



EE C245 - ME C218
Introduction to MEMS Design
Fall 2011

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Lecture Module 5: Surface Micromachining

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Lecture Outline

- Reading: Senturia Chpt. 3, Jaeger Chpt. 11, Handout: "Surface Micromachining for Microelectromechanical Systems"
- Lecture Topics:
 - ↳ Polysilicon surface micromachining
 - ↳ Stiction
 - ↳ Residual stress
 - ↳ Topography issues
 - ↳ Nickel metal surface micromachining
 - ↳ 3D "pop-up" MEMS
 - ↳ Foundry MEMS: the "MUMPS" process
 - ↳ The Sandia SUMMIT process

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Polysilicon Surface-Micromachining

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The diagram illustrates the polysilicon surface-micromachining process. It shows two cross-sectional views of a wafer stack. The top view shows a multi-layer structure with labels: Nitride, Interconnect Polysilicon, Sacrificial Oxide, Structural Polysilicon, Isolation Oxide, and Silicon Substrate. The bottom view shows the same structure after etching, with a green 'Free-Standing Polysilicon Beam' extending from the substrate. A photograph of a micromechanical resonator is shown, labeled '300 kHz Folded-Beam Micromechanical Resonator'. To the right, a bulleted list describes the process:

- Uses IC fabrication instrumentation exclusively
- Variations: sacrificial layer thickness, fine- vs. large-grained polysilicon, *in situ* vs. POCl_3 -doping

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Polysilicon

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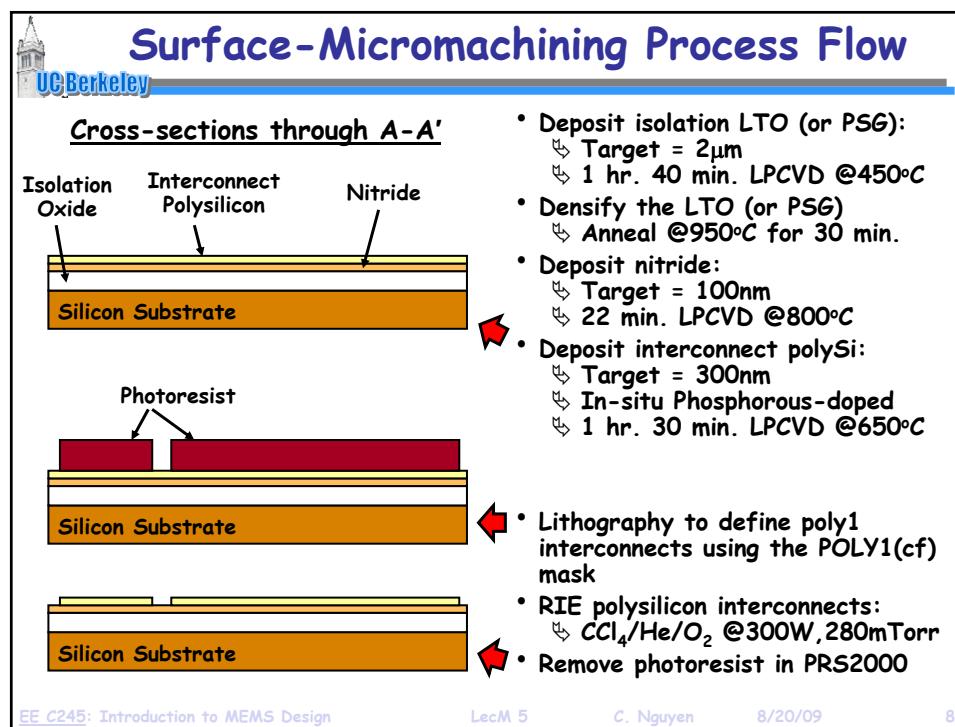
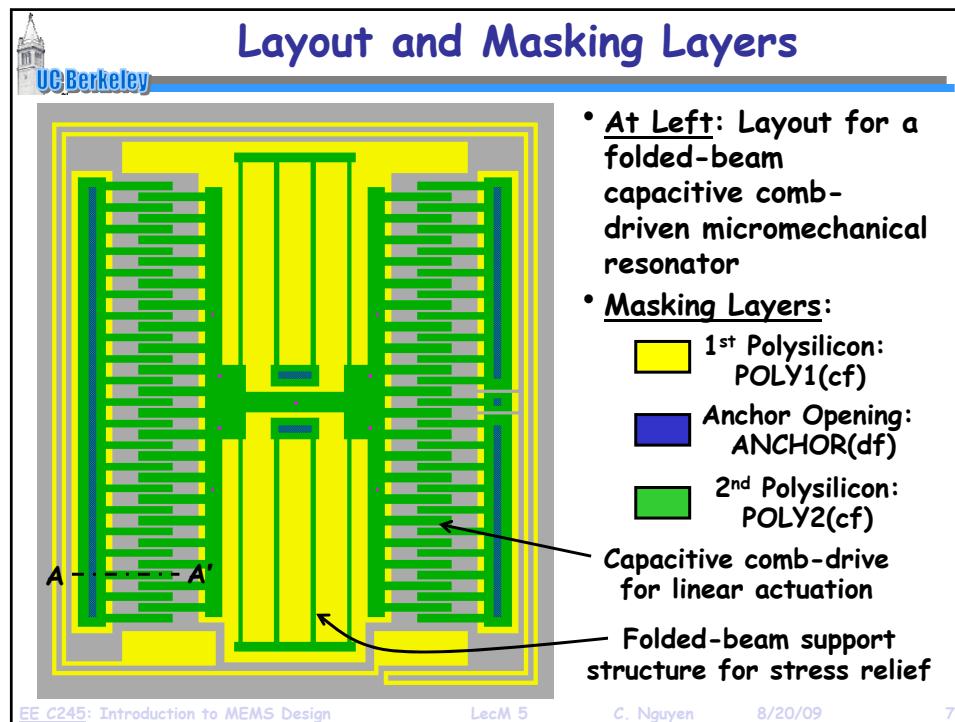
 **Why Polysilicon?**

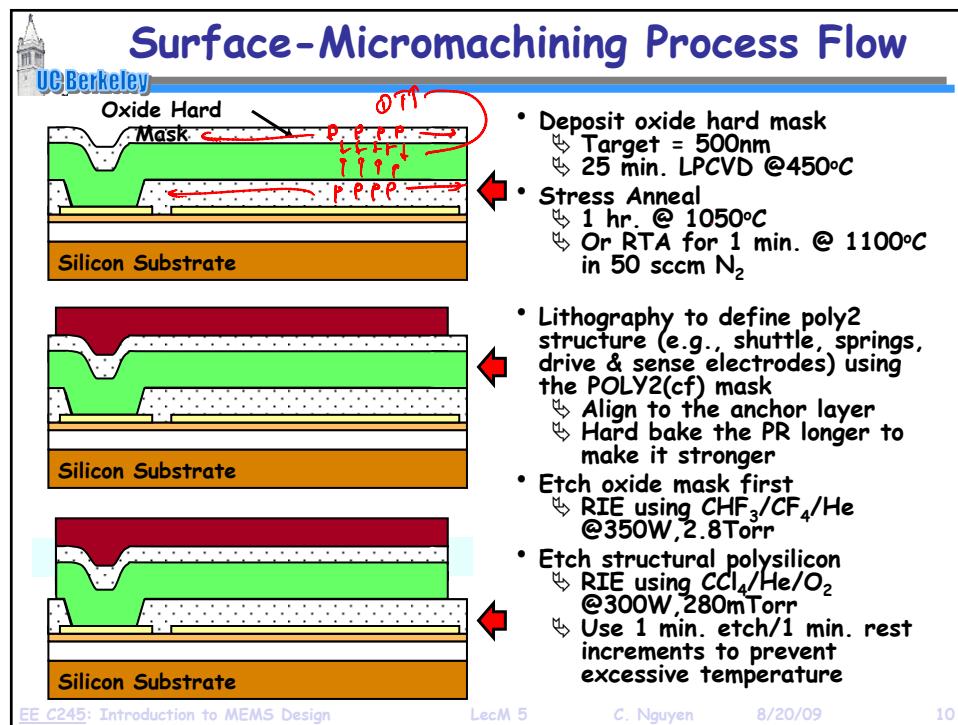
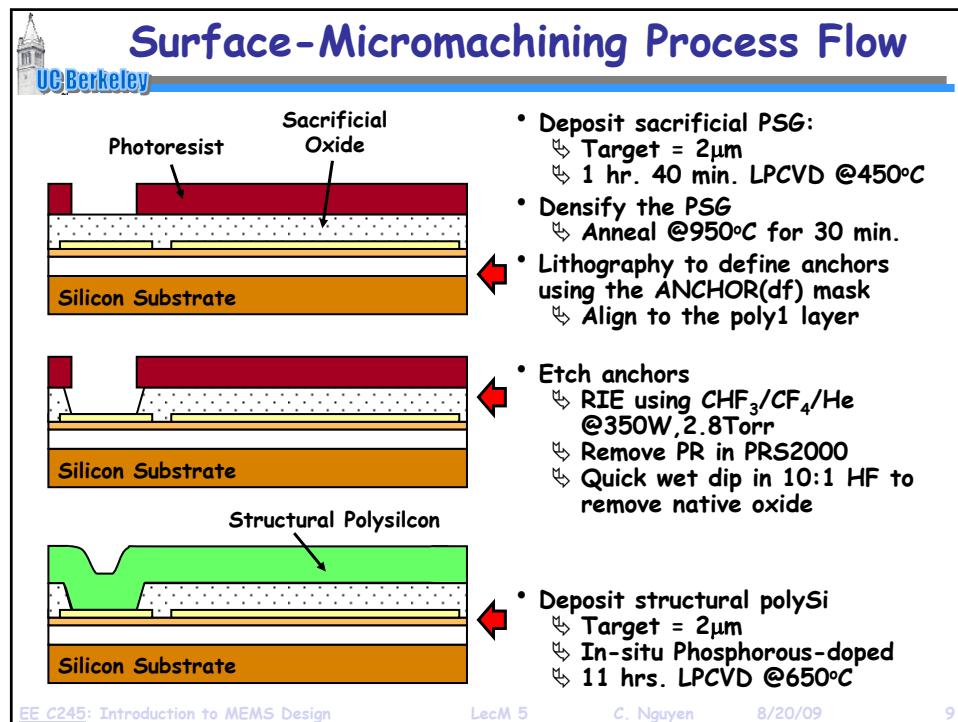
- Compatible with IC fabrication processes
 - ↳ Process parameters for gate polysilicon well known
 - ↳ Only slight alterations needed to control stress for MEMS applications
- Stronger than stainless steel: fracture strength of polySi ~ 2-3 GPa, steel ~ 0.2GPa-1GPa
- Young's Modulus ~ 140-190 GPa
- Extremely flexible: maximum strain before fracture ~ 0.5%
- Does not fatigue readily
- Several variations of polysilicon used for MEMS
 - ↳ LPCVD polysilicon deposited undoped, then doped via ion implantation, PSG source, POCl_3 , or B-source doping
 - ↳ In situ-doped LPCVD polysilicon
 - ↳ Attempts made to use PECVD silicon, but quality not very good (yet) → etches too fast in HF, so release is difficult

