

# EECS 247

## Analog-Digital Interface Integrated Circuits

© 2005

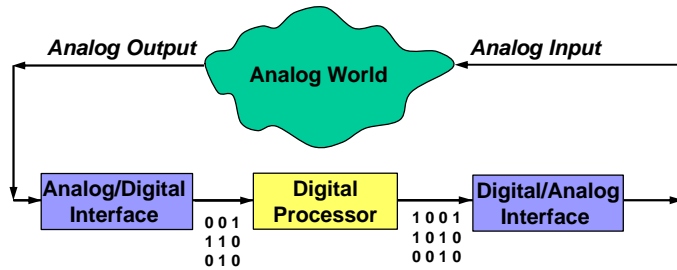
Instructor: Haideh Khorramabadi

UCB  
Department of Electrical Engineering and  
Computer Sciences

## Administrative

- Course web page:  
<http://www.eecs.berkeley.edu/~EE247>
  - All handouts are available on the web
- Office hours for Haideh Khorramabadi
  - Tues./Thurs. 3-4pm @ 485 Cory Hall
  - Email: [haidehk@eecs.berkeley.edu](mailto:haidehk@eecs.berkeley.edu)
- Homework is posted on the course website and is due on Thursdays
- Midterm exam: 10/20/05

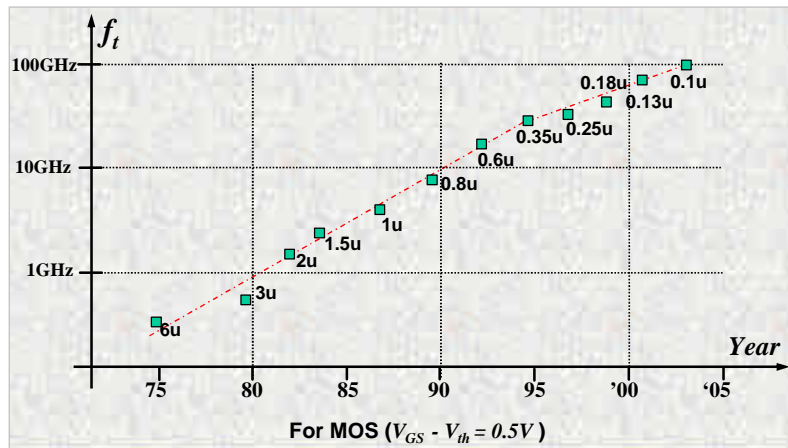
## Analog-Digital Interface Circuits



- Naturally occurring signals are analog  
→ Need Analog/Digital & Digital/Analog interface circuits

Question: Why not process the signal with analog circuits only & thus eliminate need for A/D & D/A?

## MOSFET Maximum $f_t$ versus Time



\*Ref: Paul R. Gray UCB EE290 course '95

International Technology Roadmap for Semiconductors,

<http://public.itrs.net>

## Digital Signal Processing Characteristics

- Direct benefit from the down scaling of VLSI technology
- Not sensitive to “analog” noise
- Enhanced functionality & flexibility
- Amenable to automated design & test
- “Arbitrary” precision
- Provides inexpensive storage capability

## Analog Signal Processing Characteristics

- Has not fully benefited from the down scaling of VLSI technology
  - Supply voltages scale down accordingly
    - Reduced voltage swings
  - Reduced voltage swings requires lowering of the circuit noise to keep a constant dynamic range
    - Higher power dissipation and chip area
- Sensitive to “analog” noise
- Not amenable to automated design
- Extra precision comes at a high price
- Availability of inexpensive digital capabilities on-chip enables automatic adjustments to compensate for analog circuit impairments
- Rapid progress in DSP has imposed higher demands on analog/digital interface circuitry
  - Plenty of room for innovations!

