EE C245 – ME C218
Introduction to MEMS Design
Fall 2012

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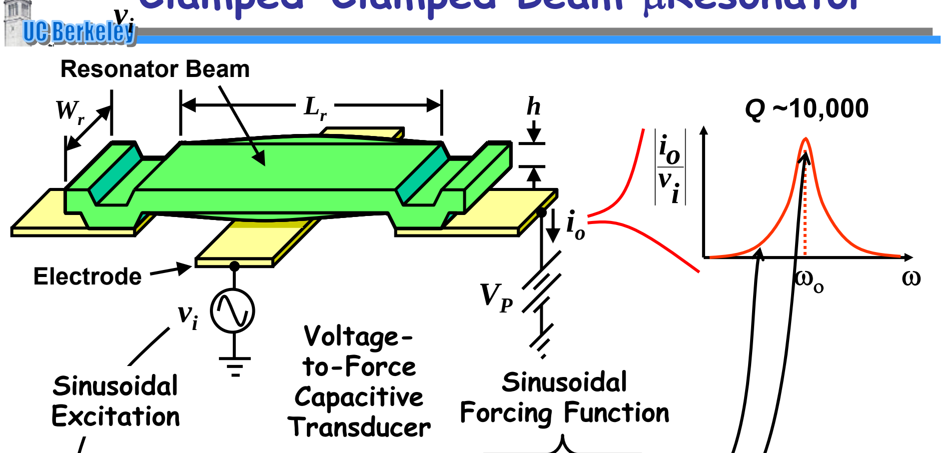
Lecture Module 10: Resonance Frequency

Lecture Outline

- Reading: Senturia, Chpt. 10: §10.5, Chpt. 19
- Lecture Topics:
  - Estimating Resonance Frequency
  - Lumped Mass-Spring Approximation
  - ADXL-50 Resonance Frequency
  - Distributed Mass & Stiffness
  - Folded-Beam Resonator

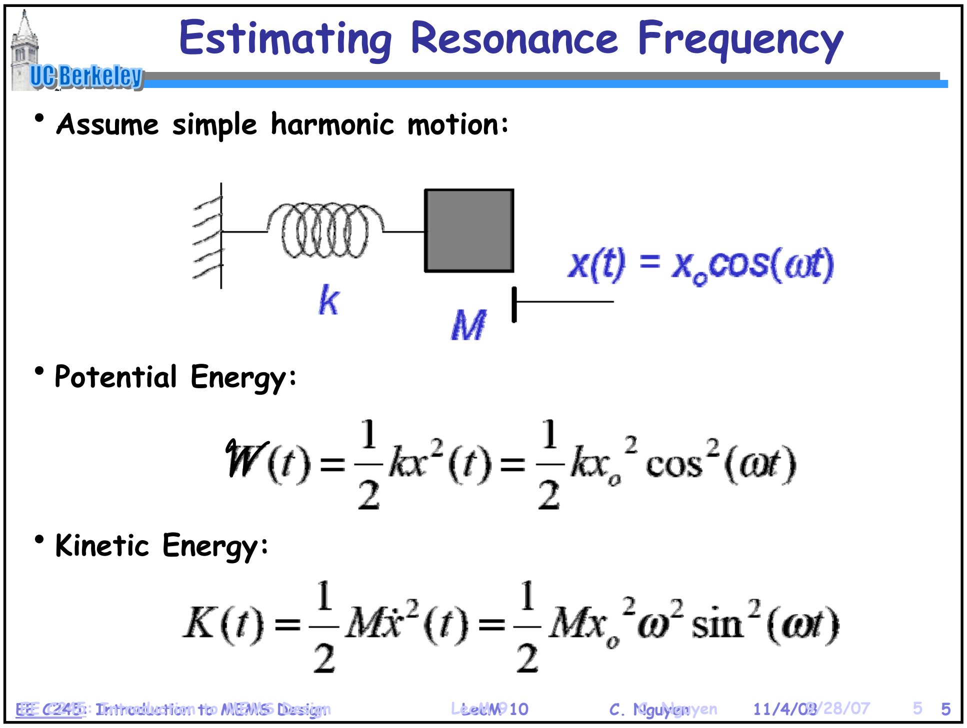
Estimating Resonance Frequency

Clamped-Clamped Beam μResonator



$$v_i = V_i \cos[\omega_o t] \longrightarrow f_i = \overbrace{F_i \cos[\omega_o t]}^{\text{Sinusoidal Forcing Function}}$$

- $\omega \neq \omega_o$: small amplitude
- $\omega = \omega_o$: maximum amplitude → beam reaches its maximum potential and kinetic energies



Estimating Resonance Frequency

- Assume simple harmonic motion:

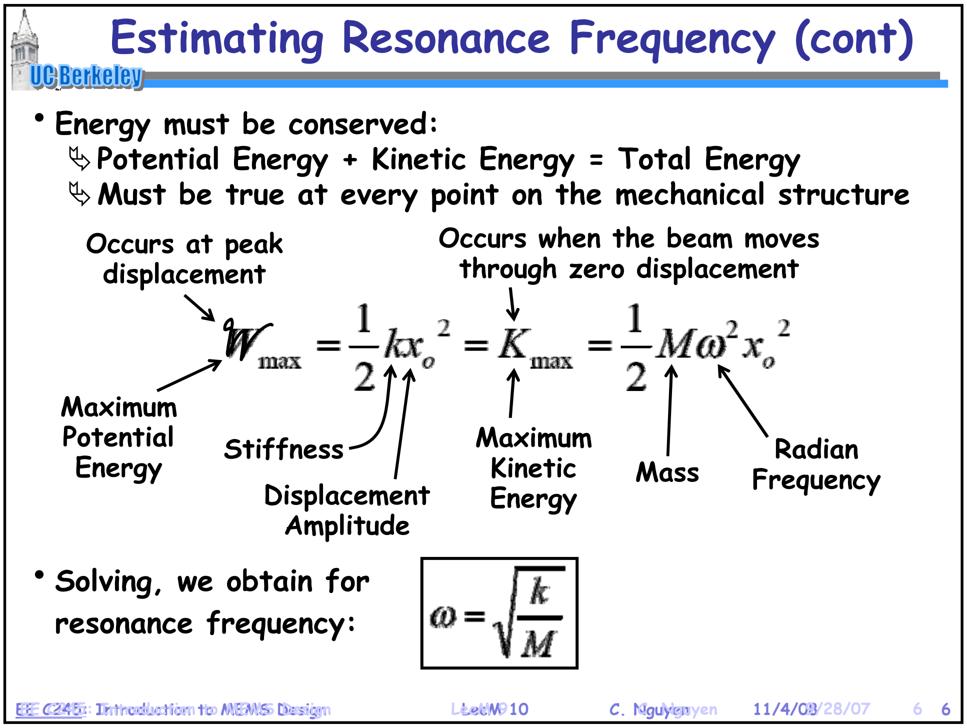
$x(t) = x_o\cos(\omega t)$

- Potential Energy:

$$\mathcal{W}(t)=\frac{1}{2}kx^2(t)=\frac{1}{2}kx_o{}^2\cos^2(\omega t)$$

- Kinetic Energy:

$$K(t)=\frac{1}{2}M\dot{x}^2(t)=\frac{1}{2}Mx_o{}^2\omega^2\sin^2(\omega t)$$



Estimating Resonance Frequency (cont)

