

Lecture 14: Beam Bending

• Announcements:

- HW#4 online and due Tuesday, Oct 18
- Lecture Module 8 online
- Slight issue with HW#1 solutions
  - ↳ Some of the circuit schematics for superposition on the last problem were not quite right ... but the solutions (i.e., equations and numbers) were still right

↳ Fix is online

- Midterm is nearing: Thursday, Oct. 27
  - ↳ I will soon pass out materials associated with the midterm, including an information sheet and old exams
- Makeup Lecture:
  - ↳ I won't be here Thursday, next week
  - ↳ We will make up the lecture on Friday, 10/14, this week, in 2 LeConte, from 3-4:30 p.m.

• Reading: Senturia, Chpt. 9

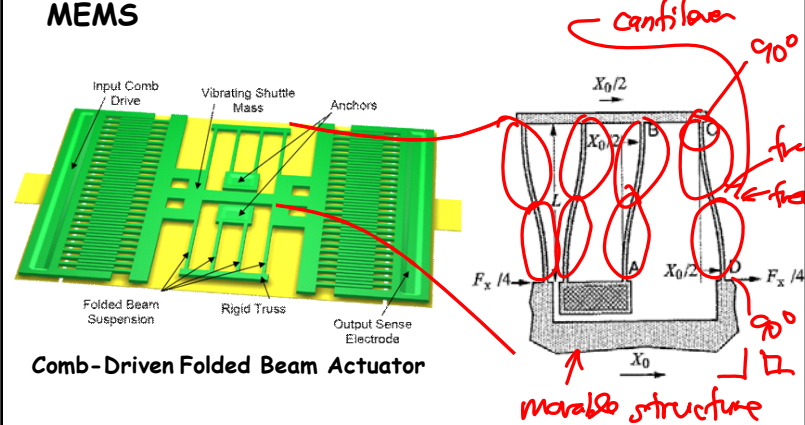
• Lecture Topics:

- ↳ Bending of beams
- ↳ Cantilever beam under small deflections
- ↳ Combining cantilevers in series and parallel
- ↳ Folded suspensions
- ↳ Design implications of residual stress and stress gradients

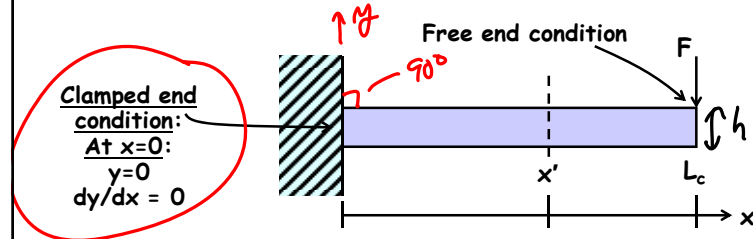
• Last Time:

- Finished Module 7 on Mechanics of Materials
- Now start a new topic: Bending of Beams

