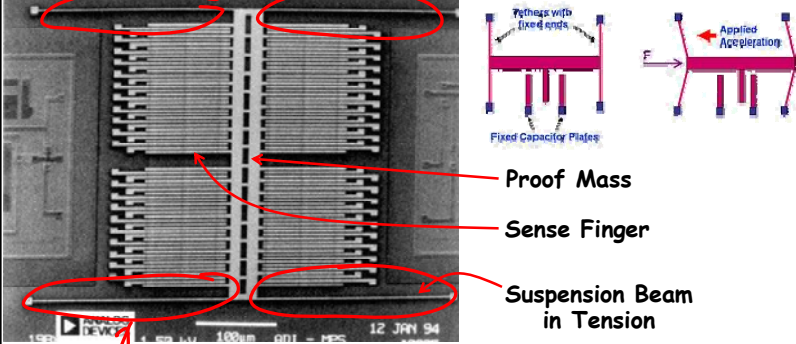


* $\omega = \sqrt{\frac{K}{m}}$ \Rightarrow good for problems where the mass & stiffness can be separated, i.e., they're distinct

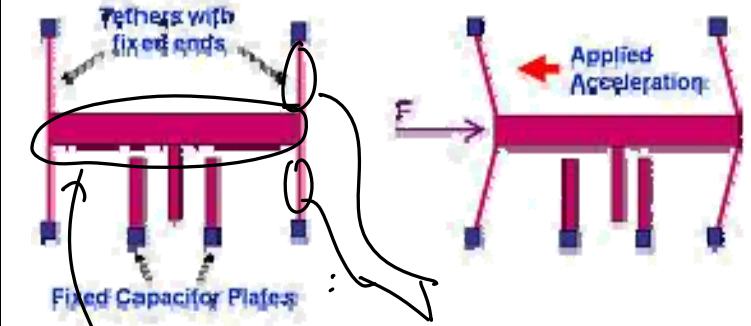
Ex. ADXL-50 Accelerometer

- The proof mass of the ADXL-50 is many times larger than the effective mass of its suspension beams
 - Can ignore the mass of the suspension beams (which greatly simplifies the analysis)
- Suspension Beam: $L = 260 \mu\text{m}$, $h = 2.3 \mu\text{m}$, $W = 2 \mu\text{m}$



In fabrication, purposely introduce a tensile stress in the beams!

a large ω_0 !

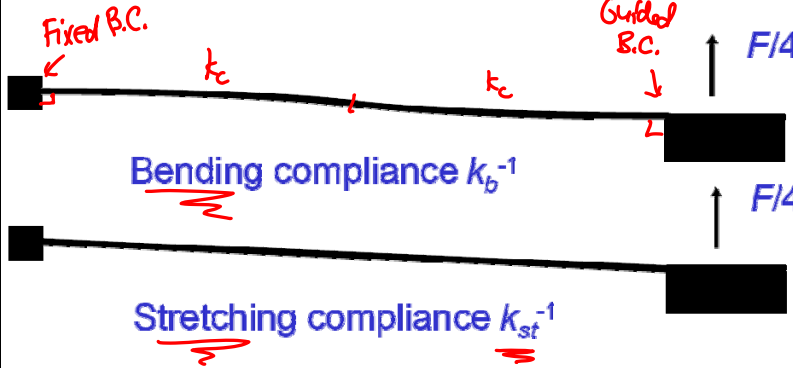


mass of the structure \gg mass of springs
 \therefore ignore the mass of the springs

stiffness of springs \ll stiffness of structure
 \therefore ignore the stiffness of the structure

For the ADXL-50: 60% of the mass comes from sense fingers $\rightarrow M = 162 \text{ ng}$

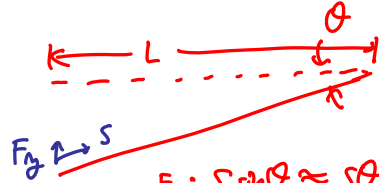
Suspension: Four tensioned beams



Bending Contribution

$$k_b^{-1} = \left(\frac{1}{k_c} + \frac{1}{k_e}\right) = 2 \left(\frac{(L/2)^3}{3E(hw^3/12)}\right) = \frac{L^3}{Ehw^3} = 4.2 \mu\text{m}/\mu\text{N}$$