- Energy must be conserved:
  - Potential Energy + Kinetic Energy = Total Energy
  - Must be true at every point on the mechanical structure

Occurs at peak displacement

Occurs when the beam moves through zero displacement

$$\mathcal{W}_{\max}=\frac{1}{2}kx_o{}^2=K_{\max}=\frac{1}{2}M\omega^2x_o{}^2$$

Maximum Potential Energy

Stiffness

Displacement Amplitude

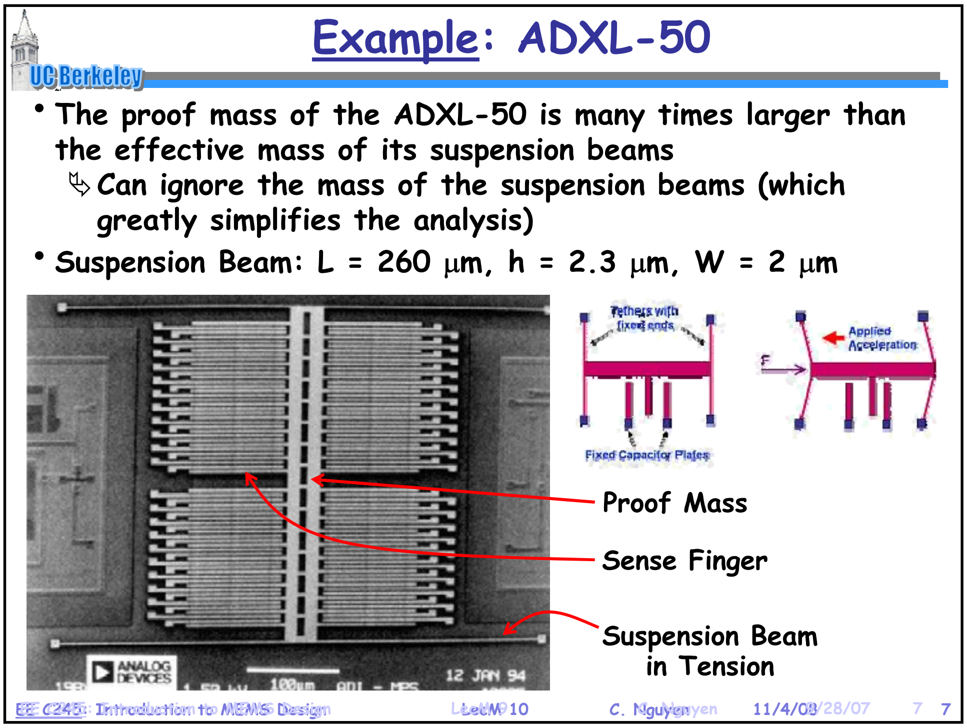
Maximum Kinetic Energy

Mass

Radian Frequency

- Solving, we obtain for resonance frequency:

$$\boxed{\omega=\sqrt{\frac{k}{M}}}$$



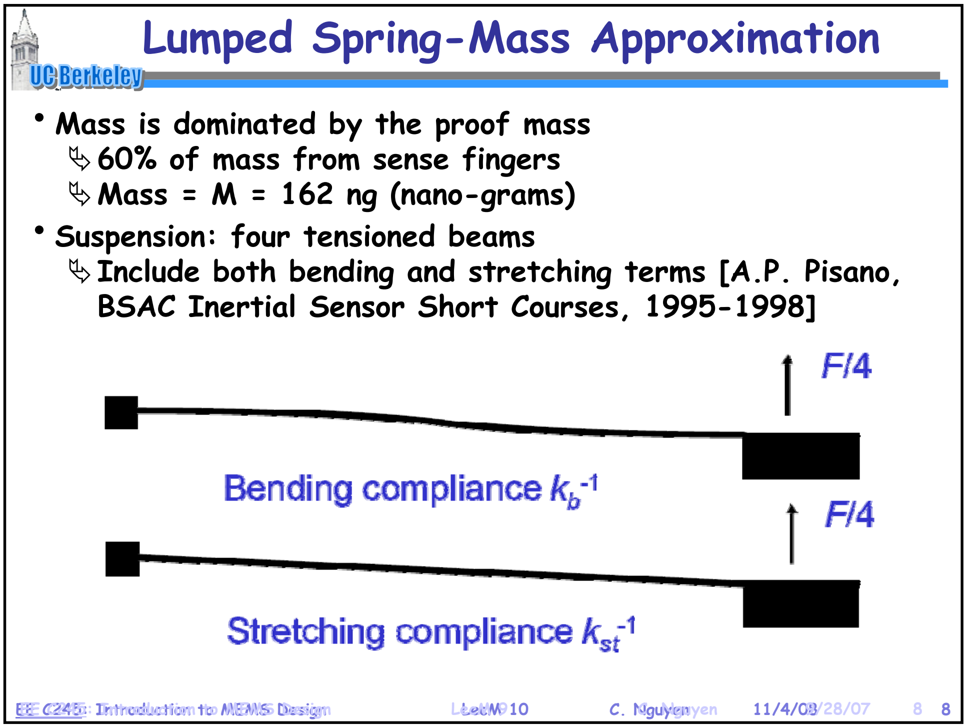
Example: ADXL-50

- The proof mass of the ADXL-50 is many times larger than the effective mass of its suspension beams
  - ↳ Can ignore the mass of the suspension beams (which greatly simplifies the analysis)
- Suspension Beam: L = 260 μm, h = 2.3 μm, W = 2 μm

Proof Mass

Sense Finger

Suspension Beam
in Tension



Lumped Spring-Mass Approximation

- Mass is dominated by the proof mass
  - ↳ 60% of mass from sense fingers
  - ↳ Mass = M = 162 ng (nano-grams)
- Suspension: four tensioned beams
  - ↳ Include both bending and stretching terms [A.P. Pisano, BSAC Inertial Sensor Short Courses, 1995-1998]

Bending compliance k_b^{-1}

Stretching compliance k_{st}^{-1}

ADXL-50 Suspension Model

- Bending contribution:

$$k_b^{-1} = (1/k_c + 1/k_c) = 2\left[\frac{(L/2)^3}{3E(Wh^3/12)}\right] = \frac{L^3}{EWh^3} = 4.2\mu m/\mu N$$

- Stretching contribution:

$$k_{st}^{-1} = L/S = \frac{L}{\sigma_r Wh} = 1.14\mu m/\mu N$$

$$F_y = S\sin\theta \approx S(x/L) = \underbrace{\left(\frac{S}{L}\right)}_{k_{st}} x$$

- Total spring constant: *add* bending to stretching

(since they are in parallel)

