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Microstructure Stiction

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Microstructure Stiction

- **Stiction:** the unintended sticking of MEMS surfaces
- **Release stiction:**
 - ↳ Occurs during drying after a wet release etch
 - ↳ Capillary forces of droplets pull surfaces into contact
 - ↳ Very strong sticking forces, e.g., like two microscope slides w/ a droplet between
- **In-use stiction:** when device surfaces adhere during use due to:
 - ↳ Capillary condensation
 - ↳ Electrostatic forces
 - ↳ Hydrogen bonding
 - ↳ Van der Waals forces

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Hydrophilic Versus Hydrophobic

contact angle

- **Hydrophilic:**
 - ↳ $\theta_c < 90^\circ$
 - ↳ A surface that invites wetting by water
 - ↳ Get stiction
 - ↳ Occurs when the contact angle $\theta_{\text{water}} < 90^\circ$
- **Hydrophobic:**
 - ↳ A surface that repels wetting by water
 - ↳ Avoids stiction
 - ↳ Occurs when the contact angle $\theta_{\text{water}} > 90^\circ$

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Microstructure Stiction

- Thin liquid layer between two solid plates \Rightarrow adhesive
- If the contact angle between liquid and solid $\theta_c < 90^\circ$:
 - ↳ Pressure inside the liquid is lower than outside
 - ↳ Net attractive force between the plates
- The pressure difference (i.e., force) is given by the Laplace equation

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Microstructure Stiction Modeling

Laplace Equation: Surface Tension @ the Liq.-Air Interface

$$\Delta p_{la} = \frac{2\gamma_{la}}{r}$$

r ← Radius of Curvature of the Meniscus (-) if concave

Pressure Difference @ the Liquid-Air Interface

$$[r = -\frac{(g/2)}{\cos\theta_c}] \Rightarrow F = -\Delta p_{la} A = \frac{2A\gamma_{la}\cos\theta_c}{g}$$

Force needed to keep the plates apart
 \Rightarrow (+) force means g
 \Rightarrow (-) Laplace pressure

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Avoiding Stiction

- Reduce droplet area via mechanical design approaches

- Avoid liquid-vapor meniscus formation
 - Use solvents that sublime
 - Use vapor-phase sacrificial layer etch
- Modify surfaces to change the meniscus shape from concave (small contact angle) to convex (large contact angle)
 - Use teflon-like films
 - Use hydrophobic self-assembled monolayers (SAMs)

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Supercritical CO₂ Drying

- A method for stictionless drying of released microstructures by immersing them in CO₂ at its supercritical point
- Basic Strategy:** Eliminate surface tension-derived sticking by avoiding a liquid-vapor meniscus
- Procedure:**
 - Etch oxide in solution of HF
 - Rinse thoroughly in DI water, but do not dry
 - Transfer the wafer from water to methanol
 - Displace methanol w/ liquid CO₂
 - Apply heat & pressure to take the CO₂ past its critical pt.
 - Vent to lower pressure and allow the supercritical CO₂ to revert to gas → liquid-to-gas Xsition in supercritical region means no capillary forces to cause stiction

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Hydrophilic Versus Hydrophobic

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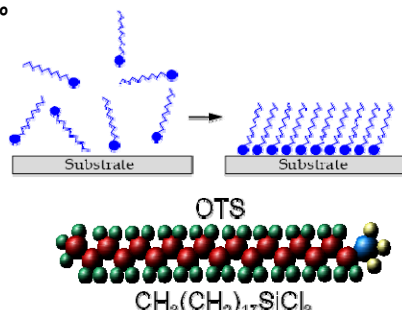
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Tailoring Contact Angle Via SAM's

- Can reduce stiction by tailoring surfaces so that they induce a water contact angle $> 90^\circ$

Self-Assembled Monolayers (SAM's):

- Monolayers of "stringy" molecules covalently bonded to the surface that then raise the contact angle
- Beneficial characteristics:
 - Conformal, ultrathin
 - Low surface energy
 - Covalent bonding makes them wear resistant
 - Thermally stable (to a point)



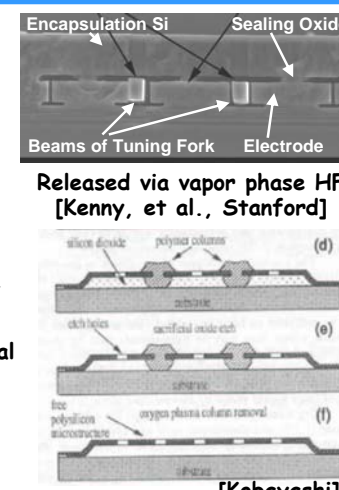
OTS
 $\text{CH}_3(\text{CH}_2)_{17}\text{SiCl}_3$

