

EE243 Advanced Electromagnetic Theory

Lec # 14: Sources in Guides

- **Solution Strategies**
- **Perfectly Electrically Conducting Guides**
- **Source Excitation via Reciprocity**
- **Plasmon fields and propagation constant**

Reading: Jackson 8.12

Plasmons now in Lecture 15

Overview

- Review construction of solutions
 - A component of A and F may be easier than Ez or Hz, but there is a little extra work to get Ez and Hz
- Reciprocity is useful for determining the excitation of a given waveguide mode.
- Waves on a single dielectric surface
 - Fields
 - Boundary conditions
 - Constraint
 - Plasmons for metals with $\epsilon_2 < -\epsilon_1$

Source Free Region

Harrington Strategy 3.12

$$\nabla^2 \bar{A} + k^2 \bar{A} = 0 \quad \bar{E} = -\nabla \times \bar{F} + i\omega\mu\bar{A} + \frac{1}{i\omega\epsilon} \nabla(\nabla \cdot \bar{A})$$

$$\nabla^2 \bar{F} + k^2 \bar{F} = 0 \quad \bar{H} = \nabla \times \bar{A} + i\omega\bar{F} + \frac{1}{i\omega\mu} \nabla(\nabla \cdot \bar{F})$$

- With the Lorenz gauge A and F satisfy the wave equation and the fields are give by above equations.
- Choosing the vectors A and B to only be in the z direction is adequate.
- Each potentially contributes 5 components of the E, H combination.

Only Electric Potential in z Direction

$$\bar{\mathbf{A}} = \psi \hat{\mathbf{z}}$$

$$E_x = \frac{1}{-i\omega\epsilon} \frac{\partial^2 \psi}{\partial x \partial z}$$

$$E_y = \frac{1}{-i\omega\epsilon} \frac{\partial^2 \psi}{\partial y \partial z}$$

$$E_z = \frac{1}{-i\omega\epsilon} \left(\frac{\partial^2}{\partial z^2} + k^2 \right) \psi$$

$$H_x = \frac{\partial \psi}{\partial y}$$

$$H_y = -\frac{\partial \psi}{\partial x}$$

$$H_z = 0$$

$$\bar{\mathbf{F}} = \psi \hat{\mathbf{z}}$$

$$E_x = -\frac{\partial \psi}{\partial y}$$

$$E_y = \frac{\partial \psi}{\partial x}$$

$$E_z = 0$$

$$H_x = \frac{1}{-i\omega\mu} \frac{\partial^2 \psi}{\partial x \partial z}$$

$$H_y = \frac{1}{-i\omega\mu} \frac{\partial^2 \psi}{\partial y \partial z}$$

$$H_z = \frac{1}{-i\omega\mu} \left(\frac{\partial^2}{\partial z^2} + k^2 \right) \psi$$

Jackson Strategy Eq. 8.26

$$\left[\nabla_t^2 + (\mu\epsilon\omega^2 - k^2) \right] \bar{E} = 0 \quad \text{Jackson 8.2}$$

$$\bar{E} = E_z \hat{z} + \bar{E}_t$$

$$\bar{E}_t = \frac{1}{(\mu\epsilon\omega^2 - k^2)} \left[k \nabla_t E_z - \omega \hat{z} \times \nabla_t B_z \right]$$

$$\bar{B}_t = \frac{1}{(\mu\epsilon\omega^2 - k^2)} \left[k \nabla_t B_z + \mu\epsilon\omega \hat{z} \times \nabla_t E_z \right]$$

- E and B satisfy wave equation with transverse operator and $-k^2$
- Break up E and B into longitudinal and transverse
- Transverse fields can be found from E_z and B_z .

Comparison of Harrington and Jackson

- In a homogeneous source free region, it is adequate in general to independently solve for TWO SCALAR FUNCTIONS but which is easier
 - z components of vector potentials A for TM and F for TE, or
 - Ez and Hz themselves?
- The vector potential A (or F) in one direction is advantageous in finding the transverse components of H (or E)
 - Pair of zeros in taking the curl => easier to determine the boundary condition
 - Only propagating known information forward
 - But Ez (or Hz) requires mult. $(1/j\omega\epsilon)(\omega^2\mu\epsilon-k_z^2)$
- To be fair Jackson though, Eq. 8.26 only propagates known information forward once Ez and Hz are known
 - Ey could have been found from z cross grad Bz to get boundary condition that normal derivative of Bz must be zero for TE case.