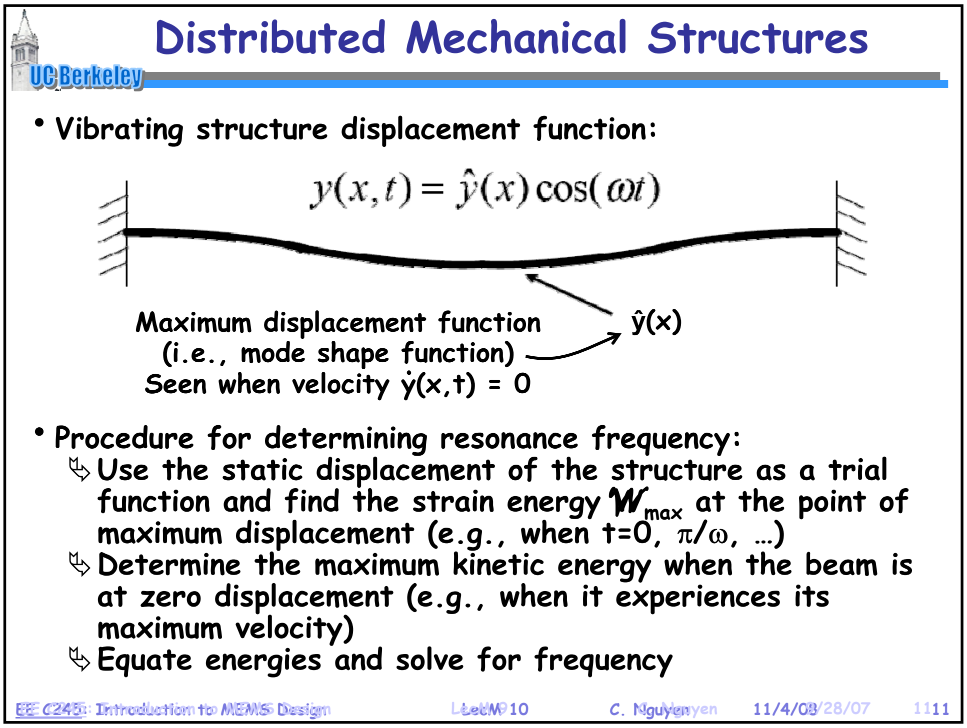
$$k = 4(k_b + k_{st}) = 4(0.24 + 0.88) = 4.5\mu N/\mu m$$

ADXL-50 Resonance Frequency

- Using a lumped mass-spring approximation:

$$f = \frac{1}{2\pi}\sqrt{\frac{k}{M}} = \frac{1}{2\pi}\sqrt{\frac{4.48N/m}{162x10^{-12}kg}} = 26.5kHz$$

- On the ADXL-50 Data Sheet: f_o = 24 kHz
  - Why the 10% difference?
  - Well, it's approximate … plus …
  - Above analysis does not include the frequency-pulling effect of the DC bias voltage across the plate sense fingers and stationary sense fingers … something we'll cover later on …



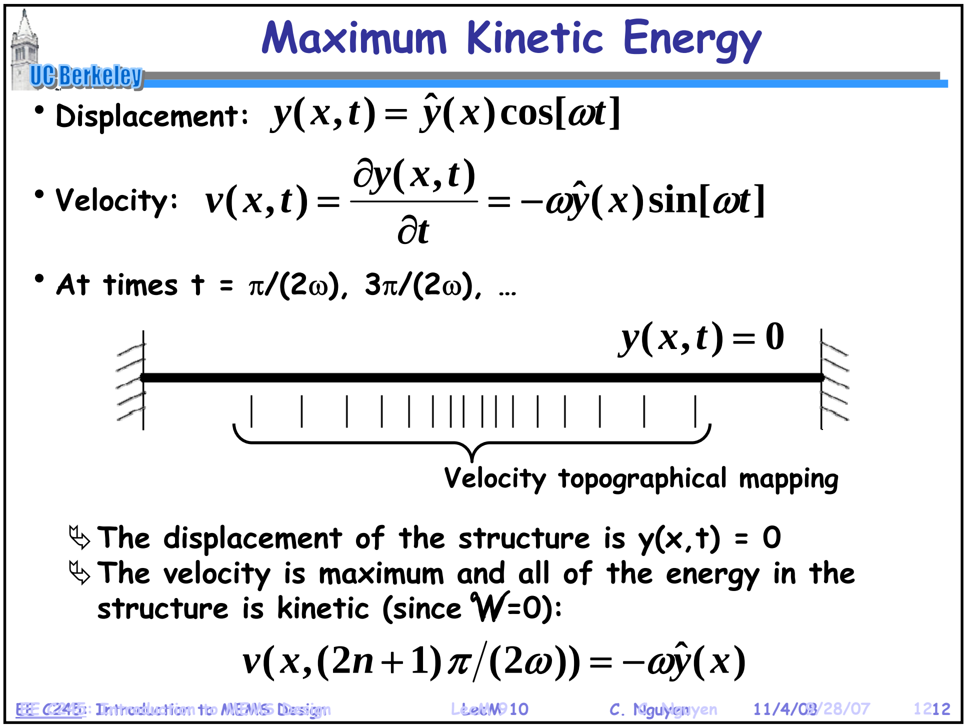
Distributed Mechanical Structures

- Vibrating structure displacement function:

$$y(x,t)=\hat{y}(x)\cos(\omega t)$$

Maximum displacement function
(i.e., mode shape function)
Seen when velocity $\dot{y}(x,t) = 0$

- Procedure for determining resonance frequency:
  - ➯ Use the static displacement of the structure as a trial function and find the strain energy $\mathcal{W}_{max}$ at the point of maximum displacement (e.g., when t=0, π/ω, …)
  - ➯ Determine the maximum kinetic energy when the beam is at zero displacement (e.g., when it experiences its maximum velocity)
  - ➯ Equate energies and solve for frequency



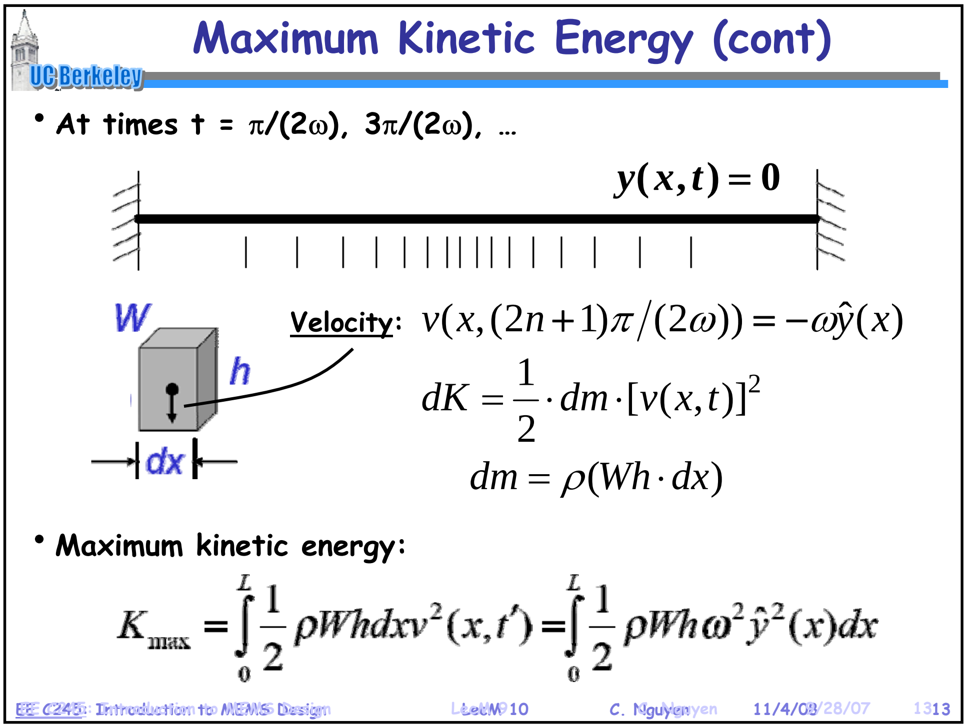
Maximum Kinetic Energy

- Displacement: $y(x,t)=\hat{y}(x)\cos[\omega t]$
- Velocity: $v(x,t)=\dfrac{\partial y(x,t)}{\partial t}=-\omega\hat{y}(x)\sin[\omega t]$
- At times t = $\pi/(2\omega)$, $3\pi/(2\omega)$, …