Stretching Contribution



$$F_s = S \sin \theta \approx S \theta \approx S \left(\frac{s}{L}\right) = \left(\frac{S}{L}\right) s$$

k_{st}

$$k_{st}^{-1} = \frac{L}{S} = \frac{L}{\sigma_r W h} = 1.14 \mu\text{m}/\mu\text{N}$$

To get the total spring constant
add the bending stiffness to
the stretching:

$$k = 4(k_b + k_{st}) = 4(0.24 + 0.88) = 4.5 \mu\text{N}/\mu\text{m} \approx 4.5 \text{N/m}$$

4.48

Now, get resonance freq.:

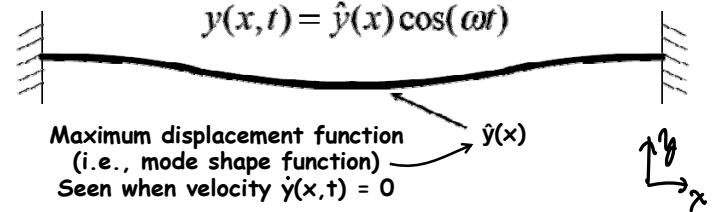
$$f = \frac{1}{2\pi} \sqrt{\frac{k}{M}} = \sqrt{\frac{4.48 \text{ N/m}}{162 \times 10^{-12} \text{ kg}}} = 26.5 \text{ kHz}$$

ADXL-50 Data Sheet: $f_0 = 24 \text{ kHz}$

difference?
capacitive transduction
& electrical stiffness

Find Resonance Frequency When Mass & Stiffness is Distributed

• Vibrating structure displacement function:



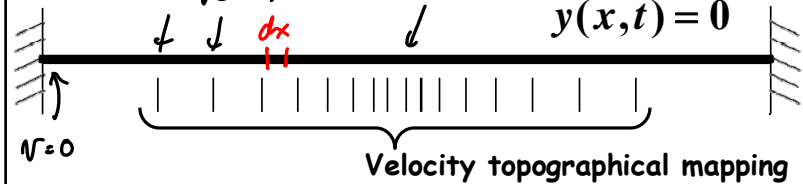
• Procedure for determining resonance frequency:

- ⊗ Use the static displacement of the structure as a trial function and find the strain energy W_{max} at the point of maximum displacement (e.g., when $t=0, \pi/\omega, \dots$)
- ⊗ Determine the maximum kinetic energy when the beam is at zero displacement (e.g., when it experiences its maximum velocity)
- ⊗ Equate energies and solve for frequency

Get Maximum Kinetic Energy

$$\text{velocity: } v(x,t) = \frac{\partial y(x,t)}{\partial t} = -\omega \hat{y}(x) \sin \omega t$$

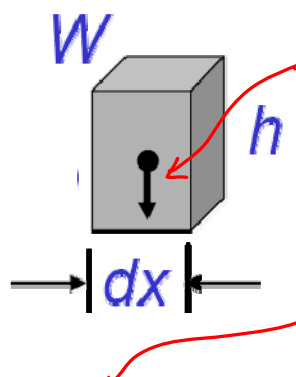
smaller velocities ← largest velocity



When $y(x,t) = 0$, all the energy in the structure is kinetic. ($v \neq 0$)

$$v(x, \frac{(2m+1)\pi}{2\omega}) = -\omega \hat{y}(x)$$

$t = \frac{\pi}{2\omega}, \frac{3\pi}{2\omega}, \dots$



velocity:
 $v = -\dot{w} q(x)$
 $\frac{(2m+1)\pi}{2w}$

$dK = \frac{1}{2} \cdot dm \cdot [v(x,t)]^2$

$dm = \rho (Wh dx)$
 ↑
 density

Maximum K.E.:
 $K_{max} = \int_0^L \frac{1}{2} \rho Wh dx v^2(x,t) = \int_0^L \frac{1}{2} \rho Wh \dot{w}^2 [q(x)]^2 dx$