Waveguide Simplifications (Revised)

$$\bar{E}_t = \pm \frac{ik}{\gamma^2} \nabla_t \bar{E}_z$$

$$\bar{B}_t = \pm \frac{ik}{\gamma^2} \nabla_t \bar{B}_z$$

$$\gamma^2 = \mu\epsilon\omega^2 - k^2$$

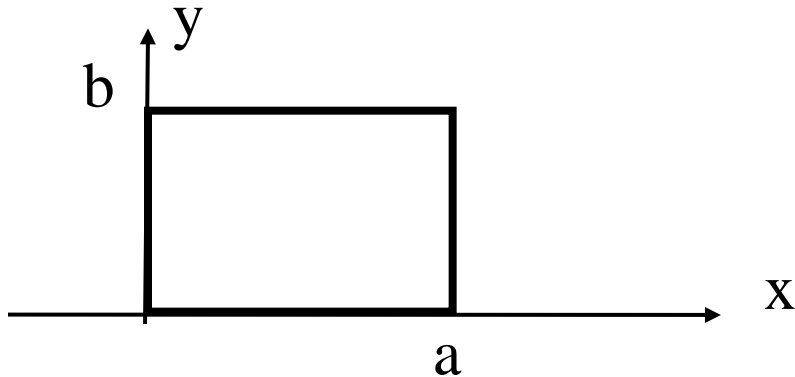
$$\bar{H}_t = \frac{\pm 1}{Z} \hat{z} \times \bar{E}_t$$

$$Z_{TM} = \frac{k}{\omega\epsilon} = \frac{k}{k_0} \sqrt{\frac{\mu}{\epsilon}}$$

$$Z_{TE} = \frac{\mu\omega}{k} = \frac{k_0}{k} \sqrt{\frac{\mu}{\epsilon}}$$

- Set Boundary Condition
 - If TE $E_z = 0$ on p.e.c. sidewall.
 - If TM use 8.26 to get normal derivative of $B_z = 0$
- Solve for E_z and/or B_z
- Then use gradient to find the associated transverse B or E
- Use impedance to find the associated transverse E and B (or use 8.26)

Rectangular Waveguide Example (TM)



$$\psi = E_z$$

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \gamma^2 \right) \psi = 0$$

$$\psi|_s = 0$$

$$\bar{E}_t = \pm \frac{ik}{\gamma^2} \nabla_t \psi$$

$$\bar{H}_t = \frac{\pm 1}{Z} \hat{z} \times \bar{E}_t$$

$$Z_{TM} = \frac{k}{\omega \epsilon} = \frac{k}{k_0} \sqrt{\frac{\mu}{\epsilon}}$$

$$E_{zmn} = E_0 \sin\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$$

$$\gamma_{mn}^2 = \pi^2 \left(\frac{m^2}{a^2} + \frac{n^2}{b^2} \right)$$

$$E_x = E_0 \frac{ik\pi}{\gamma_{mn}^2 a} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$$

$$E_y = E_0 \frac{ik\pi}{\gamma_{mn}^2 b} \sin\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right)$$

$$H_x = -E_0 \frac{ik\pi}{Z_{TM} \gamma_{mn}^2 b} \sin\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right)$$

$$H_y = E_0 \frac{ik\pi}{Z_{TM} \gamma_{mn}^2 a} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$$

