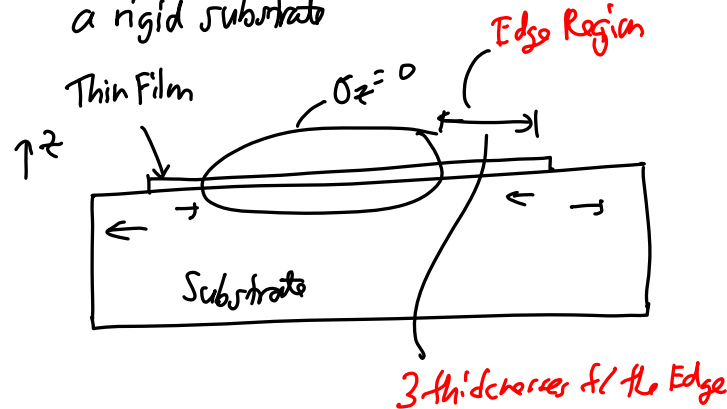


Lecture 13: Mechanics of Materials II

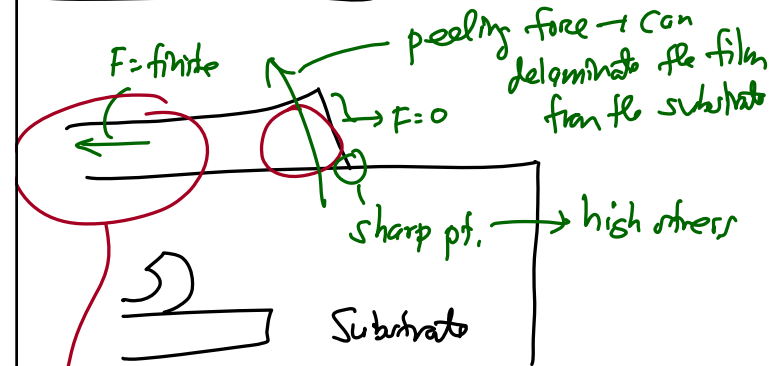
- Announcements:
- Module 7 on Mechanics of Materials online
- HW#3 due Wednesday morning
- HW#4 online soon
- No office hours this coming Wednesday
-
- Reading: Senturia, Chpt. 8
- Lecture Topics:
 - ↳ Stress, strain, etc., for isotropic materials
 - ↳ Thin films: thermal stress, residual stress, and stress gradients
 - ↳ Internal dissipation
 - ↳ MEMS material properties and performance metrics
-
- Last Time: Going thru Module 7 ... continue this

Important Case: Plane Stress

⇒ common case for a thin-film coating on a rigid substrate



Zoom-in on Edge Region



Take a closer look at this region: $\sigma_z = 0$
Get two components of stress (strain)

$$\epsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + 0)]$$

$$\epsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x + 0)]$$

Assume plane stress! → isotropic → $\sigma_x = \sigma_y = \sigma$
(symmetry in the xy -plane) ↓
 $\epsilon_x = \epsilon_y = \epsilon$

$$\epsilon_x = \frac{1}{E} [\sigma - \nu\sigma]$$

$$= \frac{\sigma}{\left(\frac{E}{1-\nu}\right)} \Rightarrow \epsilon_x = \frac{\sigma}{E'}$$

where $E' \triangleq \text{Biaxial Modulus} = \frac{E}{1-\nu}$

Linear Thermal Expansion

temperature \uparrow \rightarrow solids expand in volume

Definition. linear thermal expansion coefficient

$$\left. \begin{array}{l} \text{Linear Thermal} \\ \text{Exp. Coefficient} \end{array} \right\} \triangleq \alpha_T = \frac{d\epsilon_T}{dT} \quad [\text{Kelvin}^{-1}]$$

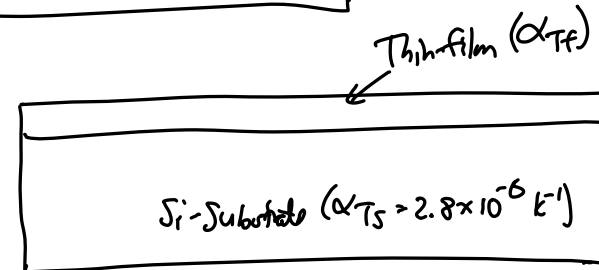
Remarks.

- ① α_T values tend to be in the 10^{-6} to 10^{-7} range
- ② $10^{-6} \text{ K}^{-1} = 1 \mu\text{strain/K}$
- ③ In 3D, get a volume thermal exp. coefficient.

$$\frac{\Delta V}{V} = 3\alpha_T \Delta T$$

- ④ For moderate ΔT 's $\rightarrow \alpha_T \approx \text{constant}$
 \searrow for larger ΔT , then $\alpha_T = f(T)$

Ex. Thin-Film Thermal Stress



Assume.

- ① Substrate is much thicker than the film.
- ② Film is deposited stress free @ $T_d \leftarrow$ deposition temperature
- ③ Then the whole thing is cooled to room temperature, T_r .

The thermal strain of the substrate: (in one plane dimension)

$$\epsilon_S = -\alpha_{TS} \Delta T, \text{ where } \Delta T = T_d - T_r$$

If the film were not attached to the substrate.

$$\epsilon_{f,\text{free}} = -\alpha_{TF} \Delta T$$

But the film is attached to the substrate

\Rightarrow thickness sub \gg thickness film

\therefore substrate wins!



σ_y
 thus, the actual strain experienced by the film
 is that of the substrate:

$$\epsilon_{f, attached} = -\alpha_{TS} \Delta T$$

Thus:

$$\text{Thermal Mismatch Strain} = \epsilon_{f, mismatch} \\ = (\alpha_{TF} - \alpha_{TS}) \Delta T$$

Note that this is a biaxial strain.
 (Assumes the film is deposited isotropically
 onto the substrate.)

$$\sigma_{f, mismatch} = \underbrace{\left(\frac{E}{1-\nu}\right)}_{E'} \epsilon_{f, mismatch}$$

Ex. Thin-film is polyimide $\rightarrow \alpha_{TF} = 70 \times 10^{-6} \text{ K}^{-1}$

$$E' = 4 \text{ GPa}$$

deposited @ 250°C , then cool to RT: 25°C

$$\Delta T = 225 \text{ K}$$

$$\epsilon_{f, mismatch} = (70 - 2.8) \mu(225) = 1.5 \times 10^{-2}$$

$$\left[\mu = 10^6, m = 10^{-3}, k = 10^2, G = 10^9 \right]$$

$$\sigma_{f, mismatch} = \underbrace{(4 \text{ G})}_{10^9} \underbrace{(1.5 \times 10^{-2})}_{1} = 60.5 \text{ MPa}$$

Stress is (+) \rightarrow tensile

$\text{SiO}_2 \rightarrow$ [(-) would be compressive]