Velocity topographical mapping

  - ➯ The displacement of the structure is y(x,t) = 0
  - ➯ The velocity is maximum and all of the energy in the structure is kinetic (since $\mathcal{W}$=0):

$$v(x,(2n+1)\pi/(2\omega))=-\omega\hat{y}(x)$$



Maximum Kinetic Energy (cont)

- At times t = π/(2ω), 3π/(2ω), …

$$y(x,t) = 0$$

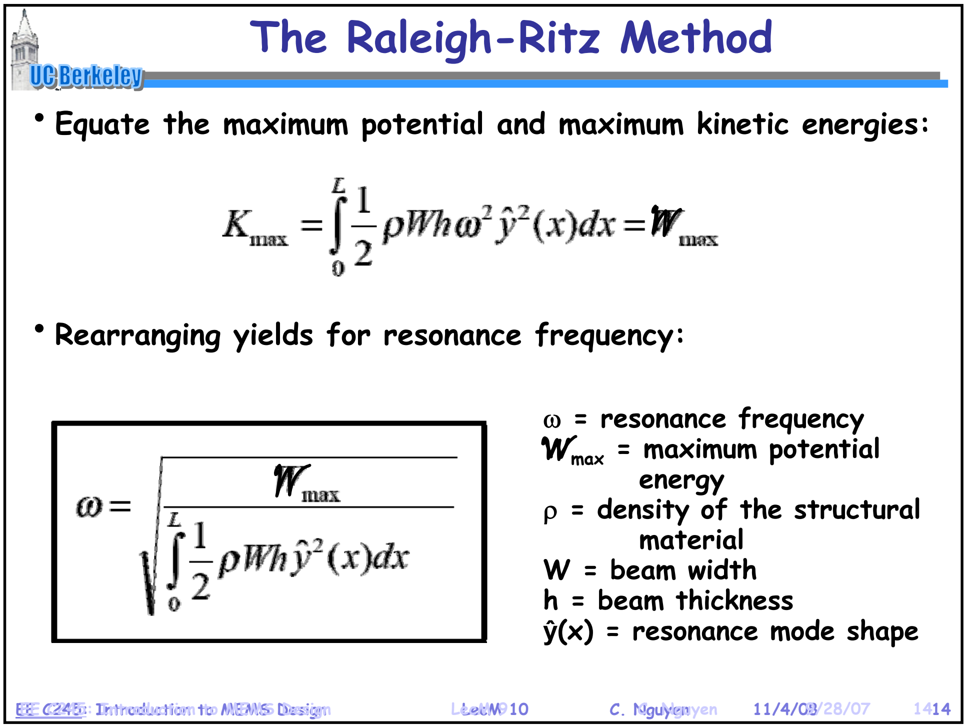
Velocity: $v(x,(2n+1)\pi/(2\omega)) = -\omega\hat{y}(x)$

$$dK = \frac{1}{2}\cdot dm\cdot[v(x,t)]^2$$

$$dm = \rho(Wh\cdot dx)$$

- Maximum kinetic energy:

$$K_{\max} = \int_0^L \frac{1}{2}\rho Whdxv^2(x,t') = \int_0^L \frac{1}{2}\rho Wh\omega^2\hat{y}^2(x)dx$$



The Raleigh-Ritz Method

- Equate the maximum potential and maximum kinetic energies:

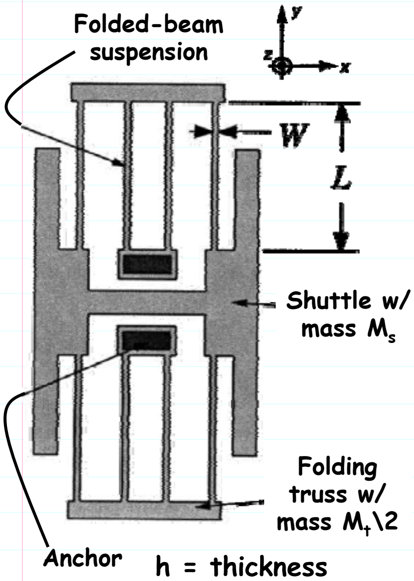
$$K_{\max} = \int_0^L \frac{1}{2}\rho Wh\omega^2\hat{y}^2(x)dx = \mathcal{W}_{\max}$$

- Rearranging yields for resonance frequency:

$$\boxed{\omega = \sqrt{\frac{\mathcal{W}_{\max}}{\int_0^L \frac{1}{2}\rho Wh\hat{y}^2(x)dx}}}$$

ω = resonance frequency
$\mathcal{W}_{max}$ = maximum potential energy
ρ = density of the structural material
W = beam width
h = beam thickness
ŷ(x) = resonance mode shape

Example: Folded-Beam Resonator



- Derive an expression for the resonance frequency of the folded-beam structure at left.

Use Rayleigh-Ritz method.

$$KE_{max} = PE_{max}$$

Kinetic Energy:

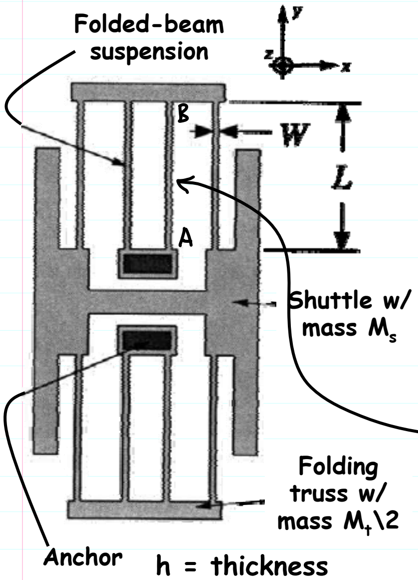
$$KE_{max} = \underbrace{KE_s}_{\text{shuttle}} + \underbrace{KE_t}_{\text{truss}} + \underbrace{KE_b}_{\text{beams}}$$

$$= \frac{1}{2}v_s^2 M_s + \frac{1}{2}v_t^2 M_t + \underbrace{\frac{1}{2}\int v_b^2 \, dM_b}$$

mass of both trusses

Must integrate since the beam velocity is a function of location y!

Get Kinetic Energies



Velocity of the shuttle: $v_s = \omega_o X_o$

Resonance Freq.