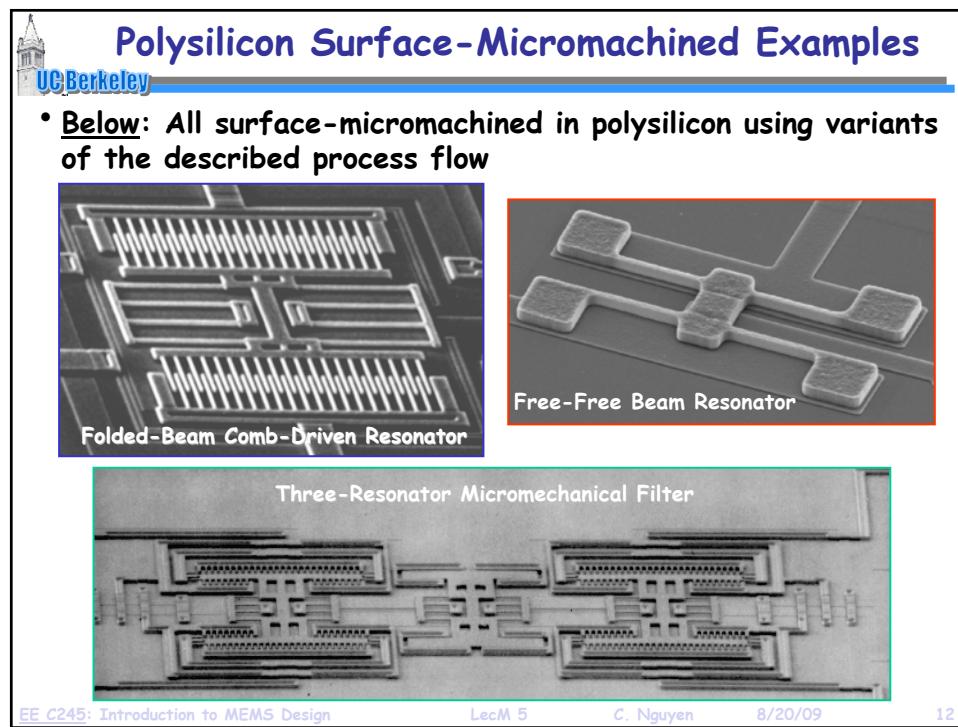
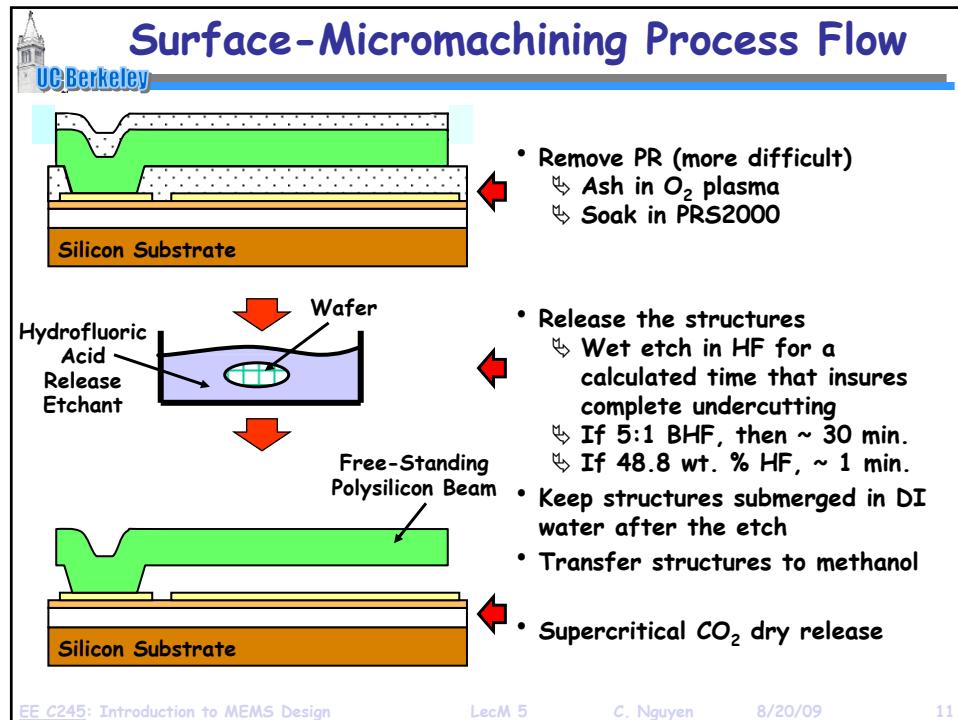
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 **Polysilicon Surface-Micromachining Process Flow**

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| Structural/Sacrificial Material Combinations | | |
|--|-----------------------------|--|
| Structural Material | Sacrificial Material | Etchant |
| Poly-Si | SiO ₂ , PSG, LTO | HF, BHF |
| Al | Photoresist | O ₂ plasma |
| SiO ₂ | Poly-Si | XeF ₂ |
| Al | Si | TMAH, XeF ₂ |
| Poly-SiGe | Poly-Ge | H ₂ O ₂ , hot H ₂ O |

- Must consider other layers, too, as release etchants generally have a finite E.R. on any material
- Ex: concentrated HF (48.8 wt. %)
 - ↳ Polysilicon E.R. ~ 0
 - ↳ Silicon nitride E.R. ~ 1-14 nm/min
 - ↳ Wet thermal SiO₂ ~ 1.8-2.3 μm/min
 - ↳ Annealed PSG ~ 3.6 μm/min
 - ↳ Aluminum (Si rich) ~ 4 nm/min (much faster in other Al)

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| Wet Etch Rates for Micromachining and IC Processing (Å/min) | | | | | | | | | | | | | | | | |
|--|--|----------------------|------------------------|-------------------|---------------------|-----------|--------------|-------------|----------------------|---------------------|---------------------------|-------------------------|------------------------|------------|--------------|--------------|
| ETCHANT EQUIPMENT CONDITIONS | TARGET MATERIAL <100n | MATERIAL | | | | | | | | | | | | | | |
| | | SC Si <100n | Poly n ^a | Poly undep | Wet Ox | Dry Ox | LTO undep | PSG unat | PSG anat | Stoic Nitrid | Low-d Nitrid | 2% Si Teng | Al/ Teng | Spat Ti | Spat Ti/W | OZO EDP/R |
| Concentrated HF (49%) Wet Sink Room Temperature | Silicon oxides | - | 0 | 23k 18k 23k | F >14k | F | 36k | 140 | 52 30 52 | 42 0 42 | <50 | F | - | F 0 | P 0 | |
| 10:1 HF Wet Sink Room Temperature | Silicon oxides | - | 7 | 0 | 230 | 230 | 340 | 15k | 4700 | 11 | 5 2800 2500 12k | 0 | 11k | <70 | 0 | 0 |
| 25:1 HF Wet Sink Room Temperature | Silicon oxides | - | 0 | 0 | 97 | 95 | 150 | W | 1500 | 6 | 1 4 3 4 | W 1400 0.25 20 | 0 | - | - | 0 |
| 5:1 BHF Wet Sink Room Temperature | Silicon oxides | - | 9 | 2 | 1000 900 1080 | 1000 | 1200 | 6800 | 4400 3500 4400 | 9 3 9 24 | 4 1400 0.25 42 | <20 9800 | - | - | 550 390 | 0 |
| Phosphoric Acid (85%) Heated Bath with Reflux 10°C | Silicon oxides | - | 7 | 0 | 0.7 | 0.8 | <1 | 37 | 34 | 28 9 28 42 | 10 9 19 42 | 9800 | - | - | 550 390 | 0 |
| Silicon Dioxane (126 HNO ₃ : 60 H ₂ O : 5 NH ₄ I) Wet Sink Room Temperature | Silicon | 1500 1200 6000 | 3100 | 1000 | 87 | W | 110 | 4000 | 1700 | 2 | 3 4000 | 130 0 | 3000 | - | 0 | 0 |
| KOH (1 KOH : 2 H ₂ O by weight) Heated Stirred Bath 80°C | <100n Silicon | 14k | >10k | F | 77 41 77 | - | 94 | W | 380 | 0 | 0 | F | 0 | - | - | F |
| Aluminum Etchant Type A (16 HNO ₃ : 1 HNO ₂ : 1 HAc : 2 H ₂ O) Heated Bath 50°C | Aluminum | - | <10 | <9 | 0 | 0 | 0 | - | <10 | 0 | 2 6600 2600 6600 | - | 0 | - | 0 | 0 |
| Titanium Etchant (2 H ₂ O : 1 H ₂ O ₂ : 1 HF) Wet Sink Room Temperature | Titanium | - | 12 | - | 120 | W | W | W | 2100 | 8 | 4 W 0 <10 | W 0 100 1000 | 8800 0 60 150 | - | 0 | 0 |
| H ₂ O ₂ (30%) Wet Sink Room Temperature | Tungsten | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | <20 190 190 1000 | 0 60 60 150 | - | <2 | 0 | |
| Piranha (-50 H ₂ SO ₄ : 1 H ₂ O ₂) Heated Bath 120°C | Cleaning off metals and organics | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1800 | - | 2400 | - | F | F |
| Acrosolve Wet Sink Room Temperature | Photoresist | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | >44k >39k | |

Notation: - = not performed; W = not performed, but known to work (> 10 Å/min); F = not performed, but known to be fast (> 10 kÅ/min); P = some of film peeled during etch or when rinsed; A = film was visibly attacked and roughened.
Each entry is all of a 4-4 inch wafer for the transparent films and half of the wafer for single-crystal silicon and the metals.
Each rate will vary with temperature and prior use of solution, area of exposure of film, other materials present (e.g., photoresist), film impurities and microstructures, etc. Some variation should be expected.