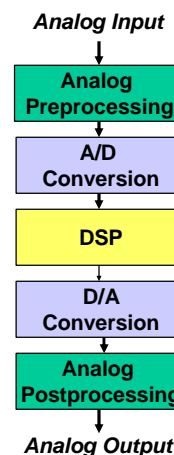
## Cost/Function Comparison DSP & Analog

- Digital circuitry: Fully benefited from CMOS device scaling
  - Cost/function decreases by ~29% each year
    - Cost/function 30X in 10 years\*
- Analog circuitry: Not fully benefited from CMOS scaling
  - Device scaling mandates drop in supply voltages → threaten analog feasibility
    - Cost/function for analog ckt almost constant or increase
- Rapid shift of functions from analog to digital signal processing & hence need for A/D & D/A interface circuitry

\*Ref: International Technology Roadmap for Semiconductors, <http://public.itrs.net>

## Example: Digital Audio

- Goal-Lossless archival and transmission of audio signals
- Circuit functions:
  - Preprocessing
    - Amplification
    - Anti-alias filtering
  - A/D Conversion
    - Resolution → 16Bits
    - Sig. bandwidth → 41kHz
  - DSP
    - Storage
    - Processing (e.g. recognition)
  - D/A Conversion
  - Postprocessing
    - Smoothing filter
    - Variable gain amplification



## Example: Typical Dual Mode Cell Phone



Contains in integrated form:

- 4 Rx filters
  - 4 Tx filters
  - 4 Rx ADCs
  - 4 Tx DACs
  - 3 Auxiliary ADCs
  - 8 Auxiliary DACs
- } Dual Standard, I/Q
- } Audio, Tx/Rx power control, Battery charge control, display, ...

**Total: Filters → 8**

**ADCs → 7**

**DACs → 12**

## Areas Utilizing Analog/Digital Interface Circuitry

- **Communications**
  - Wireline communications
    - Telephone related (DSL, ISDN, CODEC)
    - Television circuitry (Cable modems, TV tuners...)
    - Ethernet (Gigabit, 10/100BaseT...)
  - Wireless
    - Cellular telephone (CDMA, Analog, GSM...)
    - Wireless LAN (Blue tooth, 802.11a/b/g.....)
    - Radio (analog & digital), Television
- **Computing & Control**
  - Storage media (disk drives, digital tape)
  - Imagers & displays
- **Instrumentation**
  - Test equipment
  - Physical sensors & actuators
- **Consumer Electronics**
  - Audio (CD, DAT)
  - Automotive control, appliances, toys

## UCB Analog Courses EECS 247 - 240 - 242

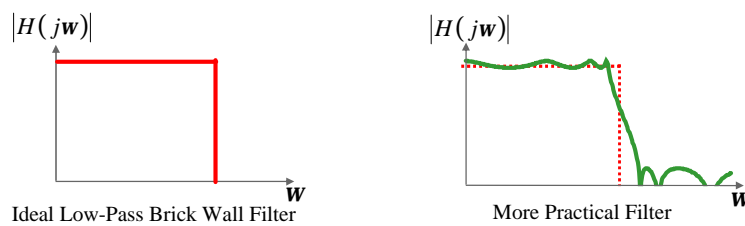
- EECS 247
  - Filters, ADCs, DACs, some system level
  - Signal processing fundamentals
  - Macro-models, large systems, some transistor level, constraints such as finite gain, supply voltage, noise, dynamic range considered
  - CAD Tools → Matlab, SPICE
- EECS 240
  - Transistor level, building blocks such as opamps, buffers, comparator....
  - Device and circuit fundamentals
  - CAD Tools → SPICE
- EECS 242
  - RF amplification, mixing
  - Oscillators
  - Exotic technology devices
  - Nonlinear circuits