	θ_{water}
ODT SAM	$112 \pm 0.7^\circ$
SiO_2	$< 10^\circ$

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Dry Release

- Another way to avoid stiction is to use a dry sacrificial layer etch
- For an oxide sacrificial layer
 - use HF vapor phase etch
 - Additional advantage: gas can more easily get into tiny gaps
 - Issue: not always completely dry \rightarrow moisture can still condense \rightarrow stiction \rightarrow soln: add alcohol
- For a polymer sacrificial layer
 - Use an O_2 plasma etch (isotropic, so it can undercut well)
 - Issues:
 - Cannot be used when structural material requires high temperature for deposition
 - If all the polymer is not removed, polymer under the suspended structure can still promote stiction



Released via vapor phase HF [Kenny, et al., Stanford]

[Kobayashi]

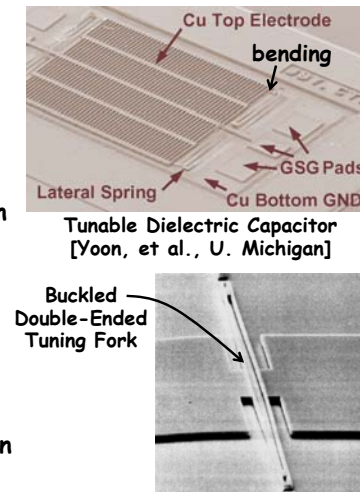
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Residual Stress

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Residual Stress in Thin Films

- After release, poorly designed microstructures might buckle, bend, or warp \rightarrow often caused by residual film stress
- Origins of residual stress, σ
 - Growth processes
 - Non-equilibrium deposition
 - Grain morphology change
 - Gas entrapment
 - Doping
 - Thermal stresses
 - Thermal expansion mismatch of materials \rightarrow introduce stress during cool-down after deposition
 - Annealing



Tunable Dielectric Capacitor [Yoon, et al., U. Michigan]

Buckled Double-Ended Tuning Fork

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Need to Control Film Stress

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- Resonance frequency expression for a lateral resonator:

$$f_0 \approx \frac{1}{2\pi} \sqrt{\frac{4E_y t W^3}{M L^3} + \frac{24\sigma_r t W}{5 M L}}$$

Since $W \ll L$, the stress term will dominate if $\sigma_r \sim E_y$

Basic term

 $\frac{4E_y t W^3}{M L^3}$

Stress term

 $\frac{24\sigma_r t W}{5 M L}$

E_y = Young's modulus
 σ_r = stress
 t = thickness
 W = beam width
 L = beam length
 M = mass

Labels: Folded-beam suspension, Shuttle, Anchor, Folding truss

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Tensile Versus Compressive Stress

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- Under tensile stress, a film wants to shrink w/r to its substrate
 - Caused, e.g., by differences in film vs. substrate thermal expansion coefficients
 - If suspended above a substrate and anchored to it at two points, the film will be "stretched" by the substrate
- Under compressive stress, a film wants to expand w/r to its substrate
 - If suspended above a substrate and anchored to it at two points, the film will buckle over the substrate

Labels: Si-substrate, tensile film, compressive film, buckled

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Vertical Stress Gradients

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- Variation of residual stress in the direction of film growth
- Can warp released structures in z-direction

200µM 20KV 00 017 S

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Stress in Polysilicon Films

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- Stress depends on crystal structure, which in turn depends upon the deposition temperature
- Temperature $\leq 600^\circ\text{C}$
 - Films are initially amorphous, then crystallize
 - Get equiaxed crystals, largely isotropic
 - Crystals have higher density \rightarrow tensile stress
 - Small stress gradient
- Temperature $\geq 600^\circ\text{C}$
 - Columnar crystals grow during deposition
 - As crystals grow vertically and in-plane they push on neighbors \rightarrow compressive stress
 - Positive stress gradient

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Annealing Out Polysilicon Stress

- Control polySi stress by annealing at high temperatures
 - Typical anneal temperatures: 900-1150°C
 - Grain boundaries move, relax
 - Can dope while annealing by sandwiching the polysilicon between similarly doped oxides (symmetric dopant drive-in), e.g. using 10-15 wt. % PSG

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Topography Issues

- Degradation of lithographic resolution
 - PR step coverage, streaking
 - Thickness differences pose problems for reduction steppers
- Stringers
 - Problematic when using anisotropic etching, e.g., RIE

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Nickel Surface-Micromachining Process Flow

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Electroplating: Metal MEMS

- Use electroplating to obtain metal μ structures
- When thick: call it "LIGA"
- Pros:** fast low temp deposition, very conductive
- Cons:** drift, low mech. Q but may be solvable?