Maximum Displacement Amplitude

$$\therefore \quad KE_s = \frac{1}{2}v_s^2 M_s = \boxed{\frac{1}{2}\omega_o^2 X_o^2 M_s}$$

Velocity of the truss: $v_t = \frac{1}{2}v_s = \frac{1}{2}\omega_o X_o$

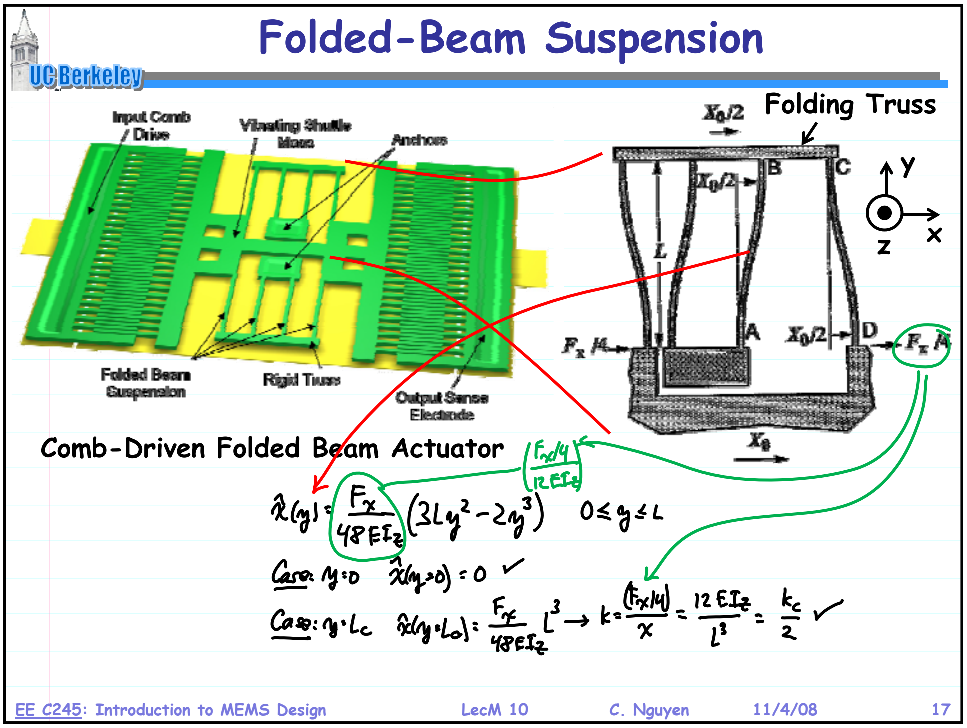
$$\therefore \quad KE_t = \frac{1}{2}\left(\frac{1}{2}\omega_o X_o\right)^2 M_t = \boxed{\frac{1}{8}\omega_o^2 X_o^2 M_t}$$

Velocity of the beam segments:

⇒ assume the mode shape is the same as the static displacement shape

⇒ For segment AB:

$$\hat{x}(y) = \frac{F_x}{48EI_z}\left(3Ly^2 - 2y^3\right) \qquad 0 \le y \le L \qquad (1)$$



Folded-Beam Suspension

Comb-Driven Folded Beam Actuator

$$\left(\frac{F_x/4}{12EI_z}\right)$$

$$\hat{x}(y) = \frac{F_x}{48EI_z}\left(3Ly^2 - 2y^3\right) \quad 0 \le y \le L$$

Case: $y = 0$ $\quad \hat{x}(y=0) = 0$ ✓

Case: $y = L_c$ $\quad \hat{x}(y=L_c) = \frac{F_x}{48EI_z}L^3 \rightarrow k = \frac{(F_x/4)}{x} = \frac{12EI_z}{L^3} = \frac{k_c}{2}$ ✓

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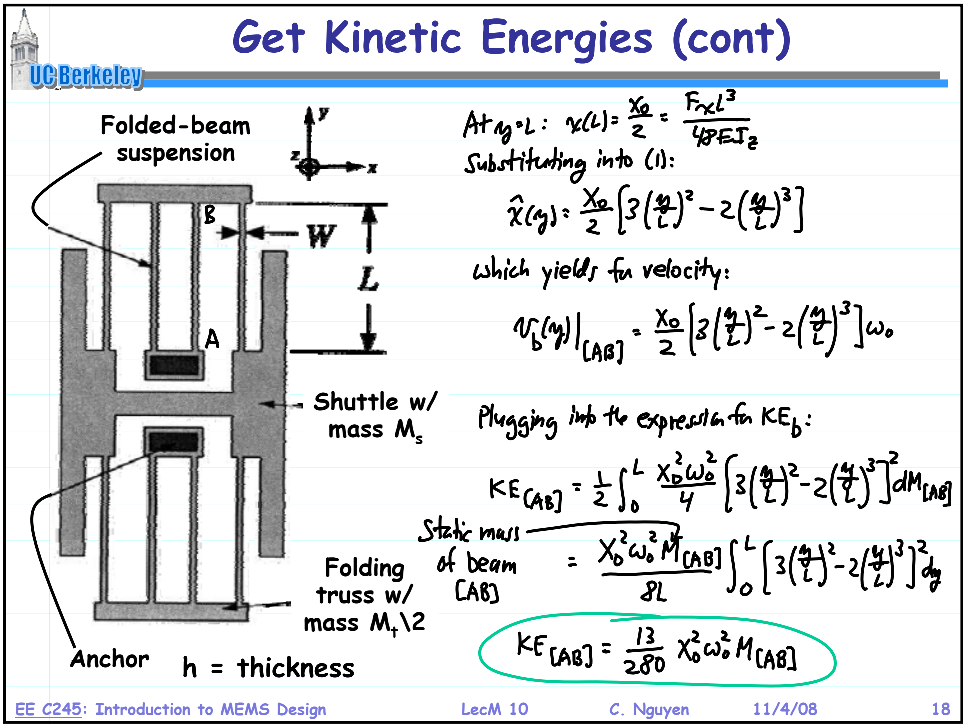

Get Kinetic Energies (cont)

Folded-beam suspension

Shuttle w/ mass M_s

Folding truss w/ mass $M_t\backslash 2$

Anchor

h = thickness

At $y = L$: $x(L) = \frac{X_0}{2} = \frac{F_x L^3}{48EI_z}$

Substituting into (1):

$$\hat{x}(y) = \frac{X_0}{2}\left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3\right]$$

which yields for velocity:

$$v_b(y)\Big|_{[AB]} = \frac{X_0}{2}\left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3\right]\omega_0$$

Plugging into the expression for KE_b:

$$KE_{[AB]} = \frac{1}{2}\int_0^L \frac{X_0^2\omega_0^2}{4}\left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3\right]^2 dM_{[AB]}$$

Static mass of beam [AB]

$$= \frac{X_0^2\omega_0^2 M_{[AB]}}{8L}\int_0^L \left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3\right]^2 dy$$

$$\boxed{KE_{[AB]} = \frac{13}{280}X_0^2\omega_0^2 M_{[AB]}}$$

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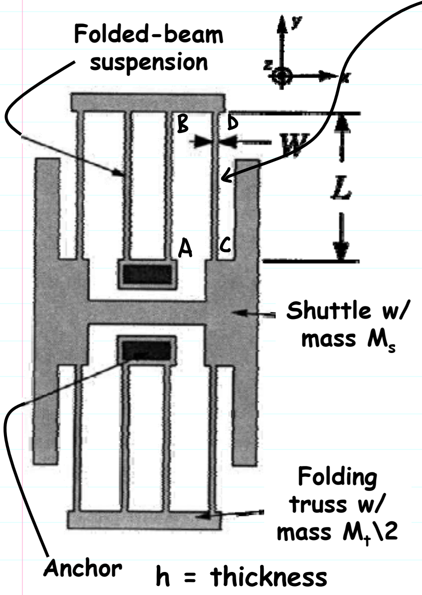
Get Kinetic Energies (cont)



For segment CD:

$$v_b(y)\big|_{[CD]} = X_o\left[1-\frac{3}{2}\left(\frac{y}{L}\right)^2+\left(\frac{y}{L}\right)^3\right]\omega_o$$

Thus:

$$KE_{[CD]} = \frac{X_o^2\omega_o^2 M_{[CD]}}{2L}\int_0^L\left[1-\frac{3}{2}\left(\frac{y}{L}\right)^2+\left(\frac{y}{L}\right)^3\right]dy$$

$$KE_{[CD]} = \frac{83}{280}X_o^2\omega_o^2 M_{[CD]}$$

Static mass of beam [CD]

Let $M_b \triangleq$ total mass of the 8 beams.