## Material Covered in EE247

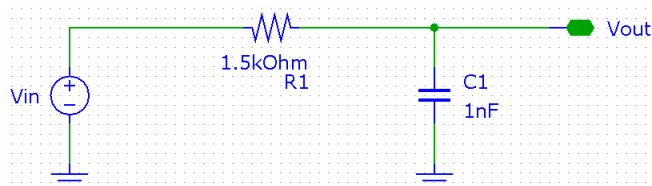
- Filters
  - Continuous-time filters
    - Biquads & ladder type filters
    - Opamp-RC, Opamp-MOSFET-C, gm-C filters
    - Automatic frequency tuning
  - Switched capacitor (SC) filters
- Data Converters
  - D/A converter architectures
  - A/D converter
    - Nyquist rate ADC- Flash, Pipeline ADCs,....
    - Oversampled converters
    - Self-calibration techniques
- Systems utilizing analog/digital interfaces
  - Wireline communication systems- ISDN, XDSL...
  - Wireless communication systems- Wireless LAN, Cellular telephone,...
  - Disk drive electronics
  - Fiber-optics systems

# Introduction to Filters

- Filtering → Frequency-selective signal processing
  - It's the most common type of signal processing
  - Examples:
    - Extraction of desired signal from many (radio)
    - Separating signal and noise
    - Amplifier bandwidth limitations



## Simplest Filter First-Order RC Filter (LPF1)



Steady-state frequency response:

$$H(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{1}{1 + \frac{s}{\omega_0}}$$

with 
$$\omega_0 = \frac{1}{RC} = 2\pi \times 100kHz$$

## Poles and Zeros

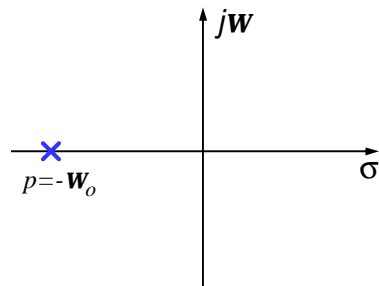
$$H(s) = \frac{1}{1 + \frac{s}{\omega_o}}$$

Pole:  $p = -\omega_o$

Zero:  $z \rightarrow \infty$

$$|H(s)| = \left| \frac{1}{1 + j \frac{\omega}{\omega_o}} \right| = \frac{1}{\sqrt{1 + \frac{\omega^2}{\omega_o^2}}}$$

s-plane (pzmap):



## Filter Frequency Response Bode Plot

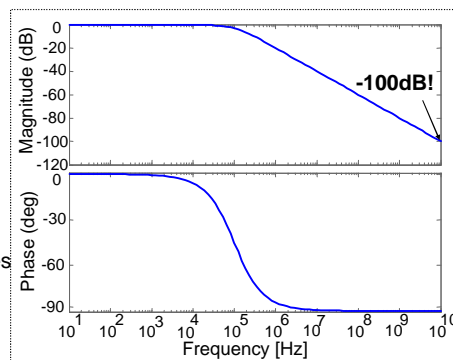
$$|H(s = j\omega)|_{\omega=0} = 1$$

$$|H(s = j\omega)|_{\omega=\omega_o} = 1/\sqrt{2}$$

$$|H(s = j\omega)|_{\omega \rightarrow \infty} = 0$$

Asymptotes:

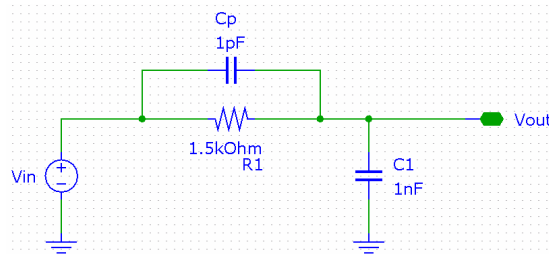
- 20dB/dec magnitude rolloff
- 90degrees phase shift per 2 decades



Question:

can we really get 100dB attenuation at 10GHz?