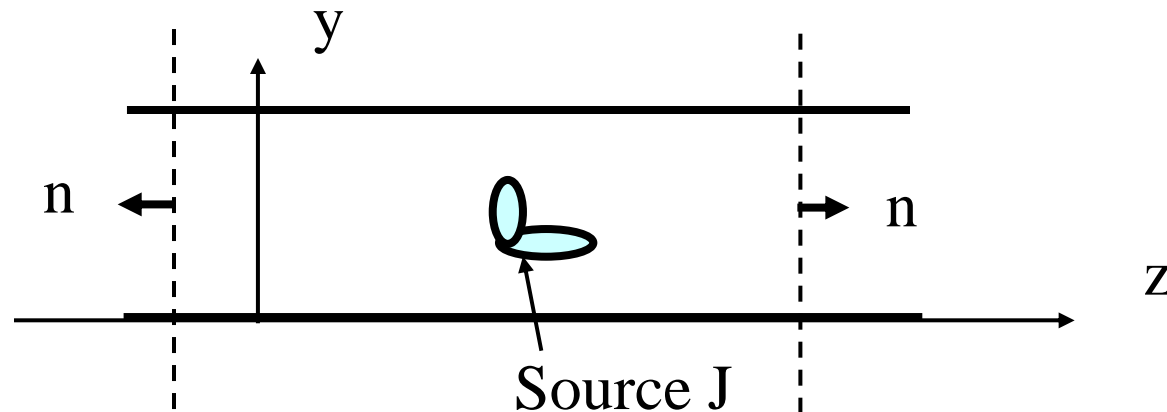
Generic Wave Properties

- The solution for the scalar function E_z or B_z introduces eigenvalues
- Phase propagation in the z direction only occurs once $\mu\epsilon\omega^2$ exceeds the eigenvalue.
 - Cutoff frequency
 - Phase velocity
 - Group velocity
- Modes that are cutoff are said to be evanescent due to their exponential decay

Rectangular Waveguide Orthonormal Modes

- The TE and TM modes are orthogonal to each other in any combination
- The TE and TM modes are orthogonal amongst themselves
- The waves can be normalized as has been done in Jackson 8.12
- The most general field in a source free region is a summation of TE and TM modes

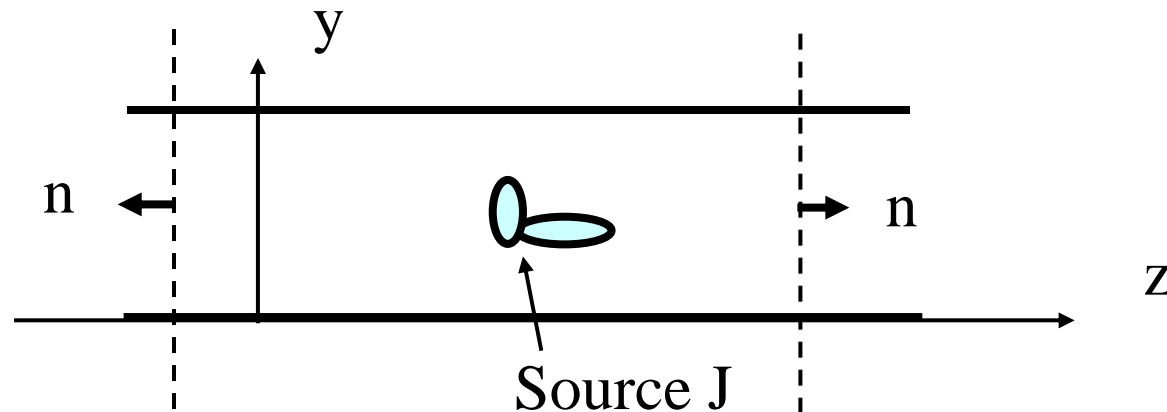
Fields Generated by a Localized Source



To find amplitude of a given mode propagating to the right

- General expansion for modes to right
- Assume the given mode of arbitrary amplitude is propagating to left from outside the boundary
- Apply reciprocity to the volume for these two sets of fields

Fields Generated by a Localized Source (Cont.)



Apply reciprocity to the volume for these two sets of fields

- Integral over wall is zero
- Integral over left cut-plane is zero as all modes going same direction
- Integral over right cut plane is proportional to outgoing mode amplitude times incoming mode amplitude
- Integral over the source measures the component of the source with the x,y eigenfunction variation as well as phase coherence with z and is proportional to incoming mode amplitude
- Ratio cancels incoming amplitude and gives outgoing amplitude.