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Film Etch Chemistries

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- For some popular films:

| Material | Wet etchant | Etch rate [nm/min] | Dry etchant | Etch rate [nm/min] |
|-----------------|---|--------------------|-------------------------------|--------------------|
| Polysilicon | $\text{HNO}_3:\text{H}_2\text{O}:\text{NH}_4\text{F}$ | 120-600 | $\text{SF}_6 + \text{He}$ | 170-920 |
| Silicon nitride | H_3PO_4 | 5 | SF_6 | 150-250 |
| Silicon dioxide | HF | 20-2000 | $\text{CHF}_3 + \text{O}_2$ | 50-150 |
| Aluminum | $\text{H}_3\text{PO}_4:\text{HNO}_3:\text{CH}_3\text{COOH}$ | 660 | $\text{Cl}_2 + \text{SiCl}_4$ | 100-150 |
| Photoresist | Acetone | >4000 | O_2 | 35-3500 |
| Gold | KI | 40 | n/a | n/a |

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Issues in Surface Micromachining

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- Stiction:** sticking of released devices to the substrate or to other on-chip structures
 - Difficult to tell if a structure is stuck to substrate by just looking through a microscope
- Residual Stress in Thin Films**
 - Causes bending or warping of microstructures
 - Limits the sizes (and sometimes geometries) of structures
- Topography**
 - Stringers can limit the number of structural levels

Beam Stiction
Substrate

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Stringer

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Microstructure Stiction

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Microstructure Stiction

- **Stiction:** the unintended sticking of MEMS surfaces
- **Release stiction:**
 - ↳ Occurs during drying after a wet release etch
 - ↳ Capillary forces of droplets pull surfaces into contact
 - ↳ Very strong sticking forces, e.g., like two microscope slides w/ a droplet between
- **In-use stiction:** when device surfaces adhere during use due to:
 - ↳ Capillary condensation
 - ↳ Electrostatic forces
 - ↳ Hydrogen bonding
 - ↳ Van der Waals forces

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Hydrophilic Versus Hydrophobic

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contact angle

- **Hydrophilic:**
 - ↳ A surface that invites wetting by water
 - ↳ Gets stiction
 - ↳ Occurs when the contact angle $\theta_{\text{water}} < 90^\circ$
- **Hydrophobic:**
 - ↳ A surface that repels wetting by water
 - ↳ Avoids stiction
 - ↳ Occurs when the contact angle $\theta_{\text{water}} > 90^\circ$

Hydrophilic case P_2 d P_1

Hydrophobic case P_2 P_1

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Microstructure Stiction

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Wetted Area A

Microstructures

Contact Angle θ_c

Liquid Layer Thickness g

Force Applied to Maintain Equilibrium F

- Thin liquid layer between two solid plates \Rightarrow adhesive
- If the contact angle between liquid and solid $\theta_c < 90^\circ$:
 - ↳ Pressure inside the liquid is lower than outside
 - ↳ Net attractive force between the plates
- The pressure difference (i.e., force) is given by the Laplace equation

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Microstructure Stiction Modeling

Laplace Equation: Surface Tension @ the Lig.-Air Interface F

$$\Delta P_{la} = \frac{\gamma_{la}}{r} \leftarrow \text{Radius of Curvature of the Liquid-Air Interface}$$

Pressure Difference @ the Meniscus (\hookrightarrow if concave)

$$[r = -\frac{(g/2)}{\cos\theta_c}] \rightarrow F = -\Delta P_{la}A = \frac{2A\gamma_{la}\cos\theta_c}{g}$$

Force needed to keep the plates apart
 $\Rightarrow (+)$ force means a (\hookrightarrow) Laplace pressure

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Avoiding Stiction

- Reduce droplet area via mechanical design approaches
 -
 -
- Avoid liquid-vapor meniscus formation
 - ↳ Use solvents that sublime
 - ↳ Use vapor-phase sacrificial layer etch
- Modify surfaces to change the meniscus shape from concave (small contact angle) to convex (large contact angle)
 - ↳ Use teflon-like films
 - ↳ Use hydrophobic self-assembled monolayers (SAMs)

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Supercritical CO₂ Drying

- A method for stictionless drying of released microstructures by immersing them in CO₂ at its supercritical point
- Basic Strategy: Eliminate surface tension-derived sticking by avoiding a liquid-vapor meniscus
- Procedure:
 - ↳ Etch oxide in solution of HF
 - ↳ Rinse thoroughly in DI water, but do not dry
 - ↳ Transfer the wafer from water to methanol
 - ↳ Displace methanol w/ liquid CO₂
 - ↳ Apply heat & pressure to take the CO₂ past its critical pt.
 - ↳ Vent to lower pressure and allow the supercritical CO₂ to revert to gas → liquid-to-gas transition in supercritical region means no capillary forces to cause stiction

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Hydrophilic Versus Hydrophobic

- Hydrophilic:
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 - ↳ Get stiction
 - ↳ Occurs when the contact angle $\theta_{\text{water}} < 90^\circ$
- Hydrophobic:
 - ↳ A surface that repels wetting by water
 - ↳ Avoids stiction
 - ↳ Occurs when the contact angle $\theta_{\text{water}} > 90^\circ$

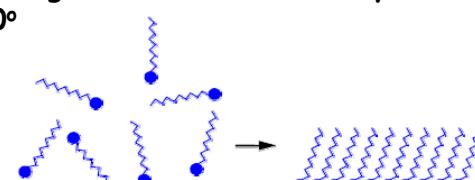
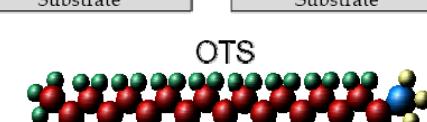
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Tailoring Contact Angle Via SAM's

- Can reduce stiction by tailoring surfaces so that they induce a water contact angle > 90°

Self-Assembled Monolayers (SAM's):

- Monolayers of "stringy" molecules covalently bonded to the surface that then raise the contact angle
- Beneficial characteristics:
 - ↳ Conformal, ultrathin
 - ↳ Low surface energy
 - ↳ Covalent bonding makes them wear resistant
 - ↳ Thermally stable (to a point)

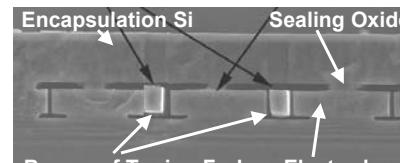



| | θ_{water} |
|---------|---------------------|
| ODT SAM | $112 \pm 0.7^\circ$ |
| SiO_2 | $<10^\circ$ |

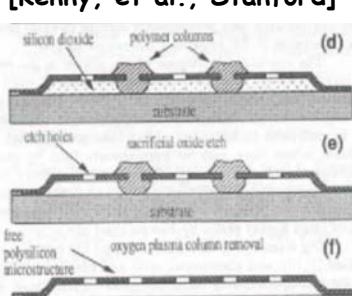
Dry Release

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- Another way to avoid stiction is to use a dry sacrificial layer etch
- For an oxide sacrificial layer
 - use HF vapor phase etching
 - Additional advantage: gas can more easily get into tiny gaps
 - Issue: not always completely dry
→ moisture can still condense → stiction → sln: add alcohol
- For a polymer sacrificial layer
 - Use an O_2 plasma etch (isotropic, so it can undercut well)
 - Issues:
 - Cannot be used when structural material requires high temperature for deposition
 - If all the polymer is not removed, polymer under the suspended structure can still promote stiction



Released via vapor phase HF [Kenny, et al., Stanford]



[Kobayashi]

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Residual Stress

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Residual Stress in Thin Films

- After release, poorly designed microstructures might buckle, bend, or warp → often caused by residual film stress
- Origins of residual stress, σ
 - ↳ Growth processes
 - Non-equilibrium deposition
 - Grain morphology change
 - Gas entrapment
 - Doping
 - ↳ Thermal stresses
 - Thermal expansion mismatch of materials → introduce stress during cool-down after deposition
 - Annealing

Tunable Dielectric Capacitor [Yoon, et al., U. Michigan]

Bending
GSG Pads
Cu Bottom GND
Lateral Spring
Cu Top Electrode
Tunable Dielectric Capacitor [Yoon, et al., U. Michigan]
Buckled Double-Ended Tuning Fork

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Need to Control Film Stress

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- Resonance frequency expression for a lateral resonator:

$$f_0 \approx \frac{1}{2\pi} \sqrt{\frac{4E_y t W^3}{ML^3} + \frac{24\sigma_r t W}{5ML}}$$

Basic term Stress term

Since $W \ll L$, the stress term will dominate if $\sigma_r \sim E_y$

E_y = Young's modulus
 σ_r = stress
 t = thickness
 W = beam width
 L = beam length
 M = mass

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Tensile Versus Compressive Stress

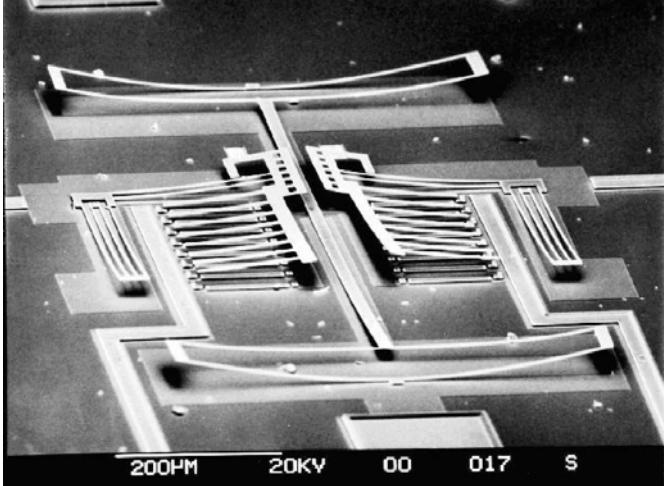
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- Under tensile stress, a film wants to shrink w/r to its substrate
 - ↳ Caused, e.g., by differences in film vs. substrate thermal expansion coefficients
 - ↳ If suspended above a substrate and anchored to it at two points, the film will be "stretched" by the substrate
- Under compressive stress, a film wants to expand w/r to its substrate
 - ↳ If suspended above a substrate and anchored to it at two points, the film will buckle over the substrate