Then: $M_{[AB]} = M_{[CD]} = \frac{1}{8}M_b$

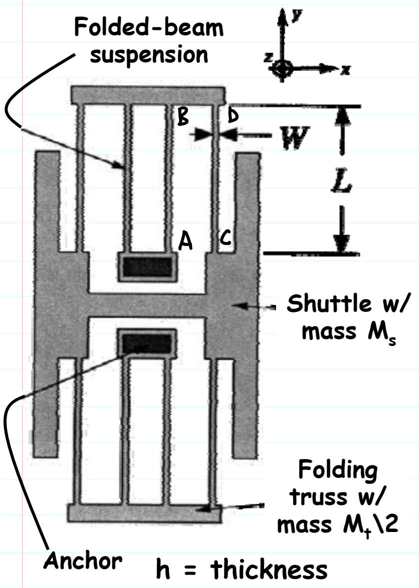
Thus:

$$KE_b = 4KE_{[AB]} + 4K_{[CD]} = \frac{6}{35}X_o^2\omega_o^2 M_b$$

and

$$KE_{max} = X_o^2\omega_o^2\left[\frac{1}{2}M_s+\frac{1}{8}M_t+\frac{6}{35}M_b\right]$$

Get Potential Energy & Frequency



PE_{max} is simply the work done to achieve maximum deflection:

$=k_c$

$$PE_{max} = \frac{1}{2}k_x X_o^2$$

Thus, using Raleigh-Ritz:

$$KE_{max} = PE_{max}$$

$=k_c$

$$\cancel{X_o^2}\omega_o^2\left[\frac{1}{2}M_s+\frac{1}{8}M_t+\frac{6}{35}M_b\right] = \frac{1}{2}k_x\cancel{X_o^2}$$

$$\boxed{\omega_o = \left[\frac{k_x}{M_{eq}}\right]^{1/2} \quad \text{where } M_{eq} = M_s + \frac{1}{4}M_t + \frac{12}{35}M_b}$$

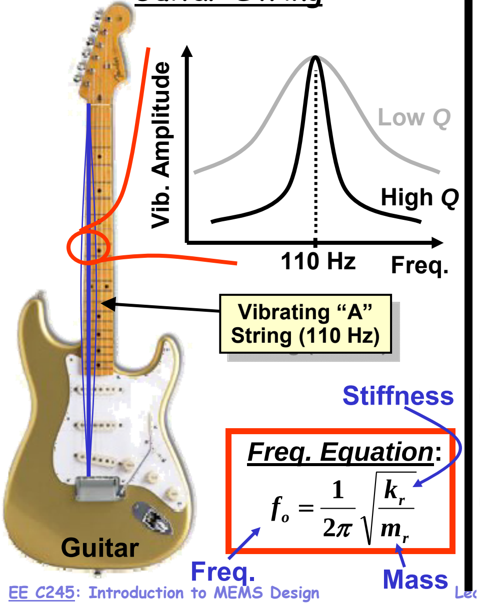
$=k_c$

(Resonance Frequency of a Folded-Beam Suspended Shuttle)

Brute Force Methods for Resonance Frequency Determination

Basic Concept: Scaling Guitar Strings

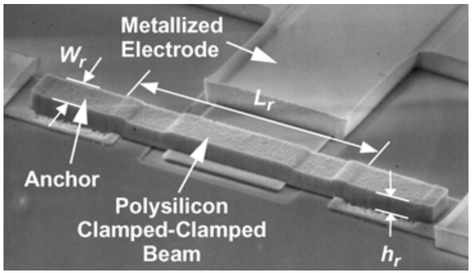
Guitar String



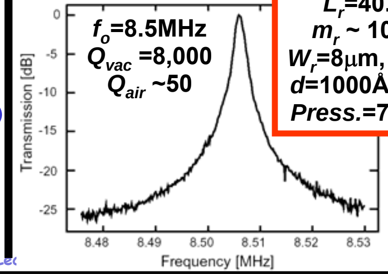
Freq. Equation:

$$f_o = \frac{1}{2\pi}\sqrt{\frac{k_r}{m_r}}$$

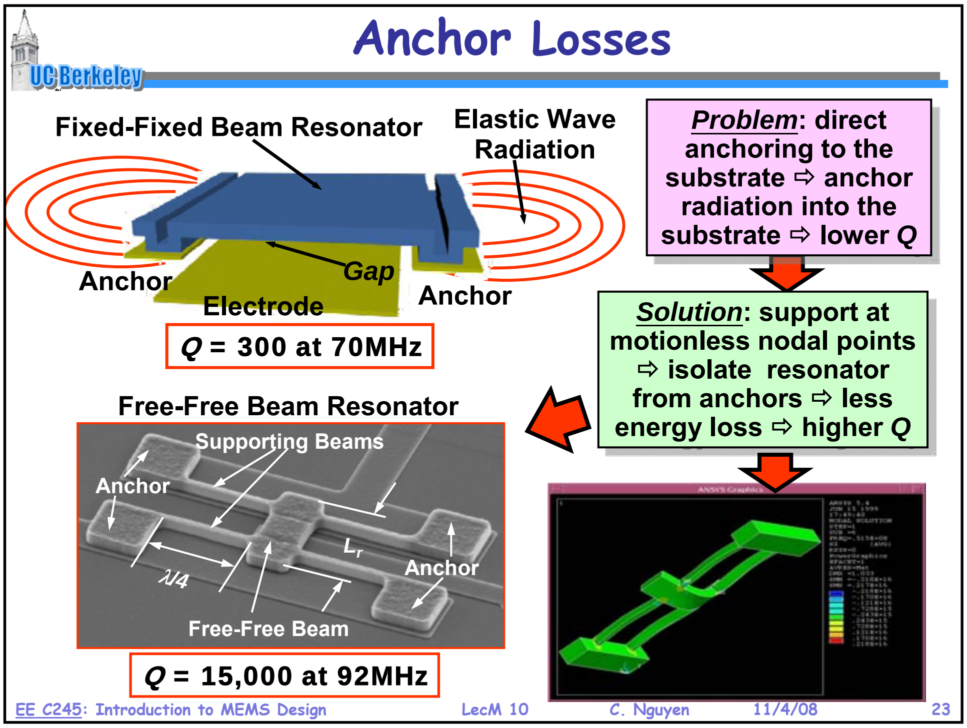
μMechanical Resonator



[Bannon 1996]



