

Lecture 15: Stress Gradients

- Announcements:
- Lecture Module 9 online
- Midterm is nearing: Thursday, Oct. 27
  - ↳ I will soon pass out materials associated with the midterm, including an information sheet and old exams
- Makeup Lecture:
  - ↳ I won't be here Thursday, next week
  - ↳ We will make up the lecture on Friday, 10/14, this week, in 2 LeConte, from 3-4:30 p.m.
- When turning in homework, staple all sheets together to avoid issues with lost pages
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- Reading: Senturia, Chpt. 9
- Lecture Topics:
  - ↳ Bending of beams
  - ↳ Cantilever beam under small deflections
  - ↳ Combining cantilevers in series and parallel
  - ↳ Folded suspensions
  - ↳ Design implications of residual stress and stress gradients
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- Last Time:
- Beam bending theory



Cantilever Beam w/ Concentrated Load

Clamped end condition:  
At  $x=0$ :  
 $y=0$   
 $dy/dx = 0$

Free end condition

Point Load  $F$

Internal Moment

responds to

Internal Moment @ position  $x$ :  $M = -F(L-x)$

Thus:  $\frac{d^2w}{dx^2} = \frac{F}{EI}(L-x)$

w/ { Clamped End B.C.:  $w(x=0) = 0, \frac{dw}{dx}(x=0) = 0$   
Free End B.C.: NONE

Solve to get for  $w$ :  
⇒ use Laplace; or a trial solution:  
 $w = Ax + Bx^2 + Cx^3$ , then apply B.C.'s

$$w = \frac{FL}{2EI} x^2 \left(1 - \frac{x}{3L}\right)$$

Deflection @  $x$  due to a point load  $F$  applied @  $x=L$

Maximum Deflection  $\rightarrow$  occurs  $x=L$ :

$$w_{max} = \left(\frac{L^3}{3EI}\right)F \rightarrow F = \left(\frac{3EI}{L^3}\right)w(x=L)$$

$= k_c w(x=L)$

stiffness  $\hat{=} k_c$   
@  $x=L$

where  $k_c = \frac{3EI}{L^3} \hat{=} \frac{0}{L}$

in general, stiffness is a function of location

$[I = \frac{1}{12}wh^3] \rightarrow k_c = \frac{1}{4}E\frac{wh^3}{L^3}$

Ex.  $L=100\mu m, w=2\mu m, h=2\mu m$   
polysilicon  $\rightarrow E=150 \text{ GPa}$

$$k_c = \frac{1}{4}(150 \text{ G})(2\mu)\left(\frac{2\mu}{100\mu}\right)^3 = \underline{\underline{0.6 \text{ N/m}}}$$

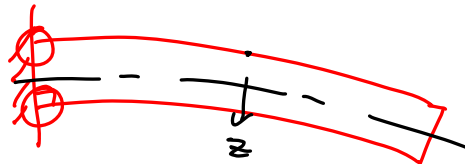
Maximum Stress in a Bent Cantilever

From before, the radius of curvature is given by

$$\frac{1}{R} = \frac{d^2w}{dx^2} = \frac{F}{EI}(L-x)$$

$\Rightarrow \frac{1}{R}$  is maximized (i.e.,  $R$  is minimized) when

$x=0$ :  
 $[x=0] \Rightarrow \frac{1}{R} = \frac{d^2w}{dx^2} = \frac{FL}{EI}$  \*



Strain is maximized:

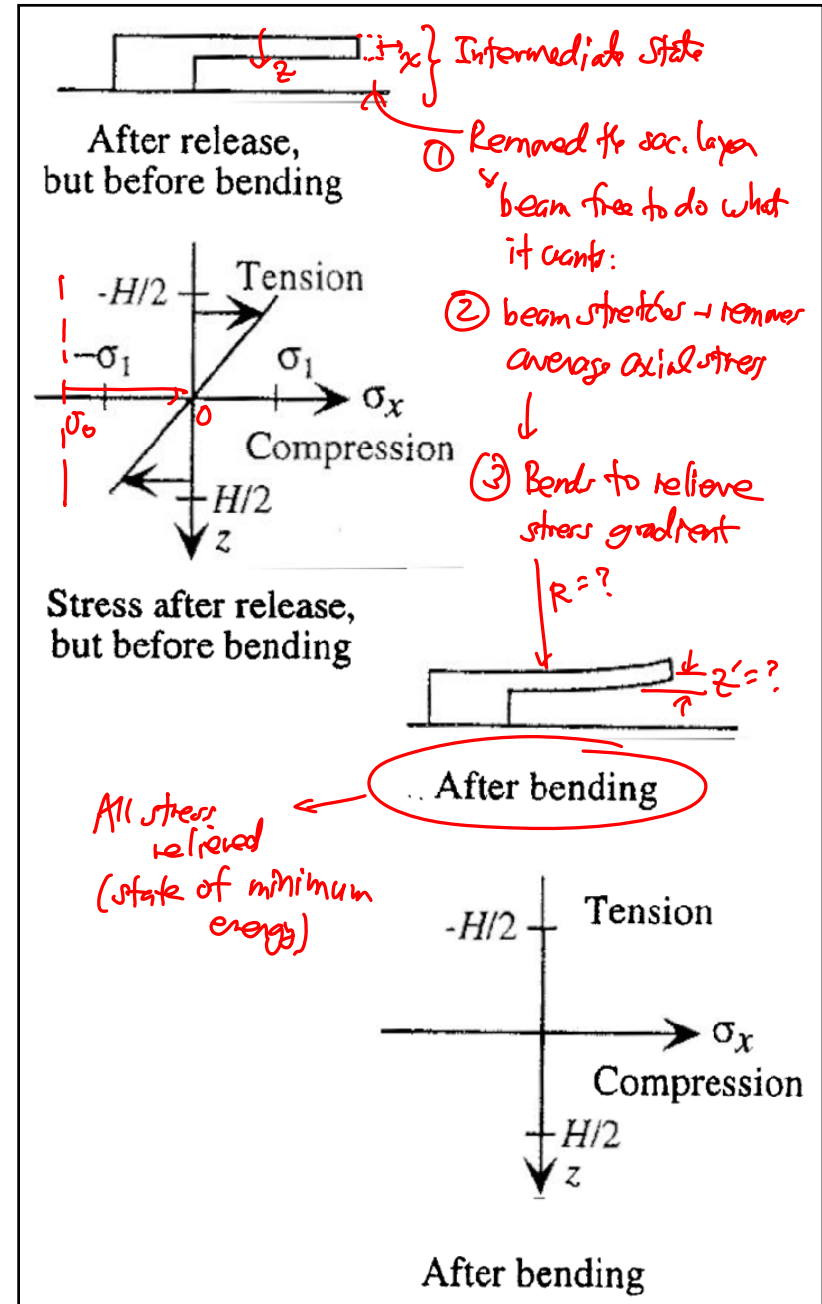
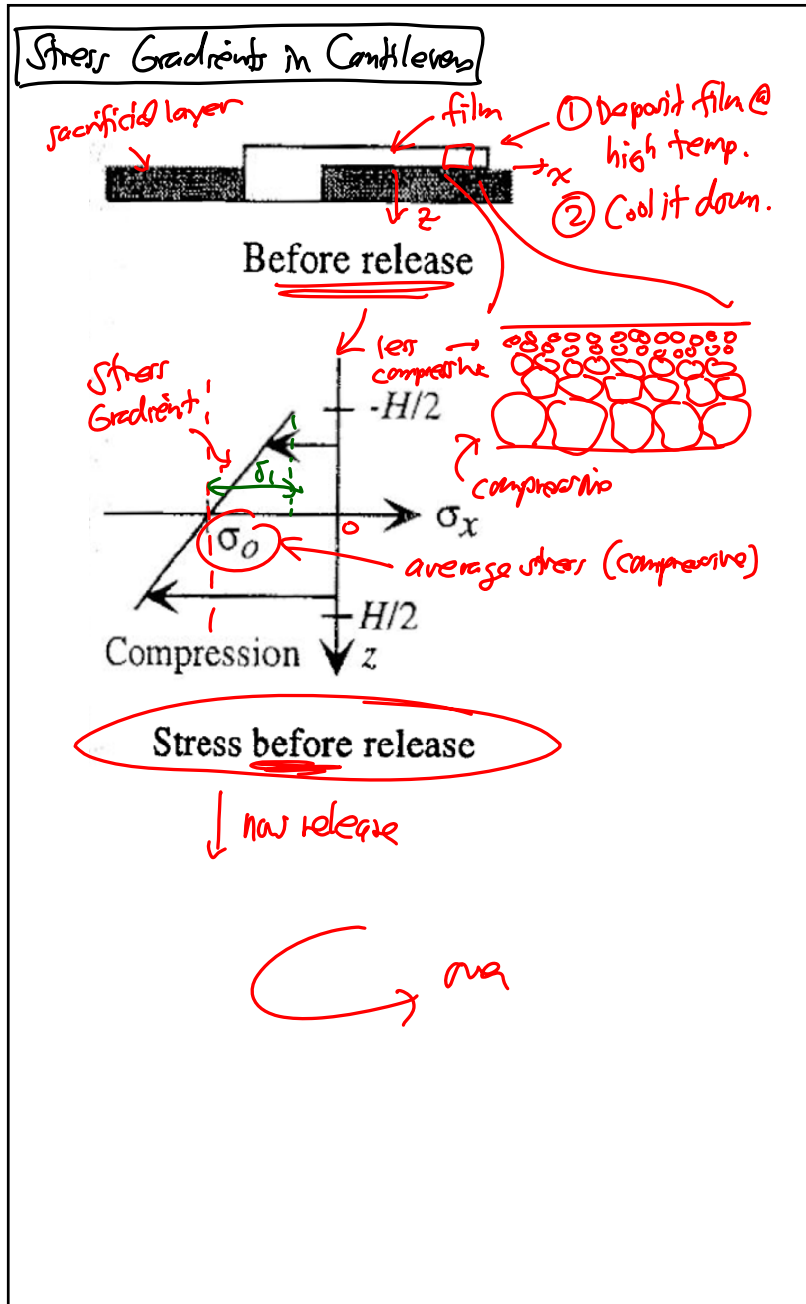
- ① At top surface  $\rightarrow$  tensile
- ② At bottom surface  $\rightarrow$  compressive