## First-Order Low-Pass RC Filter Including Parasitics (LPF2)



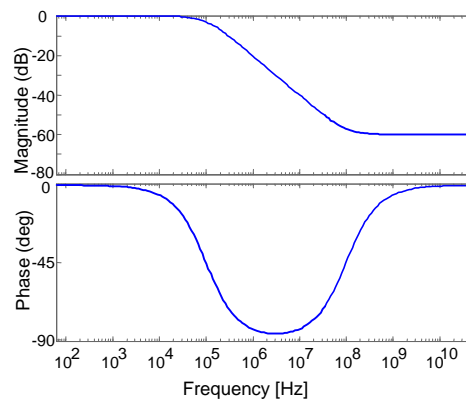
$$H(s) = \frac{1 + sRC_p}{1 + sR(C + C_p)}$$

$$\text{Pole: } p = -\frac{1}{R(C + C_p)} \approx -\frac{1}{RC}$$

$$\text{Zero: } z = -\frac{1}{RC_p}$$

## Filter Frequency Response

$$\begin{aligned} |H(j\omega)|_{\omega=0} &= 1 \\ |H(j\omega)|_{\omega \rightarrow \infty} &= \frac{C_p}{C + C_p} \\ &\approx \frac{C_p}{C} \\ &= 10^{-3} \\ &= -60dB \end{aligned}$$



- Beware of other parasitics not included in this model ...

## Dynamic Range & Electronic Noise

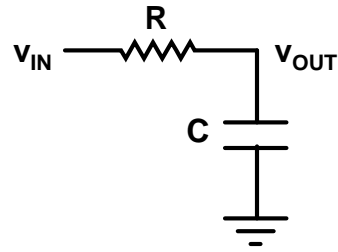
- Dynamic range is defined as the ratio of maximum possible signal handled by a circuit to the minimum useful signal
  - Maximum signal handling capability usually limited by circuit non-linearity & maximum possible voltage swings which in turn is a function of supply voltage
  - Minimum signal handling capability is normally determined by electronic noise
    - Amplifier noise due to device thermal and flicker noise
    - Resistor thermal noise
- Dynamic range in analog ckts has direct implications for power dissipation

## Analog Dynamic Range

- Once the poles and zeroes of the analog filter transfer function are defined then special attention must be paid to the actual implementation
- Of the infinitely many ways to build a filter with a given transfer function, **each of those ways has a different output noise!**
- As an example noise and dynamic range for the 1<sup>st</sup> order lowpass filter will be derived

# First Order Filter Noise

- Capacitors are noiseless
- Resistors have thermal noise
  - This noise is uniformly distributed from dc to infinity
  - Frequency-independent noise is called “white noise”



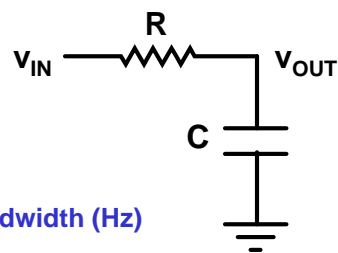
# Resistor Noise

- Resistor noise characteristics
  - A mean value of zero
  - A mean-squared value

$$\overline{v_n^2} = 4k_B T_r R \Delta f$$

Volts<sup>2</sup> (points to  $\overline{v_n^2}$ )  
 absolute temperature (°K) (points to  $T_r$ )  
 ohms (points to  $R$ )  
 measurement bandwidth (Hz) (points to  $\Delta f$ )

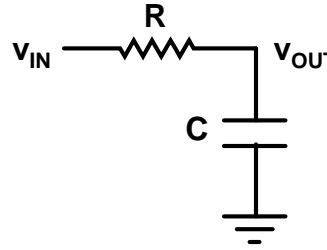
**Boltzmann's constant = 1.38e-23 J/°K**



# Resistor Noise

- Resistor rms noise voltage in a 10Hz band centered at 1kHz is the same as resistor rms noise in a 10Hz band centered at 1GHz
- Resistor noise spectral density,  $N_0$ , is the rms noise per  $\sqrt{\text{Hz}}$  of bandwidth:

$$N_0 = \sqrt{\frac{v_n^2}{\Delta f}} = \sqrt{4k_B T_r R}$$



# Resistor Noise

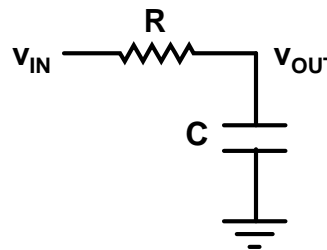
Good numbers to memorize:

- $N_0$  for a **1kW** resistor at room temperature is **4nV/ $\sqrt{\text{Hz}}$**
- Scaling R,
  - A 10M $\Omega$  resistor gives 400nV/ $\sqrt{\text{Hz}}$
  - A 50 $\Omega$  resistor gives 0.9nV/ $\sqrt{\text{Hz}}$
- Or, remember

$$k_B T_r = 4 \times 10^{-21} \text{ J} \quad (T_r = 17 \text{ }^\circ\text{C})$$

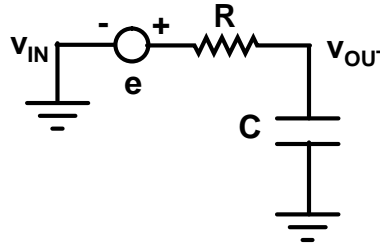
- Or, remember

$$k_B T_r / q = 26 \text{ mV} \quad (q = 1.6 \times 10^{-19} \text{ C})$$



# First Order Filter Noise

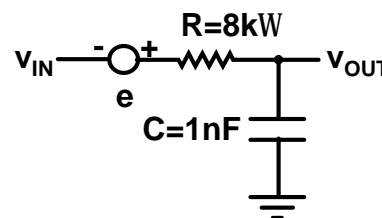
- Short circuit the input to ground.
- Resistor noise gives the filter a non-zero output when  $V_{IN}=0$
- In this simple example, both the input signal and the resistor noise obviously have the same transfer functions to the output
- Since noise has random phase, we can use any polarity convention for a noise source (but we have to use it consistently)



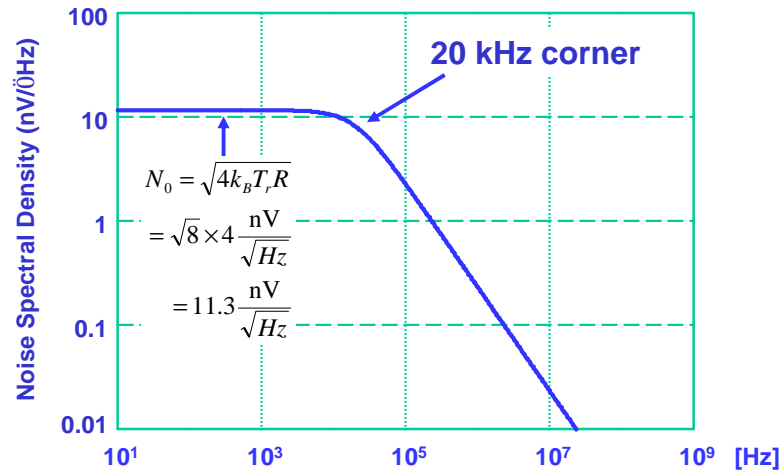
# First Order Filter Noise

- What is the thermal noise of the RC filter?
- Let's ask SPICE!  
Netlist:

```
*Noise from RC LPF
vin vin 0 ac 1V
r1 vin vout 8kOhm
c1 vout 0 1nF
.ac dec 100 10Hz 1GHz
.noise V(vout) vin
.end
```



# LPF1 Output Noise Density



## Total Noise

- Total noise is what the display on a volt-meter connected to  $v_o$  would show!
- Total noise is found by integrating the noise power spectral density with in the frequency band of interest
- Note that noise is integrated in the mean-squared domain, because noise in a bandwidth  $df$  around frequency  $f_1$  is uncorrelated with noise in a bandwidth  $df$  around frequency  $f_2$ 
  - Powers of uncorrelated random variables add
  - Squared transfer functions appear in the mean-squared integral

$$\overline{v_o^2} = \int_{f_1}^{f_2} \overline{v_n^2} |H(j\omega)|^2 df$$

$$\overline{v_o^2} = \int_0^{\infty} 4k_B T R |H(2\pi jf)|^2 df$$

\*Ref: "Analysis & Design of Analog Integrated Circuits", Gray, Hurst, Lewis, Meyer- Chapter 11