Performance:
L_r=40.8μm
m_r ~ 10^{-13} kg
W_r=8μm, h_r=2μm
d=1000Å, V_P=5V
Press.=70mTorr



Anchor Losses

Q = 300 at 70MHz

Problem: direct anchoring to the substrate ⇨ anchor radiation into the substrate ⇨ lower Q

Solution: support at motionless nodal points ⇨ isolate resonator from anchors ⇨ less energy loss ⇨ higher Q

Free-Free Beam Resonator

Q = 15,000 at 92MHz

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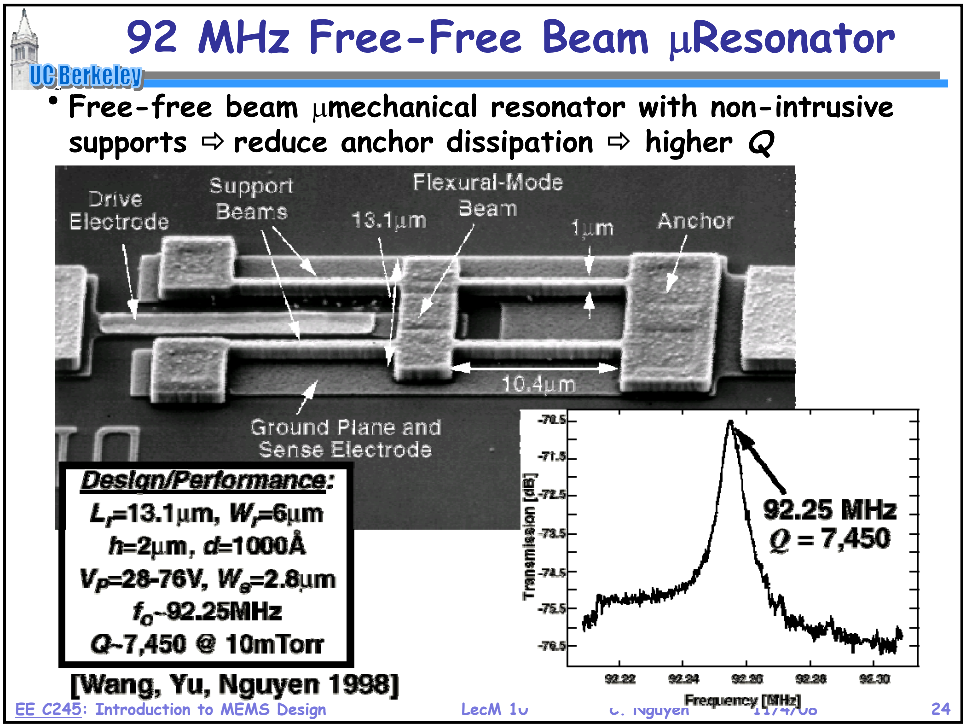

92 MHz Free-Free Beam μResonator

- Free-free beam μmechanical resonator with non-intrusive supports ⇨ reduce anchor dissipation ⇨ higher Q

Design/Performance:

L_r=13.1μm, W_r=6μm
h=2μm, d=1000Å
V_P=28-76V, W_e=2.8μm
f_o~92.25MHz
Q~7,450 @ 10mTorr

[Wang, Yu, Nguyen 1998]

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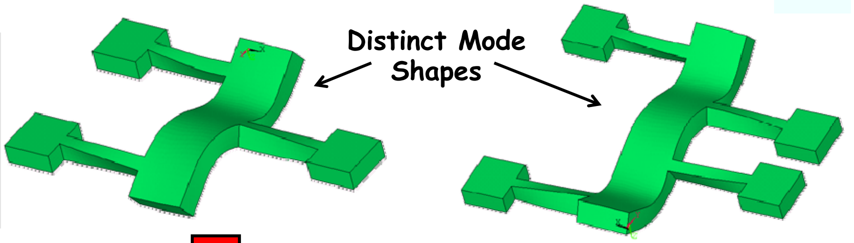
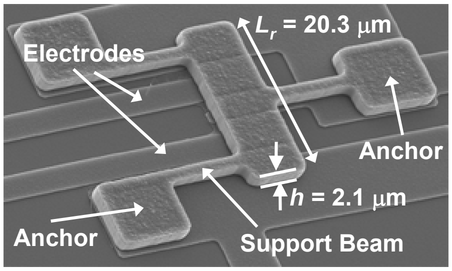
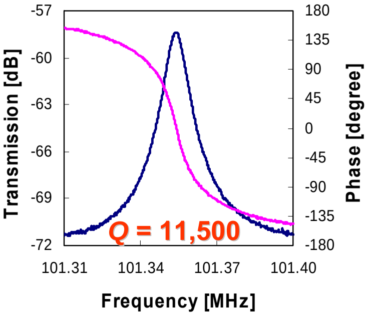
Higher Order Modes for Higher Freq.

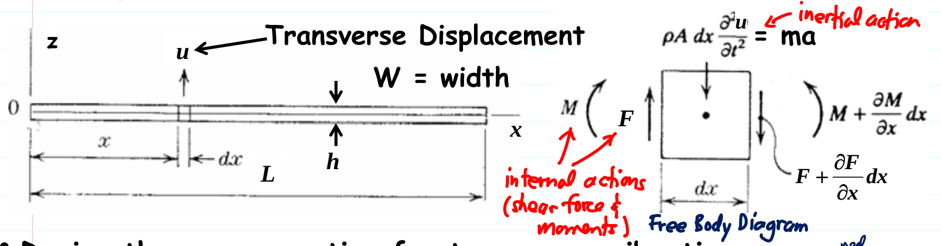
2nd Mode Free-Free Beam **3rd Mode Free Free Beam**







Flexural-Mode Beam Wave Equation



$$\rho A\,dx\frac{\partial^2 u}{\partial t^2} = ma$$

- Derive the wave equation for transverse vibration:

Dynamic Equilibrium Condition for Forces in the y-direction: $\cancel{M} + F\frac{dx}{2} + F\frac{dx}{2} + \overset{\text{neg.}}{\cancel{\frac{dF}{dx}\frac{dx}{2}}} - \cancel{M} - \frac{\partial M}{\partial x}dx = 0$

$$F - \left(F + \frac{\partial F}{\partial x}dx\right) - \rho A dx\frac{\partial^2 u}{\partial t^2} = 0 \quad (1)$$

neglect the $\frac{\partial F}{\partial x}dx$ term

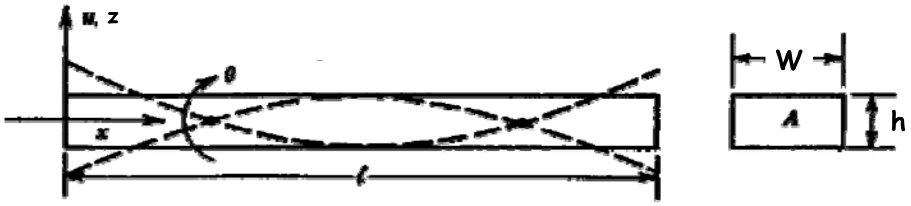
and the moment equilibrium condition: $-Fdx + \frac{\partial M}{\partial x}dx \approx 0 \quad (2)$

