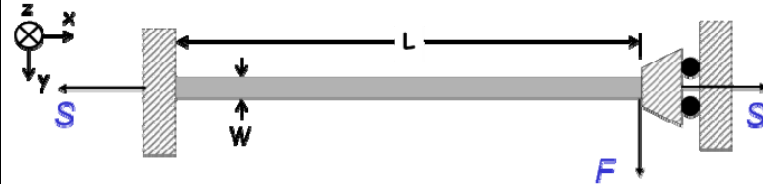


Lecture 17: Beam Combos II

- Announcements:
- No lecture this coming Thursday
 - ↳ We did the make-up for this last Friday
- Unbelievably, both recordings of the Make-Up lecture last Friday didn't work
 - ↳ So again, we only have audio
 - ↳ But there is the Lecture 16 from Fall 2010, which is very similar
 - ↳ So the audio is on the web and there is a link to the YouTube video of the Fall 2010 Lecture 16 that you can view if you missed Friday's lecture
- Midterm is nearing: Thursday, Oct. 27
 - ↳ I passed out materials associated with the midterm, including an information sheet and old exams
- HW#4 due today
- HW#5 online (soon, if not already)
-
- Reading: Senturia, Chpt. 9
- Lecture Topics:
 - ↳ Bending of beams
 - ↳ Cantilever beam under small deflections
 - ↳ Combining cantilevers in series and parallel
 - ↳ Folded suspensions
 - ↳ Design implications of residual stress and stress gradients
-
- Last Time:
- Going through effect of tension on the beam equation

Tensioned Spring (Non-Ideality)

- Important case for MEMS suspensions, since the thin films comprising them are often under residual stress
- Consider small deflection case: $y(x) \ll L$



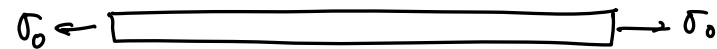
Governing differential equation: (Euler Beam Equation)

$$EI_z \frac{d^4 y}{dx^4} + S \frac{d^2 y}{dx^2} = F \delta(x-L)$$

Axial Load
Unit impulse @ $x=L$

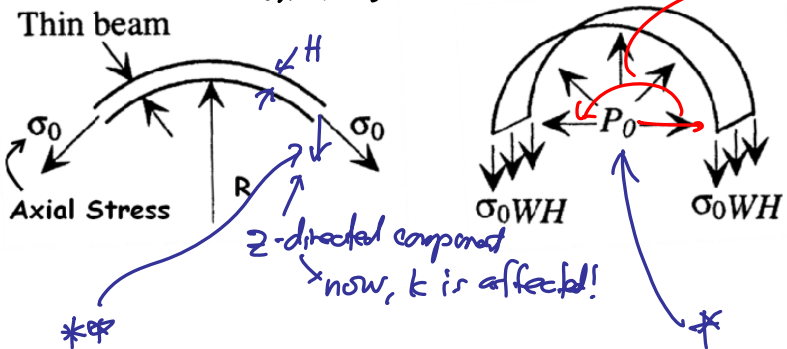
Heuristic Derivation for the Euler Beam Equation

Consider first a straight beam under an axial stress:



⇒ no effect on z-directed stiffness when the beam is straight

...but when the beam is bent:

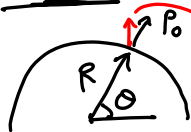


* Upward pressure P_0 to counteract the downward force from $\sigma_0 W H$ to keep everything in static equilibrium

**

For ease of analysis:
Assume the beam is bent to an angle π
Downward radial force: $2\sigma_0 W H$

Upward Force due to P_0 :



$P_{y(\theta)} = P_0 \sin \theta$
 $F_u = \int_0^\pi (P_0 \sin \theta) W(R) d\theta$
 $= -P_0 W R \cos \theta \Big|_0^\pi$
 $= 2 R W P_0$

[Equilibrium] $\Rightarrow 2 R W P_0 = 2 \sigma_0 W H \Rightarrow P_0 = \frac{\sigma_0 H}{R}$

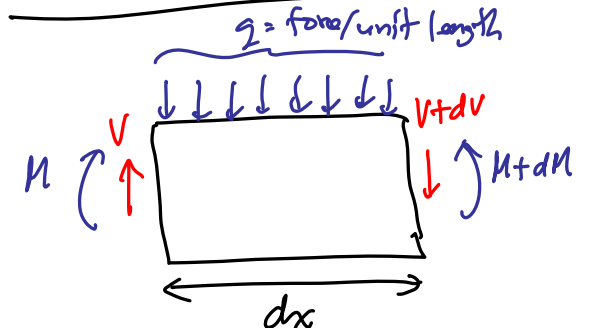
$q_0 = \frac{\text{beam load}}{\text{unit length}} = P_0 W, \frac{1}{R} = \frac{d^2 w}{dx^2}$ beam displacement

generalizer to the case of smaller displacements & angles
 $q_0 = \sigma_0 W H \frac{d^2 w}{dx^2}$