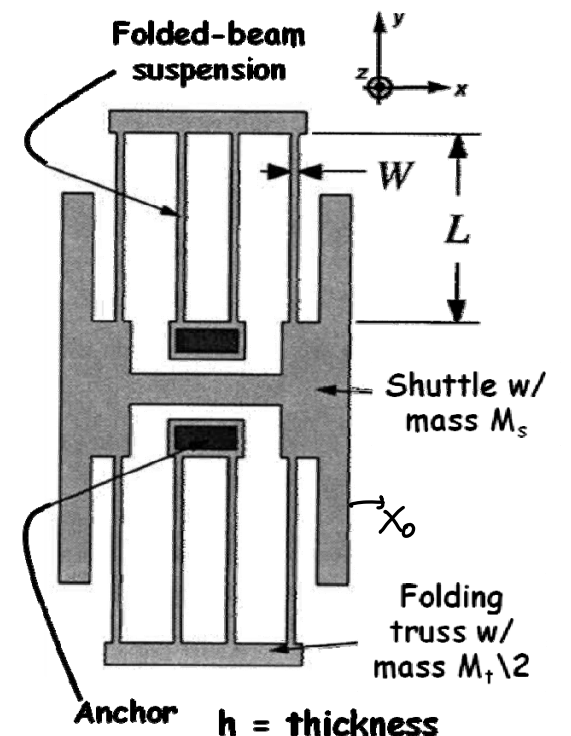
To get frequency:
 $K_{max} = W_{max}$

$$\omega = \sqrt{\frac{W_{max}}{\int_0^L \frac{1}{2} \rho Wh [q(x)]^2 dx}}$$

[radians/s]

ω = radian resonance freq.
 W_{max} = maximum potential energy
 ρ = density of the structural material
 W = beam width
 h = " thickness
 $q(x)$ = resonance mode shape

Resonance Freq. of a folded-Beam Resonator



Folded-beam suspension

Shuttle w/ mass M_s

Folding truss w/ mass $M_t/2$

Anchor $h = \text{thickness}$

- Derive an expression for the resonance frequency of the above structure

Use the Rayleigh-Ritz Method: (energy method)

$K_{max} = W_{max}$

Find the kinetic energy + one piece at a time

$$K_{max} = \underbrace{K_s}_{\text{shuttle}} + \underbrace{K_t}_{\text{truss}} + \underbrace{K_b}_{\text{beams}}$$

$$K_{max} = \frac{1}{2} N_s^2 M_s + \frac{1}{2} N_t^2 M_t + \frac{1}{2} \int N_b^2 dM_b$$

\uparrow
 mass of both
 trusses

Velocity of Shuttle: $N_s = \omega_0 X_0$

\uparrow resonance
 freq. \nwarrow maximum displacement
of the shuttle

$\therefore K_s = \frac{1}{2} N_s^2 M_s = \frac{1}{2} \omega_0^2 X_0^2 M_s$

Velocity of Truss: $N_t = \frac{1}{2} N_s = \frac{1}{2} \omega_0 X_0$

$\therefore K_t = \frac{1}{2} \left(\frac{1}{2} \omega_0 X_0\right)^2 M_t = \frac{1}{8} \omega_0^2 X_0^2 M_t$

\uparrow
 mass of both
 trusses

Velocity of the Beam Segment:

Quasistatic B.C.
 fixed B.C.
 $\hat{x}(y) = ?$
 assume the mode
 shape is the same as
 the static displacement
 shape

Segment [AB]:

$$\hat{x}(y) = \frac{F_x}{48EIz} (3Ly^2 - 2y^3), \quad 0 \leq y \leq L \quad (1)$$

At $y=L$: $x(L) = \frac{X_0}{2} = \frac{F_x L^3}{48EIz} \leftarrow$ B.C.

Substitute into (1):

$$\hat{x}(y) = \frac{X_0}{2} \left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3 \right]$$

which yields for velocity:

$$N_b(y)|_{[AB]} = \frac{X_0}{2} \left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3 \right] \omega_0$$

Plugging into the expression for K_b :

$$\begin{aligned}
 K_{[AB]} &= \frac{1}{2} \int_0^L \frac{X_0^2 \omega_0^2}{4} \left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3 \right]^2 dM_{[AB]} \\
 &= \frac{X_0^2 \omega_0^2}{8L} \underbrace{M_{[AB]}}_{\substack{\uparrow \\ \text{mass per unit length}}} \int_0^L \left[3\left(\frac{y}{L}\right)^2 - 2\left(\frac{y}{L}\right)^3 \right]^2 dy
 \end{aligned}$$

$M_{[AB]}$: static mass

$$K_{[AB]} = \frac{13}{280} X_0^2 \omega_0^2 M_{[AB]}$$