$$\epsilon_{max} = \frac{z}{R} = \frac{h}{2} \frac{1}{R} = \left(\frac{h}{2} \frac{FL}{EI}\right) = \epsilon_{max}$$

\*  $[I = \frac{1}{12}wh^3] \rightarrow \epsilon_{max} = \frac{1}{2} \frac{FL}{E} \left(\frac{12}{wh^3}\right) = \frac{6L}{Ewh^2} F$

$\sigma_{max} = \epsilon_{max} E = \frac{6L}{wh^2} F$

(maximum stress in a bent cantilever subjected to a force  $F$  at its tip)



Bending Due to Stress Gradients

Find the radius of curvature:

Prior to release, axial stress:  $\sigma = \sigma_0 - \frac{\sigma_1}{(H/2)} z$

The internal moment:

$$M_x = \int_{-H/2}^{H/2} [(w \cdot dz) \cdot \sigma] \cdot z = \int_{-H/2}^{H/2} w \left( z \sigma_0 - \frac{\sigma_1 z^2}{(H/2)} \right) dz$$

$$= w \left( \frac{1}{2} \sigma_0 z^2 - \frac{2 \sigma_1 z^3}{3H} \right) \Big|_{-H/2}^{H/2}$$

$$= w \left( \frac{1}{2} \sigma_0 \frac{H^2}{4} - \frac{2}{3} \sigma_1 \frac{H^2}{8} + \frac{1}{2} \sigma_0 \frac{H^2}{4} - \frac{2}{3} \sigma_1 \frac{H^2}{8} \right)$$

average stress cancels out

$$M_x = -\frac{1}{6} \sigma_1 w H^2$$

Thus, the radius of curvature:

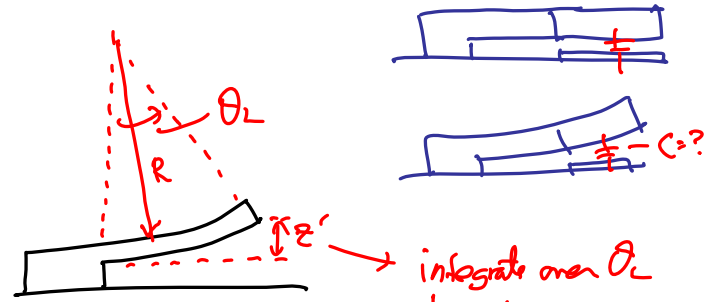
$$\frac{1}{R} = -\frac{M_x}{E'I} \rightarrow R = \frac{E'I}{M_x} = \frac{1}{2} \frac{E'H}{\sigma_1}$$

↑  
Biaxial Modulus

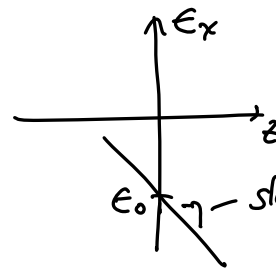
$$[I = \frac{1}{12} w h^3]$$

$$\rightarrow R = \frac{1}{2} \frac{E}{(1-\nu)} \frac{H}{\sigma_1} \quad \left[ \begin{array}{l} \text{Radius of Curvature} \\ \text{for a Cantilever w/} \\ \text{a Stress Gradient} \end{array} \right]$$

Radius of Curvature  $\rightarrow z'$



Definition. Strain Gradient



slope = Strain Gradient =  $\Gamma$

$$\Gamma = \frac{\epsilon_1}{(H/2)}$$

$$R = \frac{1}{2} \frac{E}{(1-\nu)} \frac{H}{\sigma_1} = \frac{H}{2} \frac{E'}{\sigma_1} = \frac{(H/2)}{\epsilon_1} = \frac{1}{\Gamma} \rightarrow \left( \Gamma = \frac{1}{R} \right) \checkmark$$

integrate over  $\sigma_1$  to get  $z'$   
↓  
Do this is homework...

### Series Combination of Springs

$L_c$   $L_c$   $L = 2L_c$   
 $x_1$   $x_2$   $x_{tot}$   
 $F$   
 $y(L)$   
*maintains 90°*  
*Free (just like a cantilever)*  
*cantilever → stiffness =  $k_c$*   
*also, a cantilever*  
*↓*  
*stiffness =  $k_c$*

Series:  $x_{tot} = x_1, x_{tot} = x_2$  }  $x_{tot} = x_1 + x_2$

What's the force law? →  $F$

$$y(L) = \frac{F}{k} = 2y(L_c) = 2\left(\frac{F}{k_c}\right) = F\left(\frac{1}{k_c} + \frac{1}{k_c}\right)$$

stiffness of the whole thing  $\rightarrow \frac{1}{k} = \frac{1}{k_c} + \frac{1}{k_c} \rightarrow k = k_c || k_c$

Definition for "||":  $A || B = \frac{1}{\frac{1}{A} + \frac{1}{B}} = \frac{AB}{A+B}$

### Parallel Combination of Springs

$k_a$   $x_a$   $F/2$   $F$   $x_{tot}$   
 $a$   $b$   $k_b$   $F/2$   $x_b$   $y(L)$

Parallel:  $x_{tot} = x_a = x_b$   
 $y(L) = \frac{F}{k} = \frac{F_a}{k_a} = \frac{F_b}{k_b} = \left(\frac{F}{2}\right)\left(\frac{1}{k_a}\right)$

↑ of the whole thing  $\rightarrow k = 2k_a$

↓ In general:  $k_{tot} = k_a + k_b$

For EE's: springs combine like capacitors