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Vertical Stress Gradients

- Variation of residual stress in the direction of film growth
- Can warp released structures in z-direction



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Stress in Polysilicon Films

- Stress depends on crystal structure, which in turn depends upon the deposition temperature
 - Temperature $\leq 600^{\circ}\text{C}$
 - ↳ Films are initially amorphous, then crystallize
 - ↳ Get equiaxed crystals, largely isotropic
 - ↳ Crystals have higher density \rightarrow tensile stress
 - ↳ Small stress gradient
 - Temperature $\geq 600^{\circ}\text{C}$
 - ↳ Columnar crystals grow during deposition
 - ↳ As crystals grow vertically and in-plane they push on neighbors \rightarrow compressive stress
 - ↳ Positive stress gradient

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Annealing Out Polysilicon Stress

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- Control polySi stress by annealing at high temperatures
 - Typical anneal temperatures: 900-1150°C
 - Grain boundaries move, relax
 - Can dope while annealing by sandwiching the polysilicon between similarly doped oxides (symmetric dopant drive-in), e.g. using 10-15 wt. % PSG

• Rapid thermal anneal (RTA) also effective (surprisingly)

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Topography Issues

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- Degradation of lithographic resolution
 - PR step coverage, streaking
- Stringers
 - Problematic when using anisotropic etching, e.g., RIE

Thickness differences pose problems for reduction steppers

Direction of Spin

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Nickel Surface-Micromachining Process Flow

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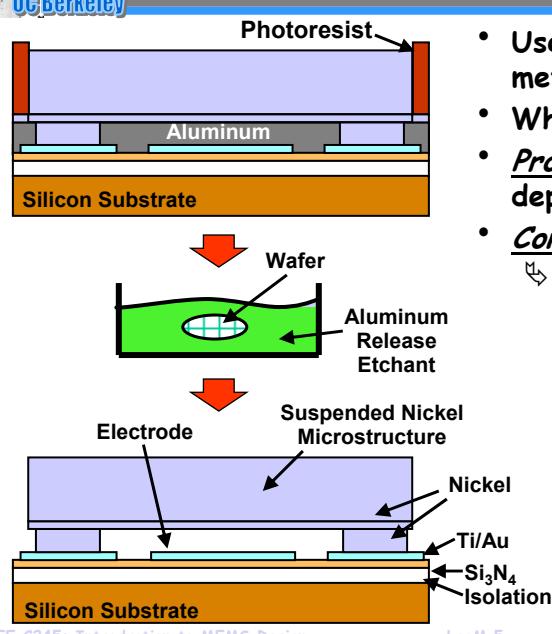
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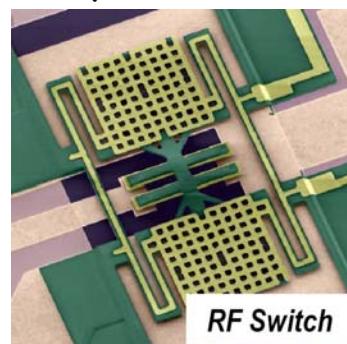
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Electroplating: Metal MEMS



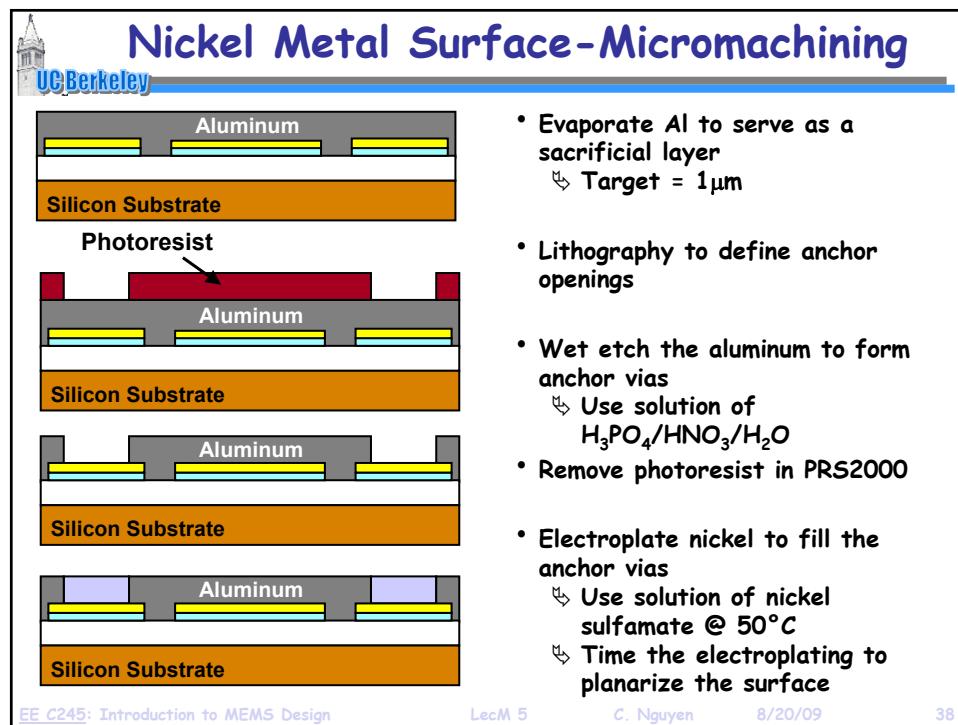
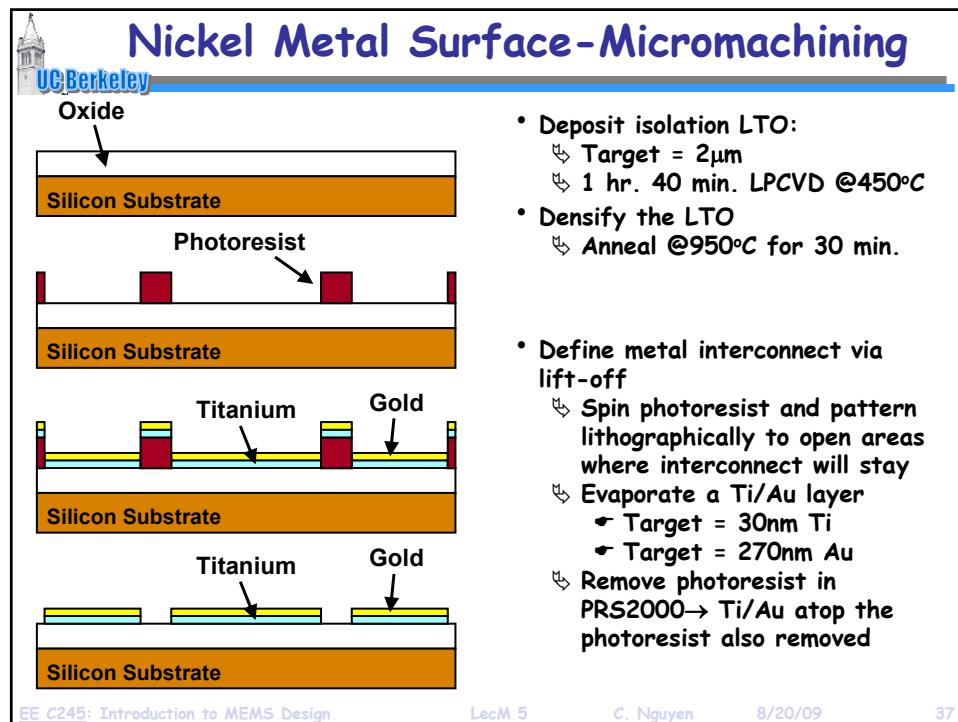
- Use electroplating to obtain metal μstructures
- When thick: call it "LIGA"
- Pros: fast low temp deposition, very conductive
- Cons: drift, low mech. Q
↳ but may be solvable?

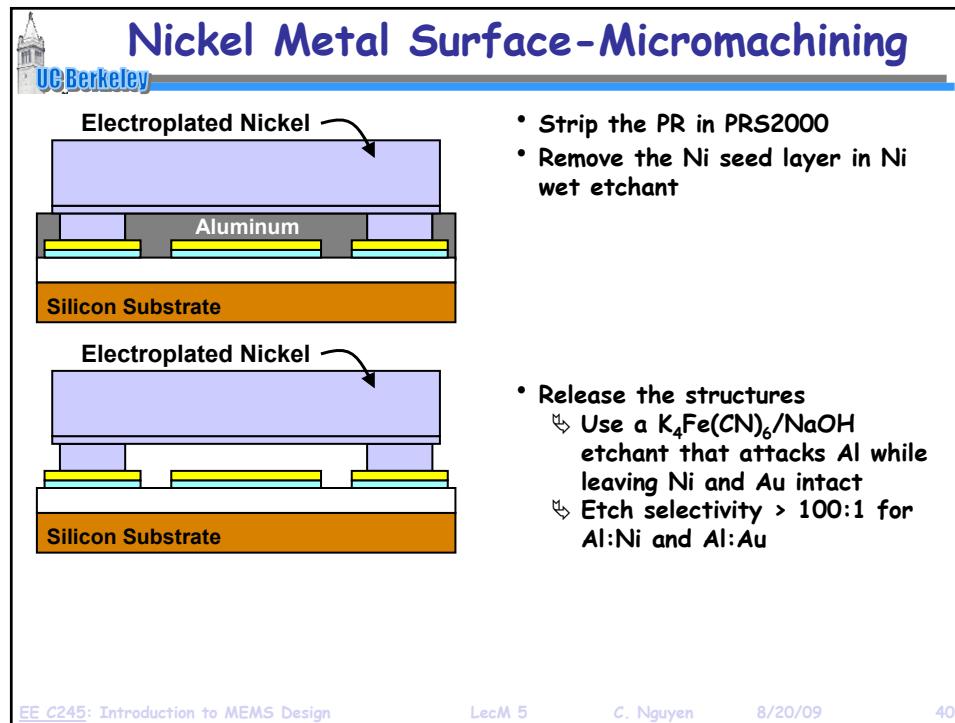
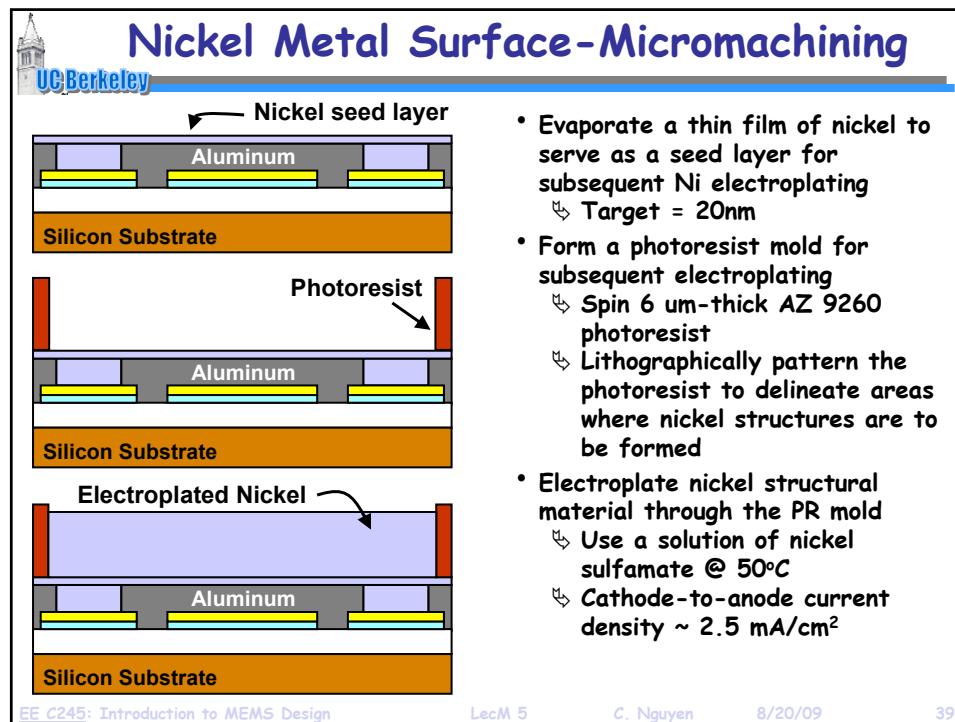


