$\Rightarrow \frac{B_z}{\partial n} |_S = 0$$

- For a perfect electric conductor there are no fields inside and E_{tan} is continuous
- For a perfect electric conductor B is zero inside and B_{normal} is continuous

Waveguide Simplifications

$$\bar{H}_t = \frac{\pm 1}{Z} \hat{z} \times \bar{E}_t$$

$$Z_{TM} = \frac{k}{\omega \epsilon} = \frac{k}{k_0} \sqrt{\frac{\mu}{\epsilon}}$$

$$Z_{TE} = \frac{\mu \omega}{k} = \frac{k_0}{k} \sqrt{\frac{\mu}{\epsilon}}$$

$$\gamma^2 = \mu \epsilon \omega^2 - k^2$$

$$\bar{E}_t = \pm \frac{ik}{\gamma^2} \nabla_t \bar{E}_z$$

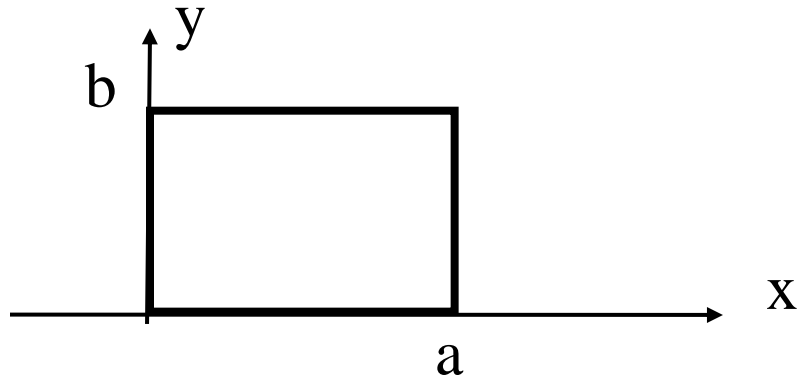
$$\bar{B}_t = \pm \frac{ik}{\gamma^2} \nabla_t \bar{B}_z$$

- First find E_z and B_z
- Then use gradient to find the associated transverse B or E
- Use impedance to find the associated transverse E and B
- Potentially there are 5 terms each for TE and TM but often there are only 3 terms each for the TE and TM

Generic Wave Properties

- The solution for the scalar function E_z or B_z introduces eigenvalues
- Phase propagation in the z direction only occurs once $\mu\epsilon\omega^2$ exceeds the eigenvalue.
 - Cutoff frequency
 - Phase velocity
 - Group velocity
- Modes that are cutoff are said to be evanescent due to their exponential decay

Rectangular Waveguide Example (TM)



$$\psi = E_z$$

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \gamma^2 \right) \psi = 0$$

$$\psi|_s = 0$$

$$\bar{E}_t = \pm \frac{ik}{\gamma^2} \nabla_t \psi$$

$$\bar{H}_t = \frac{\pm 1}{Z} \hat{z} \times \bar{E}_t$$

$$Z_{TM} = \frac{k}{\omega \epsilon} = \frac{k}{k_0} \sqrt{\frac{\mu}{\epsilon}}$$

$$E_{zmn} = E_0 \sin\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$$

$$\gamma_{mn}^2 = \pi^2 \left(\frac{m^2}{a^2} + \frac{n^2}{b^2} \right)$$

$$E_x = E_0 \frac{ik\pi}{\gamma_{mn}^2 a} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$$

$$E_y = E_0 \frac{ik\pi}{\gamma_{mn}^2 b} \sin\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right)$$

$$H_x = -E_0 \frac{ik\pi}{Z_{TM} \gamma_{mn}^2 b} \sin\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right)$$

$$H_y = E_0 \frac{ik\pi}{Z_{TM} \gamma_{mn}^2 a} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$$