Combining (1) & (2):

$$\frac{\partial^2 M}{\partial x^2}dx = -\rho A dx\frac{\partial^2 u}{\partial t^2} \longrightarrow \frac{\partial^2}{\partial x^2}\left(-EI\frac{\partial^2 u}{\partial x^2}\right) = -\rho A\frac{\partial^2 u}{\partial t^2} \longrightarrow \boxed{\begin{gathered}\frac{\partial^2 u}{\partial t^2} = \left(\frac{EI}{\rho A}\right)\frac{\partial^4 u}{\partial x^4}\\ I_y = \frac{Wh^3}{12}\end{gathered}}$$

$$\left[\frac{\partial^2 u}{\partial x^2} = -\frac{M}{EI} \rightarrow M = -EI\frac{\partial^2 u}{\partial x^2}\right]$$

Example: Free-Free Beam



- Determine the resonance frequency of the beam
- Specify the lumped parameter mechanical equivalent circuit
- Transform to a lumped parameter electrical equivalent circuit
- Start with the flexural-mode beam equation:

$$\frac{\partial^2 u}{\partial t^2} = \left(\frac{EI}{\rho A}\right)\frac{\partial^4 u}{\partial x^4}$$

Free-Free Beam Frequency

- Substitute u = $u_1 e^{j\omega t}$ into the wave equation:

$$\frac{\partial^4 u}{\partial x^4} = \left(\omega^2 \frac{\rho A}{EI}\right) u \qquad (1)$$

- This is a 4th order differential equation with solution:

$$\underline{u(x)} = \mathscr{A}\cosh kx + \mathscr{B}\sinh kx + \mathscr{C}\cos kx + \mathscr{D}\sin kx \qquad (2)$$

Gives the mode shape during resonance vibration.

- Boundary Conditions:

At $x = 0$	At $x = \ell$	
$\frac{\partial^2 u}{\partial x^2} = 0$	$\frac{\partial^2 u}{\partial x^2} = 0$	$M = 0$ (Bending moment)
$\frac{\partial^3 u}{\partial x^3} = 0$	$\frac{\partial^3 u}{\partial x^3} = 0$	$\frac{\partial M}{\partial x} = 0$ (Shearing force)

Free-Free Beam Frequency (cont)

- Applying B.C.'s, get A=C and B=D, and

$$\begin{bmatrix} (\cosh k\ell - \cos k\ell) & (\sinh k\ell - \sin k\ell) \\ (\sinh k\ell + \sin k\ell) & (\cosh k\ell - \cos k\ell) \end{bmatrix} \begin{bmatrix} \mathcal{A} \\ \mathcal{B} \end{bmatrix} = 0 \quad (3)$$

- Setting the determinant = 0 yields

$$\cos k\ell = \frac{1}{\cosh k\ell}$$

- Which has roots at

$$\underbrace{k_1\ell = 4.730 \qquad k_2\ell = 7.853 \qquad k_3\ell = 10.996}_{\text{These values of } k_n\ell \text{ correspond to the different modes of vibration!}}$$

- Substituting (2) into (1) finally yields:

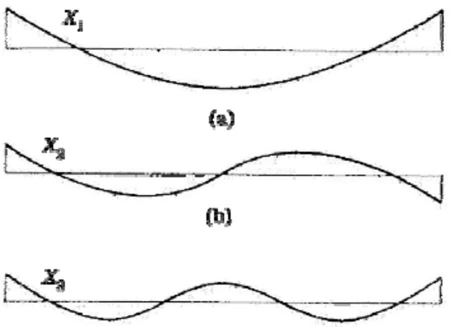
$$k^4 = \frac{\rho A}{EI}\omega^2 \longrightarrow \boxed{f_n = \frac{(k_n\ell)^2}{2\pi\ell^2}\sqrt{\frac{EI}{\rho A}}}$$

[Free-Free Beam Frequency Equation]

Higher Order Free-Free Beam Modes

Mode	n	Nodal Points	$k_n\ell$	f_n/f_1
Fundamental (f_1)	1	2	4.730	1.000
1st Harmonic	2	3	7.853	2.757
2nd Harmonic	3	4	10.996	5.404
3rd Harmonic	4	5	14.137	8.932
4th Harmonic	5	6	17.279	13.344

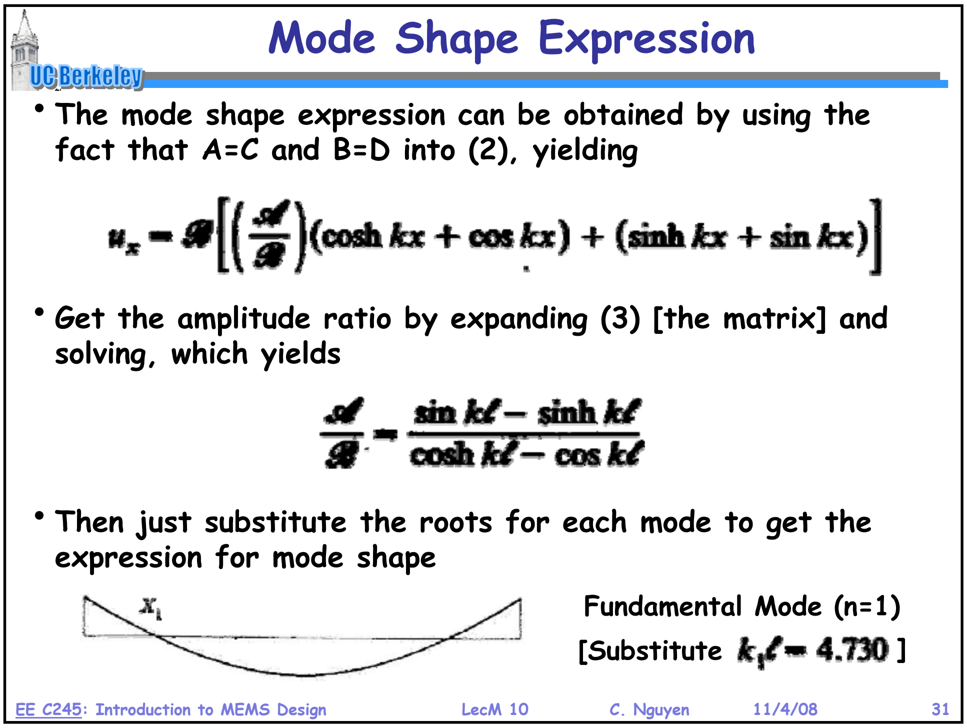
← More than 10x increase



Fundamental Mode (n=1)

1^{st} Harmonic (n=2)

2^{nd} Harmonic (n=3)



Mode Shape Expression

- The mode shape expression can be obtained by using the fact that A=C and B=D into (2), yielding

$$u_x = \mathscr{B}\left[\left(\frac{\mathscr{A}}{\mathscr{B}}\right)(\cosh kx + \cos kx) + (\sinh kx + \sin kx)\right]$$

- Get the amplitude ratio by expanding (3) [the matrix] and solving, which yields

$$\frac{\mathscr{A}}{\mathscr{B}} = \frac{\sin k\ell - \sinh k\ell}{\cosh k\ell - \cos k\ell}$$

- Then just substitute the roots for each mode to get the expression for mode shape

Fundamental Mode (n=1)
[Substitute $k_1\ell = 4.730$]