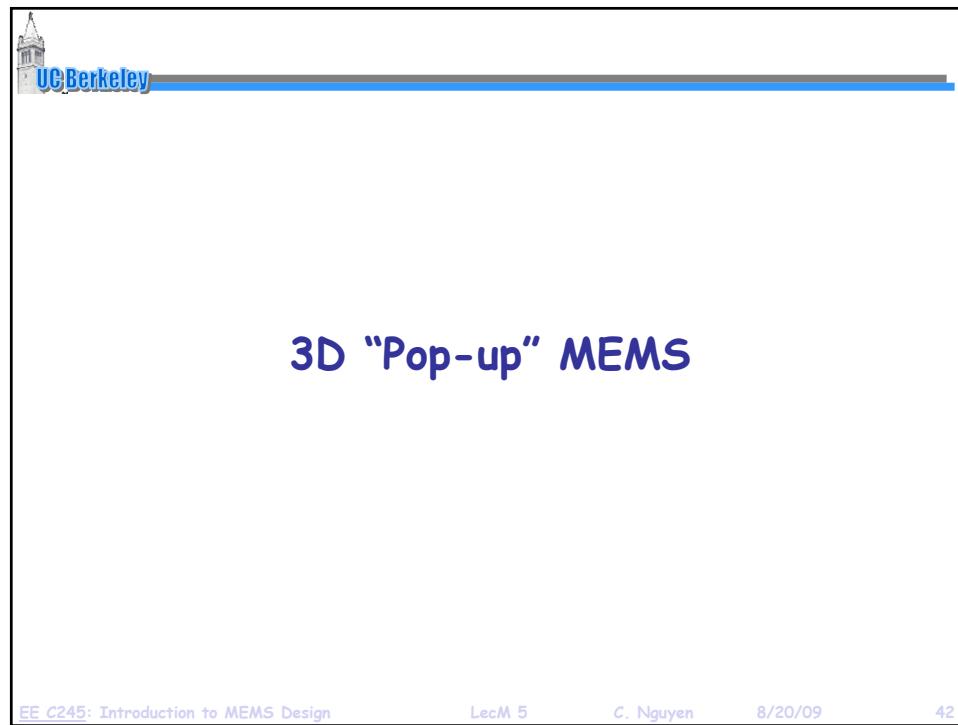
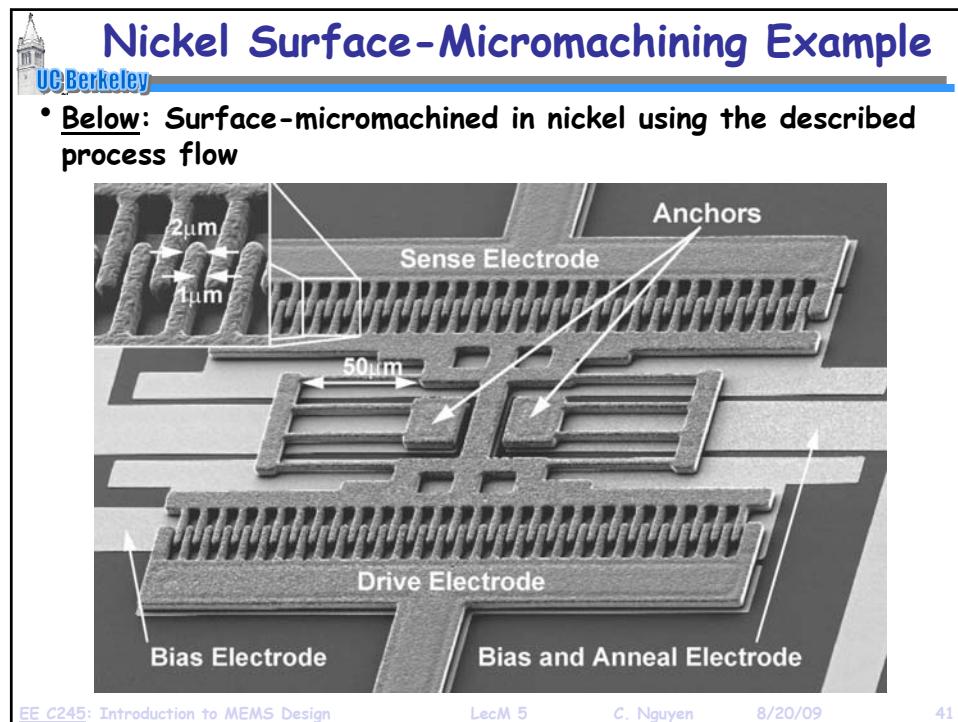
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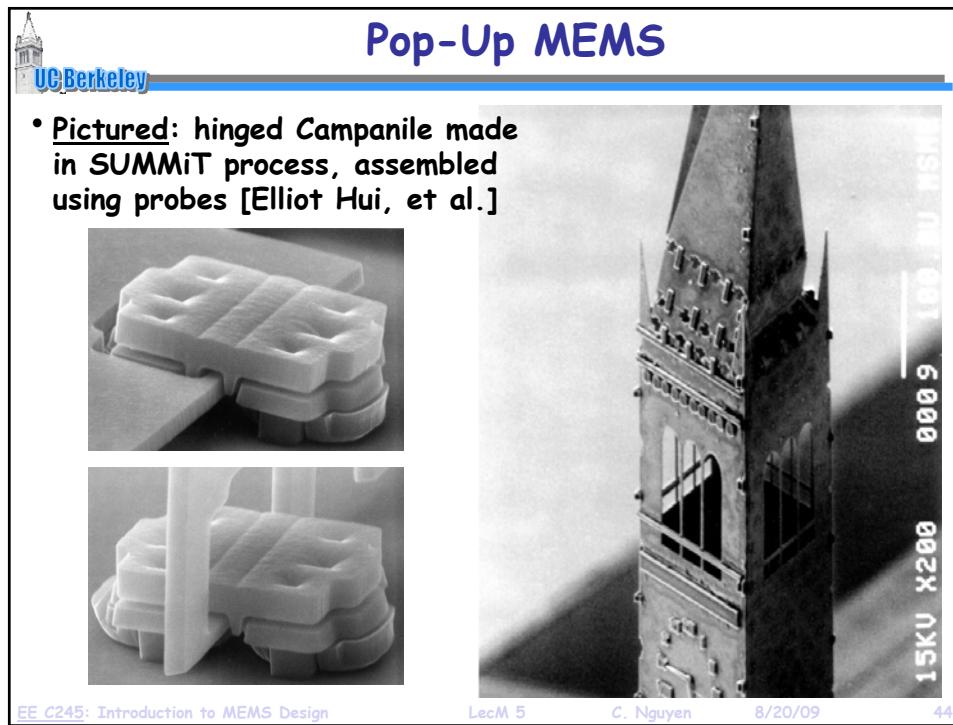
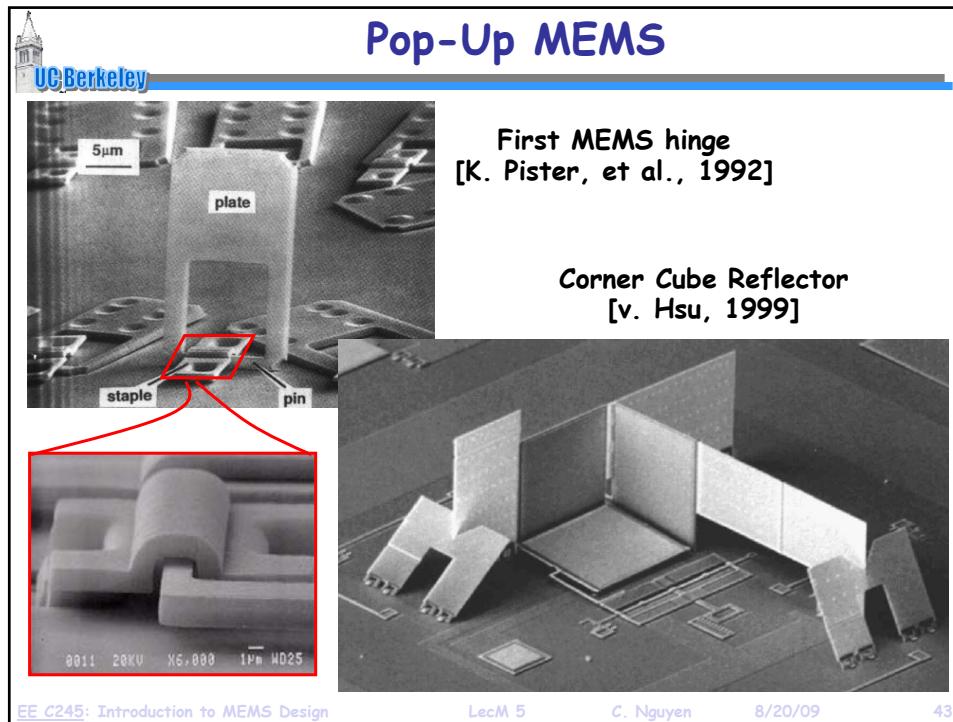
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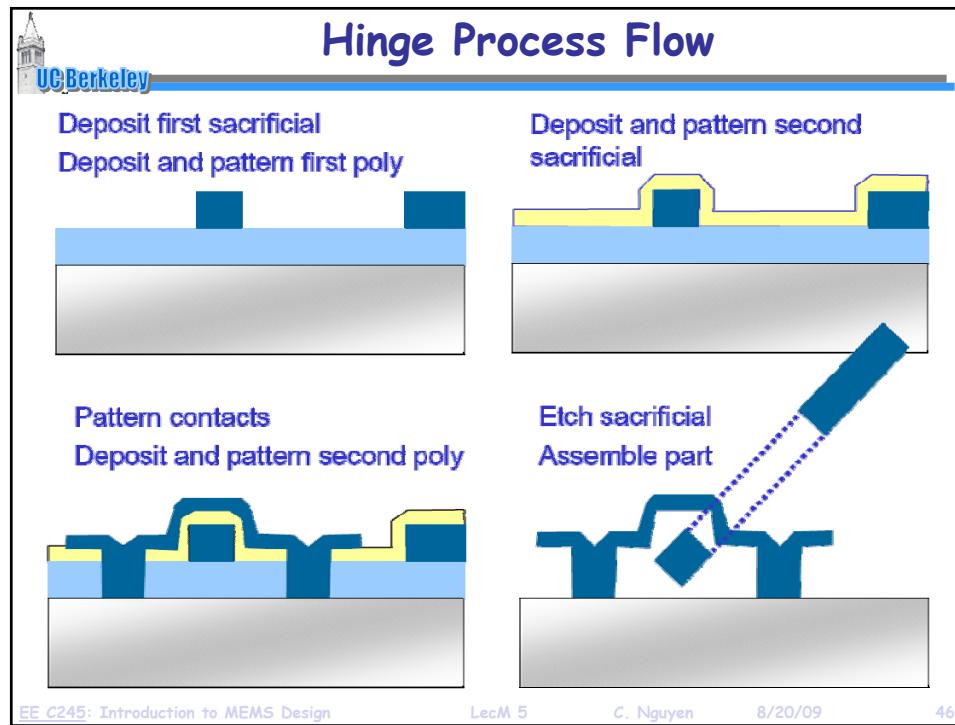
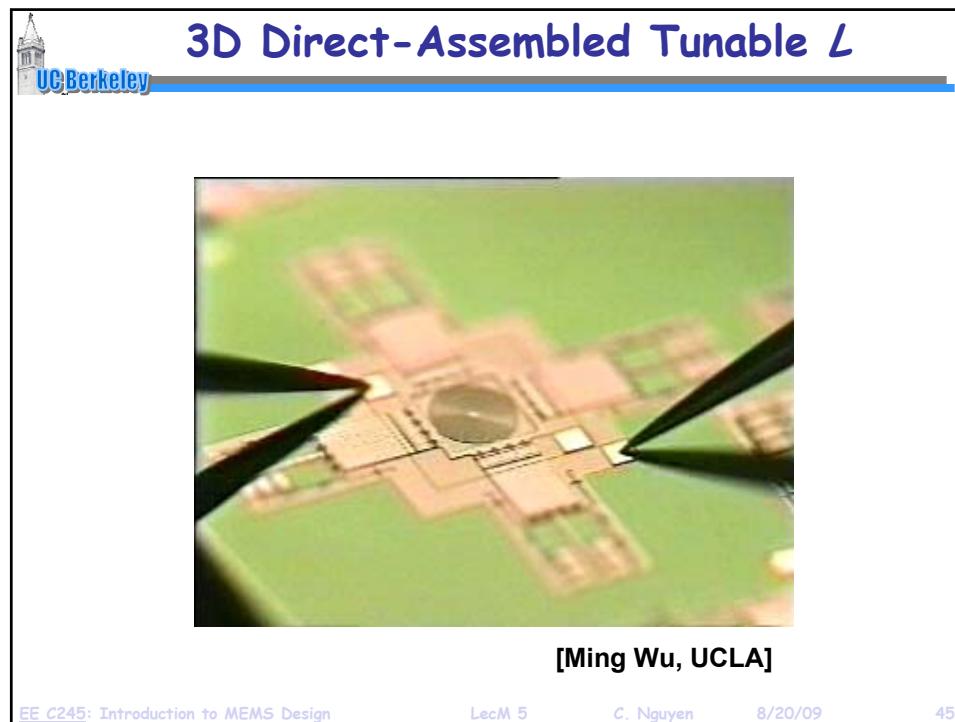
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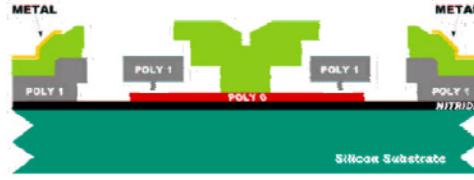
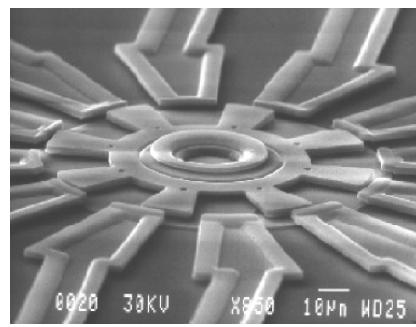
“Foundry” MEMS: The MUMPS Process