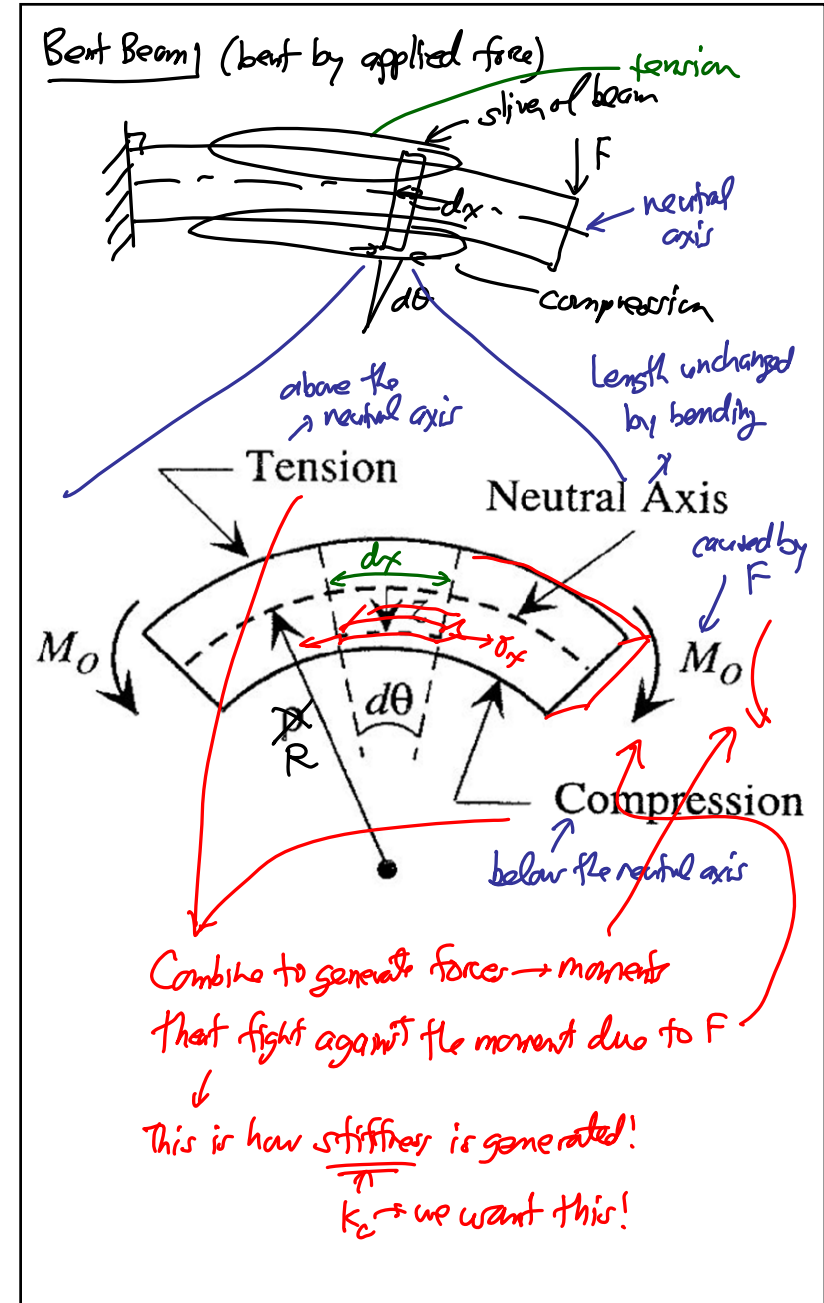
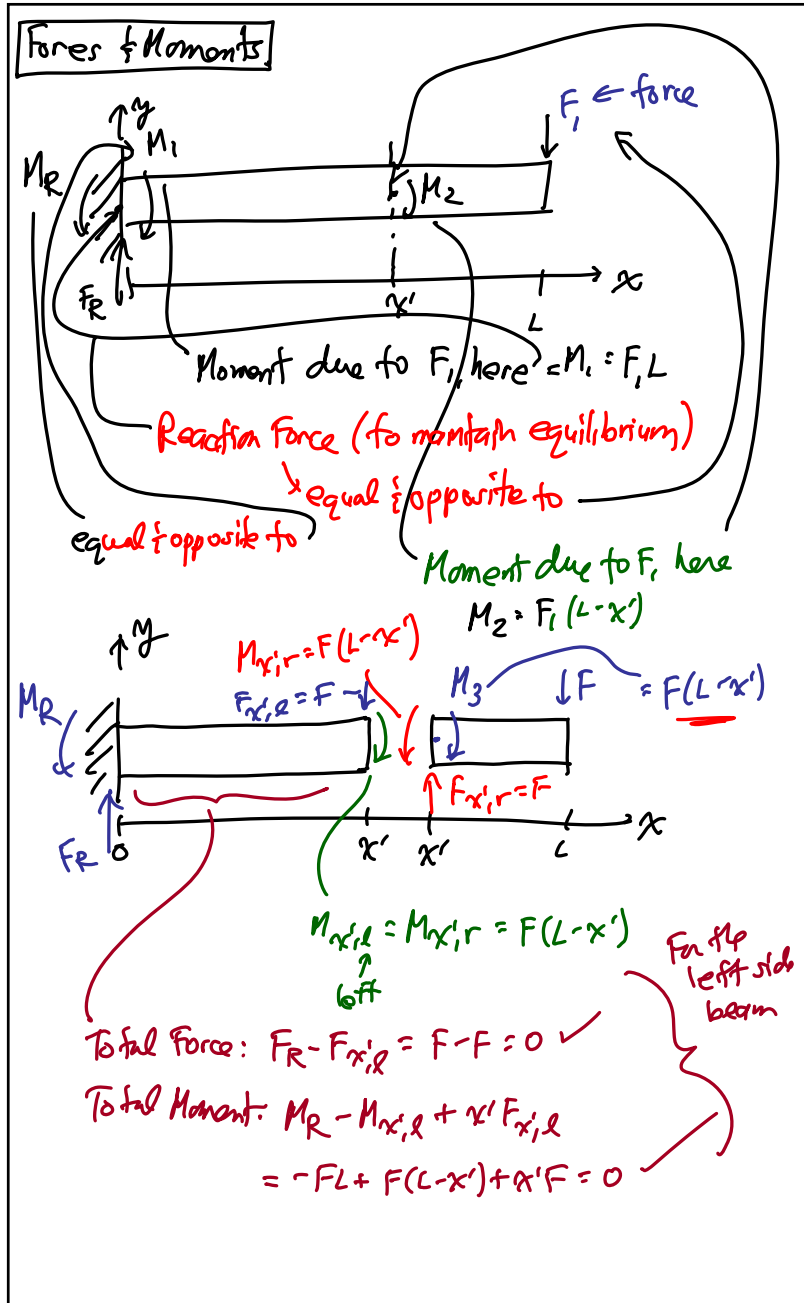
- Springs and suspensions very common in MEMS
- Coils are popular in the macro-world; but not easy to make in the micro-world
- Beams: simpler to fabricate and analyze; become "stronger" on the micro-scale → use beams for MEMS