Using the differential beam bending Equation

Equation: $\frac{d^3 w}{dx^3} = \frac{-M}{EI} \rightarrow \frac{d^4 w}{dx^4} = \frac{q}{EI}$ ← load/unit length

* Relationships Between Forces on a Fully Loaded Differential Beam Element



$q = \text{force/unit length}$

[Total Static Equilibrium] \rightarrow total force = 0

$F_T = \text{total force} = q dx + (V+dV) - V = 0$

$\therefore \frac{dV}{dx} = -q$ (1)

\Rightarrow also, total moment wrt to left hand edge = 0

$M_T = (M+dM) - M - (V+dV) dx - \frac{1}{2} q dx^2 = 0$

[neglect product of differentials] $\int_0^{dx} (q du) u = \frac{1}{2} q dx^2$

$dM - V dx = 0 \rightarrow \frac{dM}{dx} = V$ (2)

Using (1) & (2):

$\left[\frac{d^2 M}{dx^2} = \frac{dV}{dx} = -q \right]$

$EI \frac{d^4 w}{dx^4} = q + q_0 \leftarrow \text{equiv. load fr axial stress}$

$(q_0 = \sigma_0 W t \frac{d^2 w}{dx^2}) \Rightarrow$

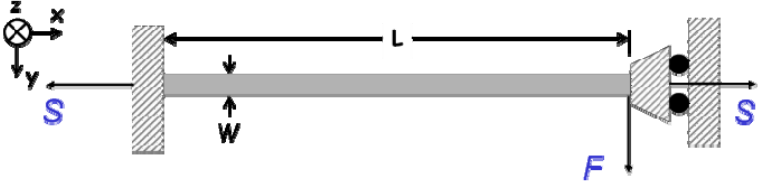
$$EI \frac{d^4 w}{dx^4} - (\sigma_0 W t) \frac{d^2 w}{dx^2} = q$$

\uparrow
 tension in the beam = S
 \uparrow
 a force

\uparrow
Euler Beam Equation

Clamped-Guided Beam Under Axial Load

- Important case for MEMS suspensions, since the thin films comprising them are often under residual stress
- Consider small deflection case: $y(x) \ll L$



Governing differential equation: (Euler Beam Equation)

$$EI_z \frac{d^4 y}{dx^4} - S \frac{d^2 y}{dx^2} = F \delta(x-L)$$

Axial Load Unit impulse @ $x=L$

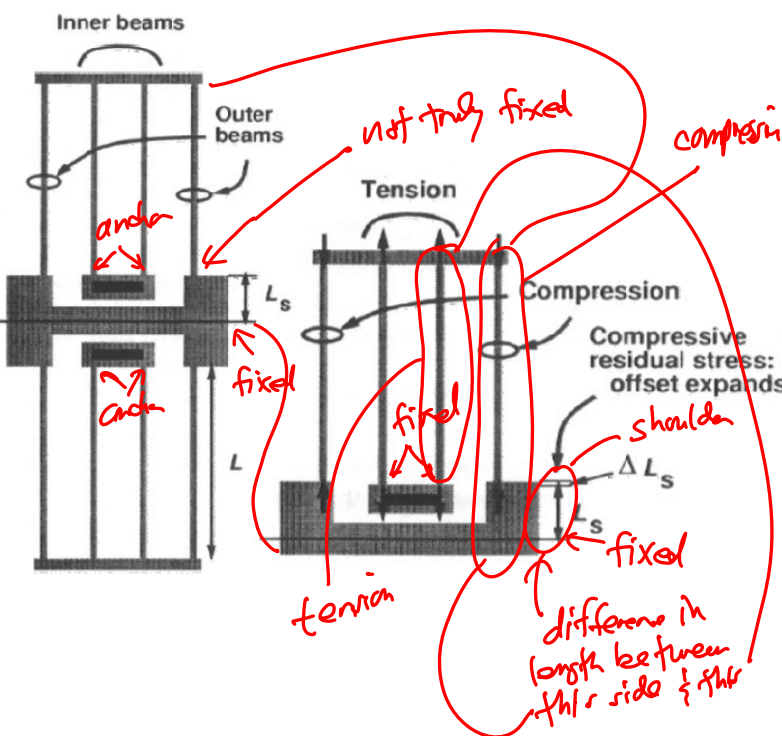
- Can solve the ODE using standard methods
 - ↳ Senturia, pp. 232-235: solves ODE for case of point load on a clamped-clamped beam (which defines B.C.'s)
 - ↳ For solution to the clamped-guided case: see S. Timoshenko, Strength of Materials II: Advanced Theory and Problems, McGraw-Hill, New York, 3rd Ed., 1955
- Result from Timoshenko:

$$S > 0 \text{ (tension)} \quad k^{-1} = \frac{pL - 2 \tanh(pL/2)}{p|S|} = \frac{y(x=L)}{F}$$

$$S < 0 \text{ (compression)} \quad k^{-1} = \frac{-pL + 2 \tan(pL/2)}{p|S|} = \frac{y(x-L)}{F}$$

where $p = \sqrt{\frac{|S|}{EI_z}}$

\uparrow
force



Inner beams Outer beams

Tension Compression

Compressive residual stress: offset expands

shoulder

difference in length between this side & that

① If polysilicon is ϵ_r , then shoulder expands by $\Delta L_s = \epsilon_r L_s$

② This then applies a load to the beams, $\Delta L = \Delta L_s$

③ Beam stress:

$$\epsilon_b = \frac{\Delta L}{2L} = \frac{\Delta L_s}{2L} = \pm \epsilon_r \frac{L_s}{2L}$$

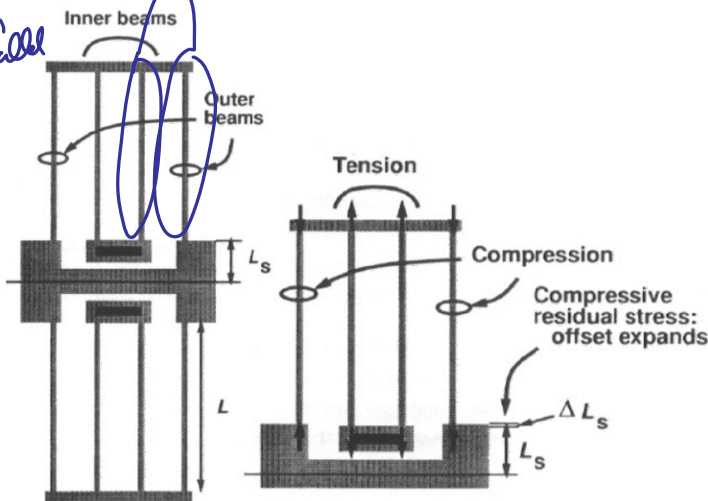
Stress Force: $S = \pm E \epsilon_r \left(\frac{L_s}{2L}\right) W h$ (axial tension)

④ Spring Constants: *series combination of beams*

$$k = 4(k_{com}^{-1} + k_{ten}^{-1})^{-1}$$

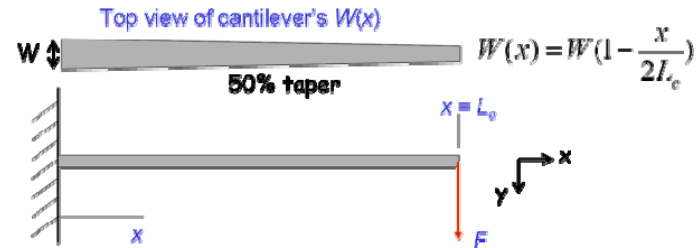
$$k = 4 \left[\frac{-pL + 2 \tan(pL/2)}{p|S|} + \frac{pL - 2 \tanh(pL/2)}{p|S|} \right]^{-1}$$

4 in parallel



More General Geometries

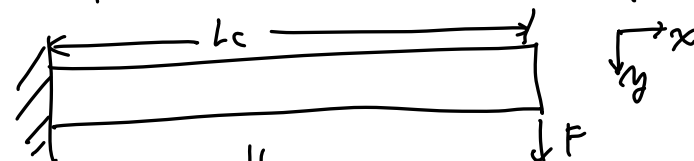
- Euler-Bernoulli beam theory works well for simple geometries
- But how can we handle more complicated ones?
- **Example:** tapered cantilever beam
- **Objective:** Find an expression for displacement as a function of location x under a point load F applied at the tip of the free end of a cantilever with tapered width $W(x)$



Look @ the "Principle of Work Slide" in Module 9.

More Visual Description

Same problem as before: Take a beam, apply a force.



- ① Apply force.
- ② Beam responds by bending.
- ③ This force has done work: $W = F \cdot y(L_c)$
- ④ Strain generated
 ↳ So the beam has received an influx of stored energy
 ↳ magnitude of " " determined by shape

⑤ Then

$$U = \text{Stored Energy} - \text{Work Done} \xrightarrow{\gamma} 0$$

when we choose the
right shape.

↓

This is how we get the
beam's response to F .