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 **MUMPS: MultiUser MEMS ProcesS**

- Originally created by the Microelectronics Center of North Carolina (MCNC) → now owned by MEMSCAP in France
- Three-level polysilicon surface micromachining process for prototyping and “foundry” services
- Designed to service as many users as possible; basically an attempt to provide a universal MEMS process
- 8 photomasks
- \$4,900 for 1 cm² dies

Micromotor fabricated via MUMPS



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MUMPS: MultiUser MEMS Process

| Material Layer | Thickness (μm) | Lithography Level Name |
|----------------|-----------------------------|----------------------------|
| Nitride | 0.6 | -- |
| Poly 0 | 0.5 | POLY0 (HOLE0) |
| First Oxide | 2.0 | DIMPLE ANCHOR1 |
| Poly 1 | 2.0 | POLY1 (HOLE1) |
| Second Oxide | 0.75 | POLY1_POLY2_VIA ANCHOR2 |
| Poly 2 | 1.5 | POLY2 (HOLE2) |
| Metal | 0.5 | METAL (HOLEM) |

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Masks in polyMUMPS

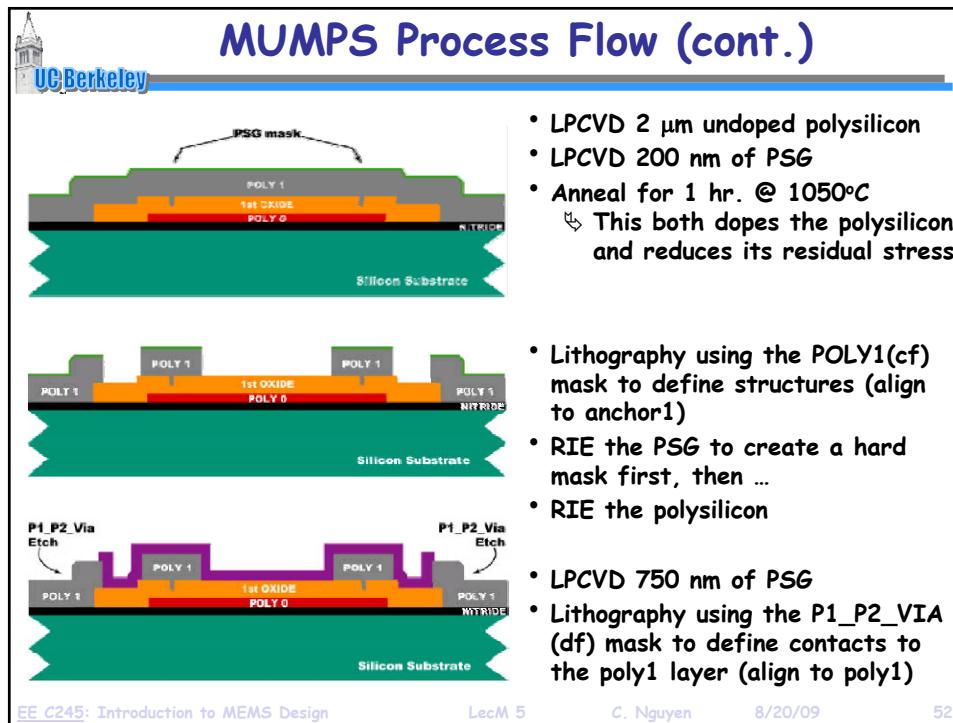
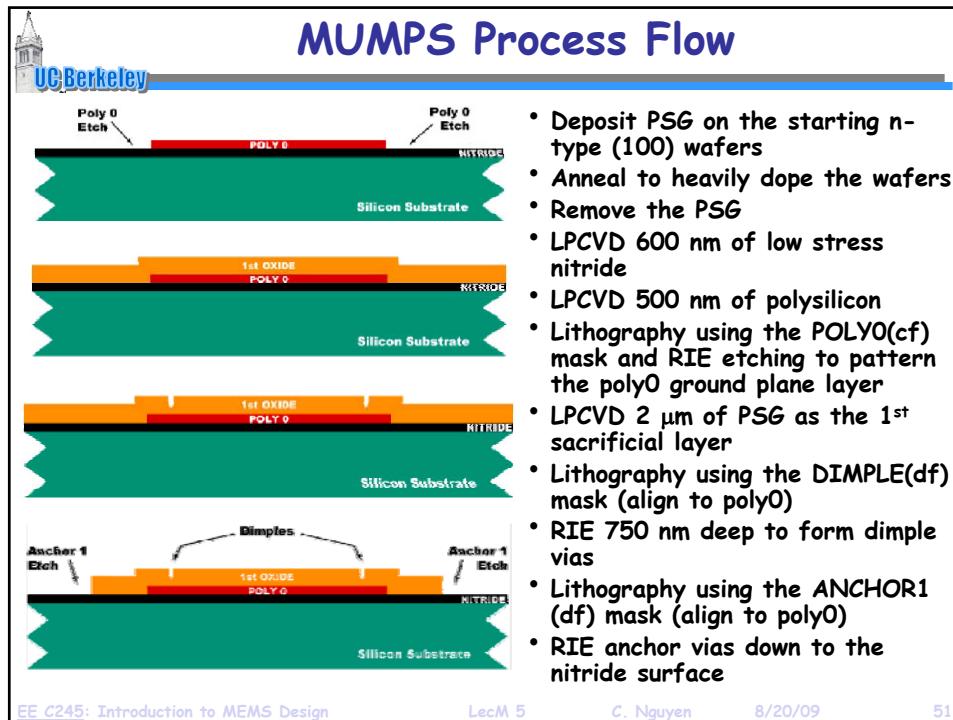
Minimum set of masks that must be used in MUMPS