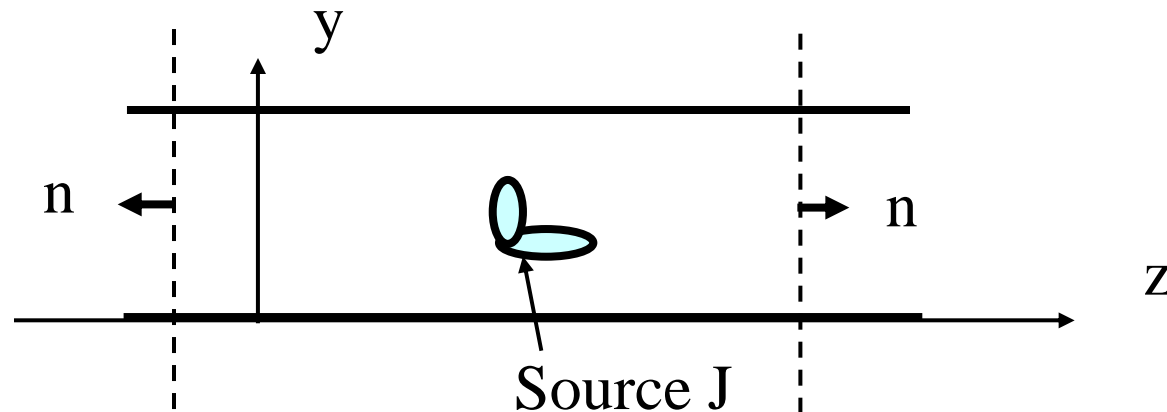
Rectangular Waveguide Orthonormal Modes

- The TE and TM modes are orthogonal to each other in any combination
- The TE and TM modes are orthogonal amongst themselves
- They can be normalized as has been done in Jackson 8.12

Representation of an Arbitrary Field

- The most general field in a source free region is a summation of TE and TM modes
- If the source is to the left then only fields propagating to the right need to be included
- FYI: Each mode by itself can be written as a sum of 4 planewaves
 - expand the sinusoidal behavior in x and y as exponentials
 - Compute the k -vector wave directions

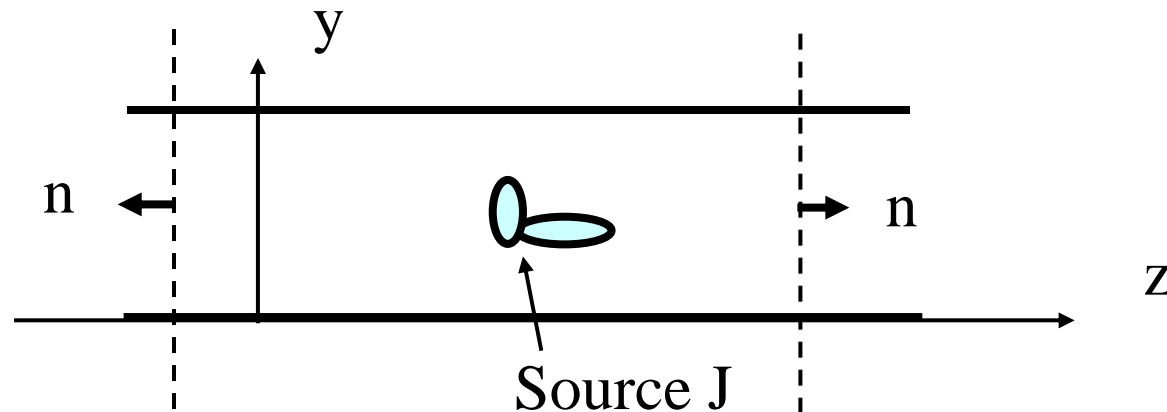
Fields Generated by a Localized Source



To find amplitude of a given mode propagating to the right

- General expansion for modes to right
- Assume the given mode of arbitrary amplitude is propagating to left from outside the boundary
- Apply reciprocity to the volume for these two sets of fields

Fields Generated by a Localized Source (Cont.)



Apply reciprocity to the volume for these two sets of fields

- Integral over wall is zero
- Integral over left cut-plane is zero as all modes going same direction
- Integral over right cut plane is proportional to outgoing mode amplitude times incoming mode amplitude
- Integral over the source measures the component of the source with the x,y eigenfunction variation as well as phase coherence with z and is proportional to incoming mode amplitude
- Ratio cancels incoming amplitude and gives outgoing amplitude.