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Nickel Metal Surface-Micromachining

- Deposit isolation LTO:
 - ↳ Target = 2µm
 - ↳ 1 hr. 40 min. LPCVD @450°C
- Densify the LTO
 - ↳ Anneal @950°C for 30 min.
- Define metal interconnect via lift-off
 - ↳ Spin photoresist and pattern lithographically to open areas where interconnect will stay
 - ↳ Evaporate a Ti/Au layer
 - ↳ Target = 30nm Ti
 - ↳ Target = 270nm Au
 - ↳ Remove photoresist in PRS2000 → Ti/Au atop the photoresist also removed

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Nickel Metal Surface-Micromachining

- Evaporate Al to serve as a sacrificial layer
 - ↳ Target = 1µm
- Lithography to define anchor openings
- Wet etch the aluminum to form anchor vias
 - ↳ Use solution of $H_3PO_4/HNO_3/H_2O$
- Remove photoresist in PRS2000
- Electroplate nickel to fill the anchor vias
 - ↳ Use solution of nickel sulfamate @ 50°C
 - ↳ Time the electroplating to planarize the surface

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Nickel Metal Surface-Micromachining

- Evaporate a thin film of nickel to serve as a seed layer for subsequent Ni electroplating
 - ↳ Target = 20nm
- Form a photoresist mold for subsequent electroplating
 - ↳ Spin 6 µm-thick AZ 9260 photoresist
 - ↳ Lithographically pattern the photoresist to delineate areas where nickel structures are to be formed
- Electroplate nickel structural material through the PR mold
 - ↳ Use a solution of nickel sulfamate @ 50°C
 - ↳ Cathode-to-anode current density ~ 2.5 mA/cm²

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Nickel Metal Surface-Micromachining

- Strip the PR in PRS2000
- Remove the Ni seed layer in Ni wet etchant
- Release the structures
 - ↳ Use a $K_4Fe(CN)_6/NaOH$ etchant that attacks Al while leaving Ni and Au intact
 - ↳ Etch selectivity > 100:1 for Al:Ni and Al:Au

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Nickel Surface-Micromachining Example

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- Below: Surface-micromachined in nickel using the described process flow

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3D "Pop-up" MEMS

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Pop-Up MEMS

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First MEMS hinge
[K. Pister, et al., 1992]

Corner Cube Reflector
[v. Hsu, 1999]

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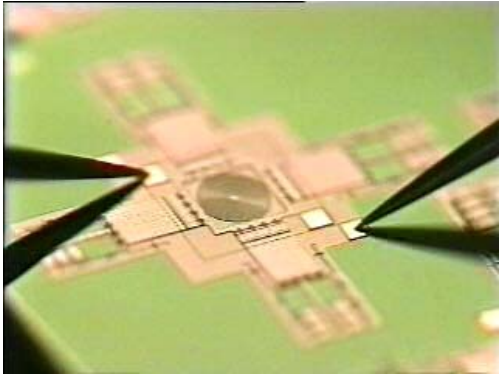
Pop-Up MEMS

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- Pictured: hinged Campanile made in SUMMIT process, assembled using probes [Elliot Hui, et al.]

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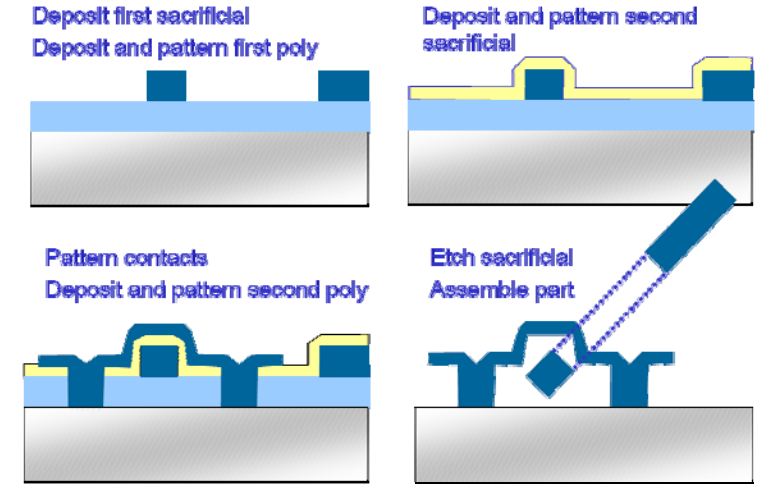
3D Direct-Assembled Tunable L



[Ming Wu, UCLA]

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Hinge Process Flow



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Deposit first sacrificial
Deposit and pattern first poly

Deposit and pattern second sacrificial

Pattern contacts
Deposit and pattern second poly

Etch sacrificial
Assemble part

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