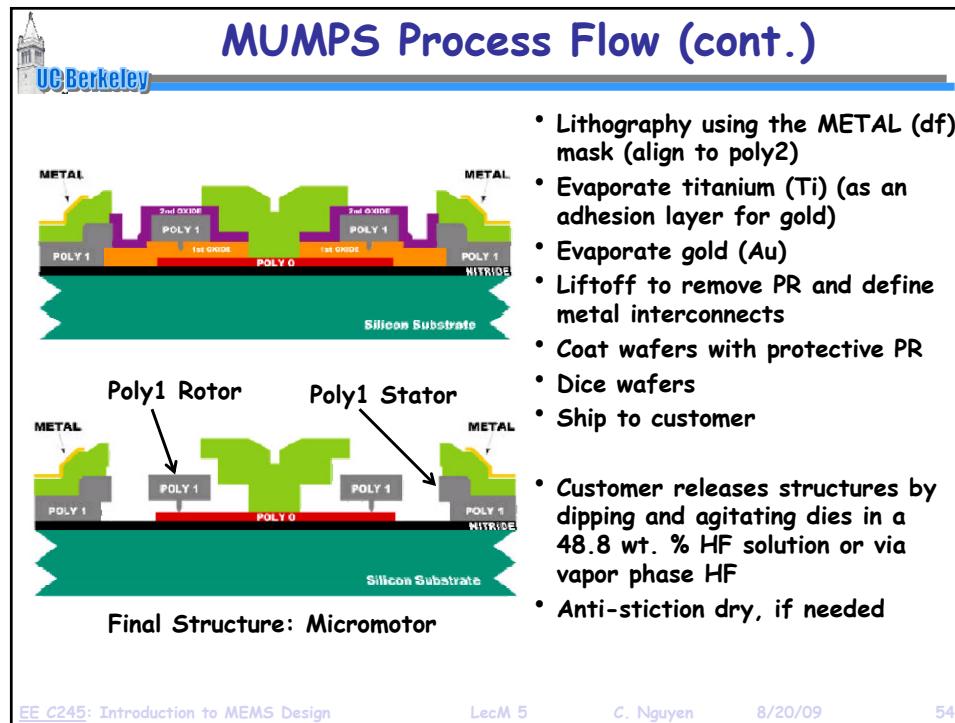
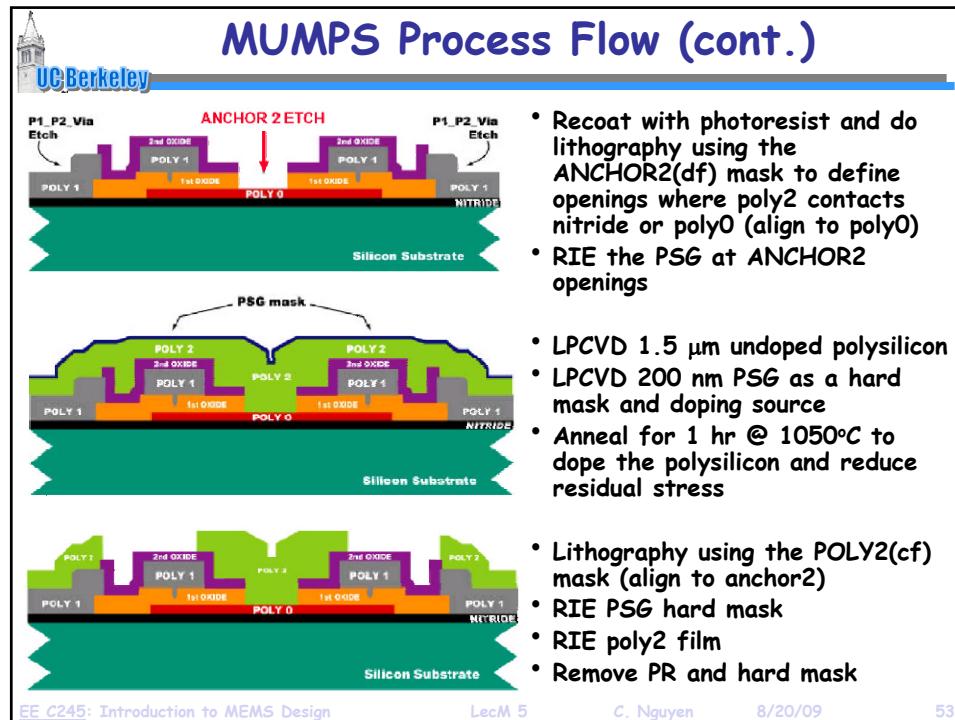
| Mnemonic level name | Field type | Purpose |
|---------------------|------------|---|
| POLY0 | light | pattern ground plane |
| ANCHOR1 | dark | open holes for Poly 1 to Nitride or Poly 0 connection |
| DIMPLE | dark | create dimples/bushings for Poly 1 |
| POLY1 | light | pattern Poly 1 |
| POLY1_POLY2_VIA | dark | open holes for Poly 1 to Poly 2 connection |
| ANCHOR2 | dark | open holes for Poly 2 to Nitride or Poly 0 connection |
| POLY2 | light | pattern Poly 2 |
| METAL | light | pattern Metal |
| HOLE0 | dark | provide holes for POLY0 |
| HOLE1 | dark | provide release holes for POLY1 |
| HOLE2 | dark | provide release holes for POLY2 |
| HOLEM | dark | provide release holes in METAL |

Extra masks for more flexibility & ease of release

- **Field type:**
 - ↳ Light (or clear) field (cf): in layout, boxes represent features that will stay through fabrication
 - ↳ Dark field (df): in layout, boxes represent holes to be cut out

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MUMPS: MultiUser MEMS Process

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- Originally created by the Microelectronics Center of North Carolina (MCNC) → now owned by MEMSCAP in France
- Three-level polysilicon surface micromachining process for prototyping and “foundry” services
- Designed to service as many users as possible; basically an attempt to provide a universal MEMS process
- 8 photomasks
- \$4,900 for 1 cm² dies

Micromotor fabricated via MUMPS

Scanning electron micrograph (SEM) showing a micromotor fabricated via the MUMPS process. The image displays a complex polysilicon structure with a central cavity and radial features. Technical parameters at the bottom of the image are: 0.020, 30KU, X850, 10μm WD25.

METAL
POLY 1
POLY 1
POLY 1
NITRIDE
Silicon Substrate

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polyMUMPS Minimum Feature Constraints

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- Minimum feature size
 - Determined by MUMPS' photolithographic resolution and alignment precision
 - Violations result in missing (unanchored), under/oversized, or fused features
 - Use minimum feature only when absolutely necessary

| | Nominal [μm] | Min Feature [μm] | Min Spacing [μm] |
|---------------------|--------------|------------------|------------------|
| POLY0, POLY1, POLY2 | 3 | 2 | 2 |
| POLY1_POLY2_VIA | 3 | 2 | 2 |
| ANCHOR1, ANCHOR2 | 3 | 3 | 2 |
| DIMPLE | 3 | 2 | 3 |
| METAL | 3 | 3 | 3 |
| HOLE1, HOLE2 | 4 | 3 | 3 |
| HOLEM | 5 | 4 | 4 |

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MUMPS Design Rules (cont.)

| Rule | Rule Letter | Figure # | Min. Value (μm) |
|------------------------|-------------|----------|------------------------------|
| POLY0 space to ANCHOR1 | A | 2.5 | 4.0 |
| POLY0 enclose ANCHOR1 | B | 2.5 | 4.0 |
| POLY0 enclose POLY1 | C | 2.6 | 4.0 |
| POLY0 enclose POLY2 | D | 2.7 | 5.0 |
| POLY0 enclose ANCHOR2 | E | 2.8 | 5.0 |
| POLY0 space to ANCHOR2 | F | 2.8 | 5.0 |

Cross Sections

| | | |
|-------|--------|--------|
| Poly0 | Oxide1 | Oxide2 |
| Poly1 | Poly2 | Meta |

Mask Levels

| | | | |
|-------|---------|-------|-----------------|
| Poly0 | Anchor1 | Poly1 | Poly1-Poly2 Via |
| Poly2 | Anchor2 | Metal | Dimple |

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MUMPS Design Rules (cont.)

| Rule | Min. Value (μm) |
|------------------------------------|------------------------------|
| POLY1 enclose ANCHOR1 | G 4.0 |
| POLY1 enclose DIMPLE | N 4.0 |
| POLY1 enclose POLY1_Poly2_VIA | H 4.0 |
| POLY1 enclose POLY2 | O 4.0 |
| POLY1 space to ANCHOR2 | K 3.0 |
| *Lateral etch holes space in POLY1 | R ≤30 (max. value) |

Cross Sections

| | | |
|-------|--------|--------|
| Poly0 | Oxide1 | Oxide2 |
| Poly1 | Poly2 | Meta |

Mask Levels

| | | | |
|-------|---------|-------|-----------------|
| Poly0 | Anchor1 | Poly1 | Poly1-Poly2 Via |
| Poly2 | Anchor2 | Metal | Dimple |

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MUMPS Design Rules (cont.)