# Total Noise

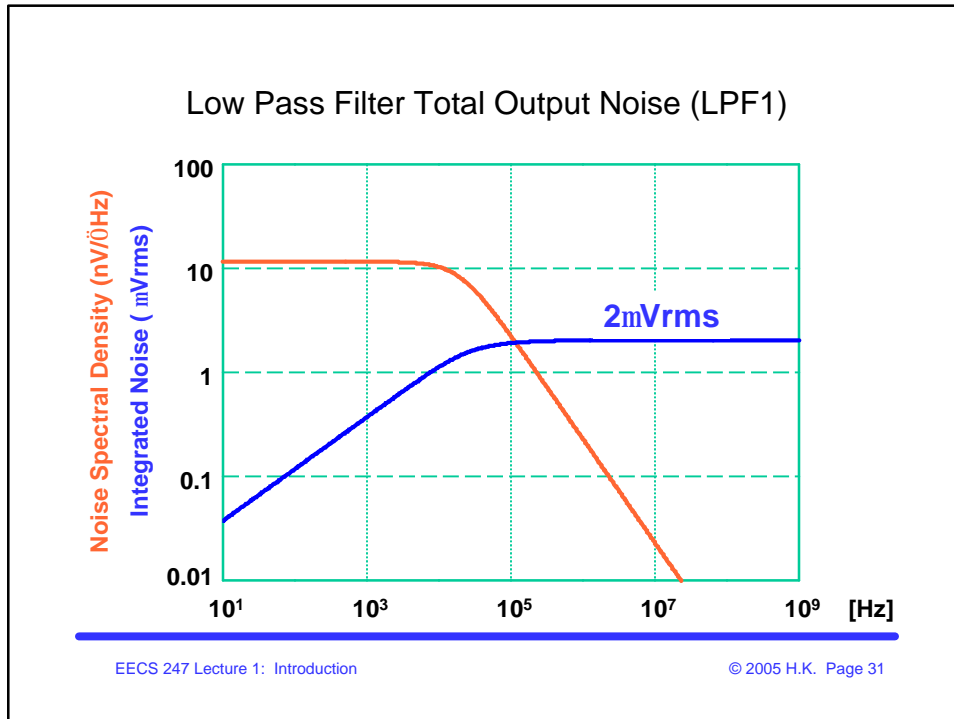
$$\begin{aligned}\overline{v_o^2} &= \int_0^{\infty} 4k_B T R |H(j\omega)|^2 df \\ &= \int_0^{\infty} 4k_B T R \left| \frac{1}{1 + j\omega RC} \right|^2 df \\ &\rightarrow \boxed{\overline{v_o^2} = \frac{k_B T}{C}}\end{aligned}$$

- This interesting and somewhat counter intuitive result means that even though resistors provide the noise sources, total noise is determined by noiseless capacitors!
- For a given capacitance, as resistance goes up, the increase in noise density is balanced by a decrease in noise bandwidth

# kT/C Noise

- kT/C noise is a fundamental analog circuit limitation
- The rms noise voltage of the simplest possible (first order) filter is  $\sqrt{k_B T/C}$
- For 1pF capacitor,  $\sqrt{k_B T/C} = 64 \mu\text{V-rms}$  (at 298°K)
- 1000pF gives 2  $\mu\text{V-rms}$
- The noise of a more complex & higher order filter is given by:  
 $\sqrt{\alpha} \times \sqrt{k_B T/C}$