Representation of Fields in Guide

- Localized source J creates waves

$$\bar{E}^+ = \sum_{\lambda} A_{\lambda}^+ [\bar{E}_{t\lambda}(x, y) + \bar{E}_{z\lambda}(x, y)] e^{-ik_{\lambda}z}$$

$$\bar{H}^+ = \sum_{\lambda} A_{\lambda}^+ [\bar{H}_{t\lambda}(x, y) + \bar{H}_{z\lambda}(x, y)] e^{-ik_{\lambda}z}$$

$$\bar{E}^- = \sum_{\lambda} A_{\lambda}^- [\bar{E}_{t\lambda}(x, y) - \bar{E}_{z\lambda}(x, y)] e^{+ik_{\lambda}z}$$

$$\bar{H}^- = \sum_{\lambda} A_{\lambda}^- [-\bar{H}_{t\lambda}(x, y) + \bar{H}_{z\lambda}(x, y)] e^{+ik_{\lambda}z}$$

$$\bar{E}_{TEST}^- = C_{\lambda}^- [\bar{E}_{t\lambda}(x, y) - \bar{E}_{z\lambda}(x, y)] e^{+ik_{\lambda}z}$$

$$\bar{H}_{TEST}^- = C_{\lambda}^- [-\bar{H}_{t\lambda}(x, y) + \bar{H}_{z\lambda}(x, y)] e^{+ik_{\lambda}z}$$

- Index λ goes over TE, TM, m, n
- To right of source only waves to $+z$ and sum over all TE and TM modes that propagate
- To left of source only waves to $-z$ and sum over all TE and TM waves
- To left fields have signs altered $\text{div } E = \text{div } H = 0$
- Test wave from outside going to left across volume

Apply Reciprocity Formulation

$$\nabla \cdot \left(\bar{\mathbf{E}}_{TEST} \times \bar{\mathbf{H}}_{\lambda}^{\pm} - \bar{\mathbf{E}}_{\lambda}^{\pm} \times \mathbf{H}_{TEST} \right) = \bar{\mathbf{J}} \cdot \bar{\mathbf{E}}_{TEST}$$

$$\int_S \left(\bar{\mathbf{E}}_{TEST} \times \bar{\mathbf{H}}_{\lambda}^{\pm} - \bar{\mathbf{E}}_{\lambda}^{\pm} \times \mathbf{H}_{TEST} \right) \cdot \hat{\mathbf{n}} da = \int_V \bar{\mathbf{J}} \cdot \bar{\mathbf{E}}_{TEST} d^3x$$

- Source J produces the modes leaving the localized source region with amplitudes A_{λ}
- Source free TEST wave enters the volume and takes a measure of E
- Take Poynting Theorem like interaction

Evaluating Terms on Surfaces

$$\left(\bar{E}_{TEST} \times \bar{H}_{\lambda}^{\pm} - \bar{E}_{\lambda}^{\pm} \times H_{TEST} \right) \cdot \hat{n}$$

$$\left(C\bar{E}_{\tau}^{-} \times A_{\tau}\bar{H}_{\tau}^{-} - A_{\tau}\bar{E}_{\tau}^{-} \times CH_{\tau}^{-} \right) \cdot (-\hat{z}) = 0$$

$$\left(C\bar{E}_{\tau}^{-} \times A_{\tau}\bar{H}_{\tau}^{+} - A_{\tau}\bar{E}_{\tau}^{+} \times CH_{\tau}^{-} \right) \cdot \hat{z}$$

$$= \left(C\bar{E}_{\tau}^{+} \times A_{\tau}\bar{H}_{\tau}^{+} - A_{\tau}\bar{E}_{\tau}^{+} \times (-CH_{\tau}^{+}) \right) \cdot \hat{z}$$

$$= 2CA_{\tau} (\bar{E}_{\tau}^{+} \times \bar{H}_{\tau}^{+}) \cdot \hat{z} = 2CA_{\tau} Power$$

- Integral over p.e.c. is zero because E parallel to the surface is zero.
- Integral over left plane
 - Due to orthogonality between TE and TM and within TE or TM this integral could only be non-zero for $\lambda = TEST = \tau$.
 - But for this term the two cross products are identical and cancel

Combining to find the mode amplitude

$$\int_S \left(\bar{E}_{TEST} \times \bar{H}_\lambda^\pm - \bar{E}_\lambda^\pm \times H_{TEST} \right) \cdot \hat{n} da = \int_V \bar{J} \cdot \bar{E}_{TEST} d^3x$$

$$2CA_\tau Power = \int_V \bar{J} \cdot C\bar{E}_\tau^- d^3x$$

$$A_\tau = \frac{1}{2Power} \int_V \bar{J} \cdot \bar{E}_\tau^- d^3x$$

- The amplitude of the test wave cancels
- The mode amplitude is half of the power normalized integral of the electric field of the inward traveling mode with the source current

Plasmons now in Lecture 15