| Rule | Rule Letter | Figure # | Min. Value (μm) |
|------------------------|-------------|----------|------------------------------|
| POLY0 space to ANCHOR1 | A | 2.5 | 4.0 |
| POLY0 enclose ANCHOR1 | B | 2.5 | 4.0 |
| POLY0 enclose POLY1 | C | 2.6 | 4.0 |
| POLY0 enclose POLY2 | D | 2.7 | 5.0 |
| POLY0 enclose ANCHOR2 | E | 2.8 | 5.0 |
| POLY0 space to ANCHOR2 | F | 2.8 | 5.0 |

| Rule | Rule Letter | Figure # | Min. Value (μm) |
|------------------------------------|-------------|-----------|------------------------------|
| POLY1 enclose ANCHOR1 | G | 2.6 | 4.0 |
| POLY1 enclose DIMPLE | N | 2.13 | 4.0 |
| POLY1 enclose POLY1_POLY2_VIA | H | 2.9, 2.11 | 4.0 |
| POLY1 enclose POLY2 | O | 2.14 | 4.0 |
| POLY1 space to ANCHOR2 | K | 2.11 | 3.0 |
| *Lateral etch holes space in POLY1 | R | 2.15 | ≤ 30 (max. value) |

| Rule | Rule Letter | Figure # | Min. Value (μm) |
|------------------------------------|-------------|-----------|------------------------------|
| POLY2 enclose ANCHOR2 | J | 2.7, 2.10 | 5.0 |
| POLY2 enclose POLY1_POLY2_VIA | L | 2.9 | 4.0 |
| POLY2 cut-in POLY1 | P | 2.14 | 5.0 |
| POLY2 cut-out POLY1 | Q | 2.14 | 4.0 |
| POLY2 enclose METAL | M | 2.12 | 3.0 |
| POLY2 space to POLY1 | I | 2.10 | 3.0 |
| HOLE2 enclose HOLE1 | T | 2.16 | 2.0 |
| HOLEM enclose HOLE2 | U | 2.16 | 2.0 |
| *Lateral etch holes space in POLY2 | S | 2.15 | ≤ 30 (max. value) |

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MUMPS Design Rules (cont.)



| Level 1 | Level 2 | Min. Feature | Min. Spacing | Enclose | Spacing | Cut-In | Cut-Out |
|---------|-----------------|--------------|----------------------|----------|----------|----------|----------|
| POLY0 | - | 2 | 2 | | | | |
| | ANCHOR1 | | | 4/B/2.5 | 4/A/2.5 | | |
| | POLY1 | | | 4/C/2.6 | | | |
| | ANCHOR2 | | | 5/E/2.8 | 5/F/2.8 | | |
| | POLY2 | | | 5/D/2.7 | | | |
| POLY1 | - | 2 | 2 / 2.5 ² | | | | |
| | POLY0 | | | | | | |
| | ANCHOR1 | | | 4/G/2.6 | | | |
| | ANCHOR2 | | | | 3/K/2.11 | | |
| | POLY2 | | | 4/O/2.14 | | | |
| | DIMPLE | | | 4/N/2.13 | | | |
| POLY2 | POLY1_POLY2_VIA | | | 4/H/2.9 | | | |
| | - | 2 | 2 / 2.5 ² | | | | |
| | POLY0 | | | | | | |
| | POLY1 | | | | | | |
| | VIA | | | | 3/I/2.10 | 5/P/2.14 | 4/Q/2.14 |
| | ANCHOR2 | | | 4/L/2.9 | | | |
| | METAL | | | 5/J/2.7 | | | |
| HOLEM | HOLE2 | | | 3/M/2.12 | | | |
| | HOLE2 | | | 2/U/2.16 | | | |
| | HOLE1 | | | 2/T/2.16 | | | |

TABLE 2.7. PolyMUMPs design rule reference sheet. Table shows minimum dimensions (μm), rule name, and figure number, respectively.

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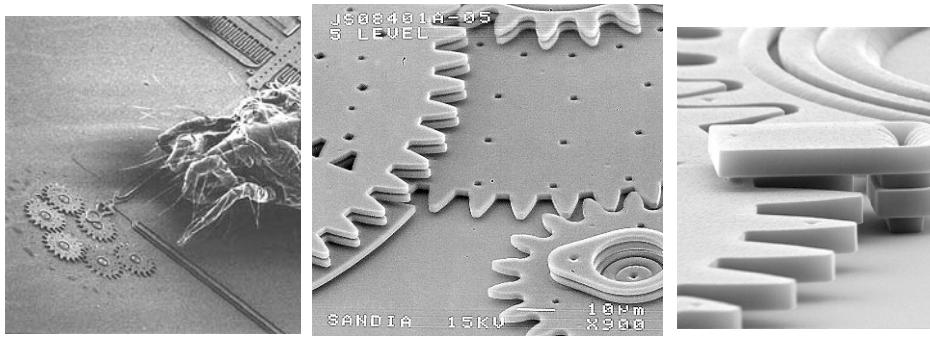
The Sandia SUMMIT Process

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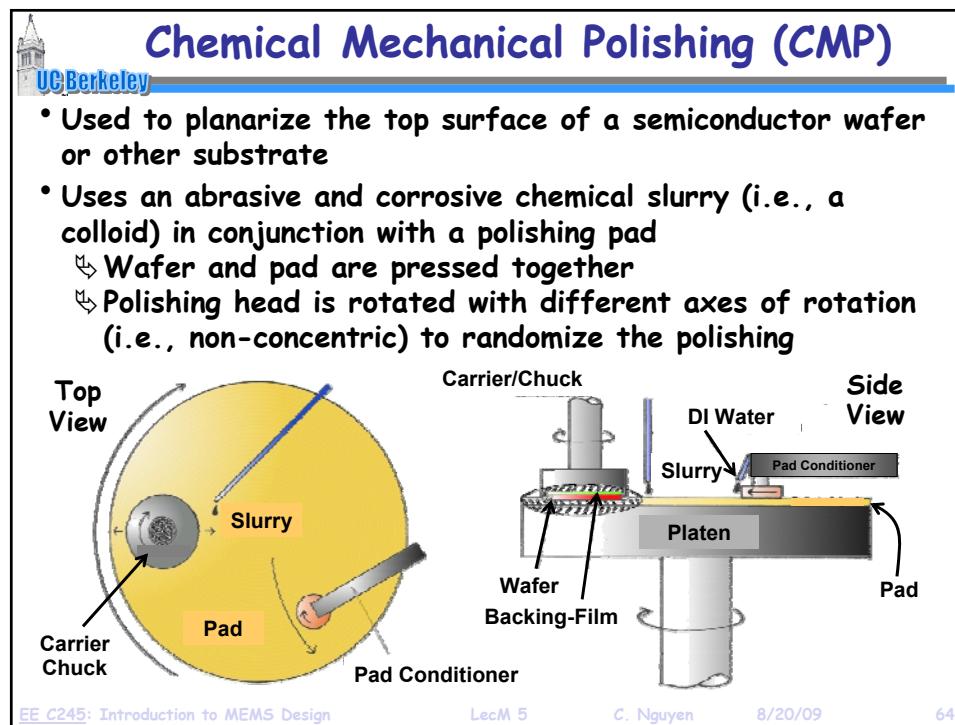
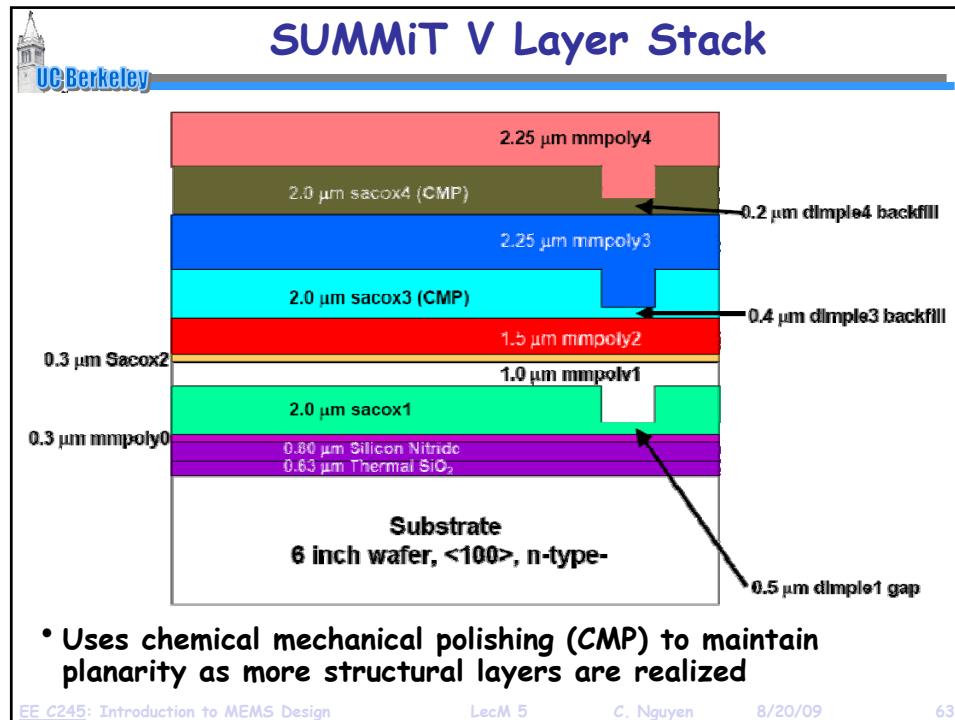
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Sandia's SUMMiT V

- **SUMMiT V:** "Sandia Ultra-planar Multi-level MEMS Technology 5" fabrication process
 - ↳ Five-layer polysilicon surface micromachining process
 - ↳ One electrical interconnect layer & 4 mechanical layers
 - ↳ Uses chemical mechanical polishing (CMP) to maintain planarity as more structural layers are realized
 - ↳ 14 masks



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CMP: Not the Same as Lapping

Lapping

- Lapping is merely the removal of material to flatten a surface without selectivity
- Everything is removed at approximately the same rate

Removes diff. materials at same rate

Chemical Mechanical Polishing

- CMP is selective to certain films, and not selective to others

CMP →

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Actual SUMMiT Cross-Section

• No CMP until after the first three polySi layers

• 1 μm mmpoly1 and 1.5 μm mmpoly2 can be combined to form a 2.5 μm polysilicon film

• Refer to the SUMMiT V manual (one of your handouts) for more detailed information on masks and layout instructions

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