Problem: Bending a Cantilever Beam



- Objective: Find relation between tip deflection  $y(x=L_c)$  and applied load  $F$
- Assumptions:
  1. Tip deflection is small compared with beam length
  2. Plane sections (normal to beam's axis) remain plane and normal during bending, i.e., "pure bending"
  3. Shear stresses are negligible



Beam Segment in Pure Bending

⇒ consider the segment bounded by the dashed lines defining  $d\theta$

At  $z=0$ : neutral axis → segment length =  $dx = R d\theta$  (1)

At any  $z$ : segment length =  $dL = (R-z) d\theta$  (2)

Combine (1) & (2):  $dL = dx - z d\theta = dx - \frac{z}{R} dx$

Thus, the axial strain @  $z$ :

$$\epsilon_x = \frac{dL - dx}{dx} = -\frac{z}{R}$$

$$\epsilon_x = -\frac{z}{R}$$

Thus, the strain varies linearly along the beam thickness:

Of course, there is a correspondingly axial stress:

$$\sigma_x = \epsilon_x E = \frac{-zE}{R} = \sigma_x$$

This gradient of stress then generates a bending moment!

in response to the original applied moment (from F)

Stress → Force:  $M = Fz$ , what is F?

$\sigma_{x,z} = \frac{F}{A} \rightarrow F = (wdz) \cdot \sigma_{x,z}$   
 $A = wdz$

⇒ integrate stress through the thickness of the beam:

$$M = \int_{-\frac{h}{2}}^{\frac{h}{2}} \underbrace{(w dz)}_{\text{force}} \sigma_x \cdot z$$

$$= \int_{-\frac{h}{2}}^{\frac{h}{2}} \frac{E w z^2}{R} dz \Rightarrow M = -\left(\frac{1}{2} W h^3\right) \frac{E}{R}$$

$\uparrow$   $\left[\sigma_x = -\frac{zE}{R}\right]$

$\frac{1}{2} W h^3 = I \triangleq$  Moment of Inertia

Note: (+) of radius of curvature  
(-) internal bending moment

$$\frac{1}{R} = -\frac{M}{EI}$$

Differential Equation for Beam Bending

Write out some geometric relationships:

⇒ then use small angle approx:

$$\cos \theta = \frac{dx}{ds} \rightarrow ds = \frac{dx}{\cos \theta} \rightarrow ds \approx dx$$

$$\tan \theta = \frac{dw}{dx} = \text{slope of the beam @ this point} \rightarrow \theta \approx \frac{dw}{dx} \quad (1)$$

$$ds = R d\theta \rightarrow \frac{1}{R} = \frac{d\theta}{ds} \rightarrow \frac{1}{R} = \frac{d^2 w}{dx^2} \quad (2)$$

Inserting (1) into (2)

$$\frac{1}{R} = \frac{d^2 w}{dx^2} = -\frac{M}{EI}$$

Diff. Eqn. for Small Angle Beam Bending

Cantilever Beam w/ Concentrated Load

Clamped end condition:  
At  $x=0$ :  
 $y=0$   
 $dy/dx = 0$

Free end condition

Point Load  $F$

Internal Moment

responds to

Internal Moment @ position  $x$ :  $M = -F(L-x)$

Thus:  $\frac{d^2 w}{dx^2} = \frac{F}{EI} (L-x)$

69 { Clamped End B.C.:  $w(x=0) = 0, \frac{dw}{dx}(x=0) = 0$   
Free End B.C.: none