where  $\alpha$  depends on implementation and features such as filter order

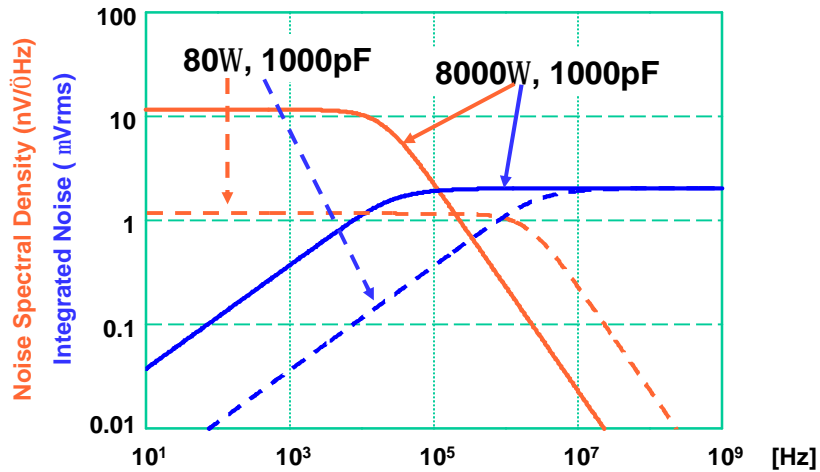


## LPF1 Output Noise

- Note that the integrated noise essentially stops growing above 100kHz for this 20kHz lowpass filter
- Beware of faulty intuition which might tempt you to believe that an 80Ω, 1000pF filter has lower integrated noise compared to our 8000Ω, 1000pF filter...

© 2005 H.K. Page 32

## LPF1 Output Noise



## Analog Circuit Dynamic Range

- Maximum voltage swing for analog circuits can at most be equal to power supply voltage  $V_{DD}$  (normally is smaller)
- Assuming a sinusoid signal

$$V_{\max}(rms) = \frac{1}{\sqrt{2}} \frac{V_{DD}}{2}$$

- Noise for a filter:

$$V_n(rms) = \sqrt{a \frac{k_B T}{C}}$$

$$D.R. = \frac{V_{\max}(rms)}{V_n(rms)} = \frac{V_{DD} \sqrt{C}}{\sqrt{8ak_B T}} \quad [V/V]$$

→ Dynamic range in dB is:

$$= 20 \log_{10} \left( V_{DD} \sqrt{\frac{C}{a}} \right) + 75 \quad [\text{dB}] \quad \text{with } C \text{ in [pF]}$$

## Analog Circuit Dynamic Range

- For integrated circuits built in modern CMOS processes,  $V_{DD} < 3V$  and  $C < 100pF$  ( $a = 1$ )
  - $D.R. < 104 dB$
- For PC board circuits built with “old-fashioned”  $30V$  opamps and discrete capacitors of  $< 100nF$ 
  - $D.R. < 140dB$
  - A  $36dB$  advantage!

## Dynamic Range versus Number of Bits

- Number of bits and dB are related:
$$D.R. = (1.76 + 6.02N) [dB] \quad N \rightarrow \text{number of bits}$$
  - see “quantization noise”, later in the course
- Hence

$104 dB$	$\rightarrow$	$17 Bits$
$140 dB$	$\rightarrow$	$23 Bits$

## Dynamic Range versus Power Dissipation

- Each extra bit corresponds to 6dB
- Increasing dynamic range by one bit → 6dB less noise → decrease in noise power by 4!
- This translates into 4x larger capacitors
- To drive these at the same speed,  $G_m$  must increase 4x
- Power is proportional to  $G_m$  (for fixed supply and  $V_{dsat}$ )

In analog circuits with performance limited by thermal noise,

**1 extra bit costs 4x power**

E.g. 16Bit ADC at 200mW → 17Bit ADC at 800mW

**Do not overdesign the dynamic range of analog circuits!**

## Noise Summary

- Thermal noise is a fundamental property of (electronic) circuits
- Noise is closely related to
  - Capacitor size
- In higher order filters, noise is proportional to C, filter order, Q, and depends on implementation
- Operational amplifiers can contribute significant levels of extra noise to overall filter noise
- Reducing noise in most analog circuits costs in terms of power dissipation and chip area