EE C247B – ME C218 Introduction to MEMS Design Spring 2015

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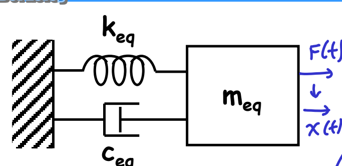
Lecture Module 13: Equivalent Circuits II

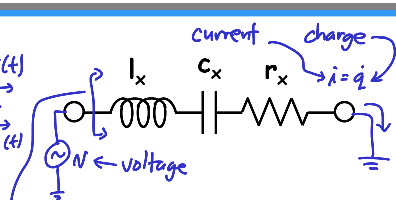
Lecture Outline

- Reading: Senturia, Chpt. 6, Chpt. 14
- Lecture Topics:
  - Input Modeling
    - Force-to-Velocity Equiv. Ckt.
    - Input Equivalent Ckt.
  - Current Modeling
    - Output Current Into Ground
    - Input Current
    - Complete Electrical-Port Equiv. Ckt.
  - Impedance & Transfer Functions

Input Modeling

Electromechanical Analogies





$F(t) = F\cos(\omega t) \rightarrow x(t) = X\cos\omega t$

Equation of Motion:

$m_{eq}\ddot{x} + c_{eq}\dot{x} + k_{eq}x = F(t)$

⇒ using phasor concepts:

$F = j\omega m_{eq}\dot{x} + \frac{k_{eq}}{j\omega}\dot{x} + c_{eq}\dot{x}$

⇒ by analogy:

$F \rightarrow v$	$m_{eq} \rightarrow l_x$	$c_{eq} \rightarrow r_x$
$\dot{x} \rightarrow i$	$k_{eq} \rightarrow \frac{1}{c_x}$	

[Parameter Relationships in the Current Analogy]

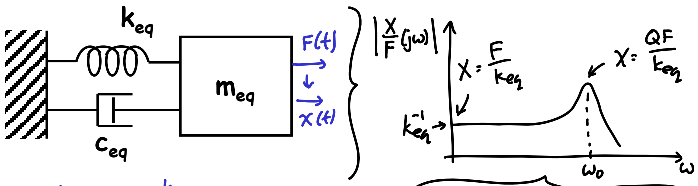
$v(t) = V\cos\omega t \rightarrow i(t) = I\cos\omega t$

Impedance looking in:

$\frac{v}{i} = j\omega l_x + \frac{1}{j\omega c_x} + r_x$

$v = j\omega l_x i + \frac{(1/c_x)}{j\omega} i + r_x i$

Bandpass Biquad Transfer Function



$F = j\omega m_{eq}\dot{x} + \frac{k_{eq}}{j\omega}\dot{x} + c_{eq}\dot{x}$

$\Rightarrow$ Converting to full phasor form:

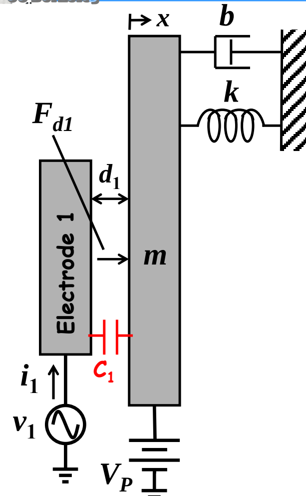
$F = (j\omega)(j\omega X)m_{eq} + \frac{k_{eq}}{j\omega}(j\omega X) + c_{eq}(j\omega X)$

$\frac{X}{F}(j\omega) = \frac{1}{k_{eq}}\left[-\omega^2\frac{m_{eq}}{k_{eq}} + 1 + j\frac{c_{eq}\omega}{k_{eq}}\right]^{-1} = \frac{1}{k_{eq}}\left[-\left(\frac{\omega}{\omega_o}\right)^2 + 1 + j\frac{\omega}{Q\omega_o}\right]^{-1}$

$\left[\frac{k_{eq}}{m_{eq}} = \omega_o^2,\ Q = \frac{m_{eq}\omega_o}{c_{eq}} = \frac{k_{eq}}{\omega_o c_{eq}} \rightarrow \frac{k_{eq}}{c_{eq}} = Q\omega_o\right]$

$$\frac{X}{F}(j\omega) = \frac{k_{eq}^{-1}}{1-\left(\frac{\omega}{\omega_o}\right)^2 + j\frac{\omega}{Q\omega_o}}$$

Force-to-Velocity Relationship



- The relationship between input voltage v_1 and force F_{d1}:

$$F_{d1} \approx -V_P \frac{\partial C_1}{\partial x} v_1$$

- When displacement x is the mechanical output variable:

$$\frac{X(s)}{F_{d1}(s)} = \frac{1}{k}\frac{\omega_o^2}{s^2 + (\omega_o/Q)s + \omega_o^2}$$

s = jω

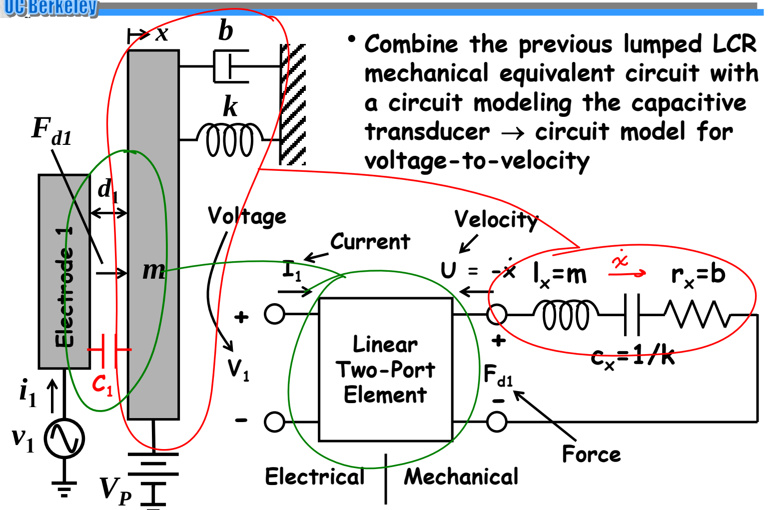
- When velocity υ is the mechanical output variable:

$$\frac{\upsilon(s)}{F_{d1}(s)} = \frac{sX(s)}{F_{d1}(s)} = \frac{1}{k}\frac{\omega_o^2 s}{s^2 + (\omega_o/Q)s + \omega_o^2}$$

×s

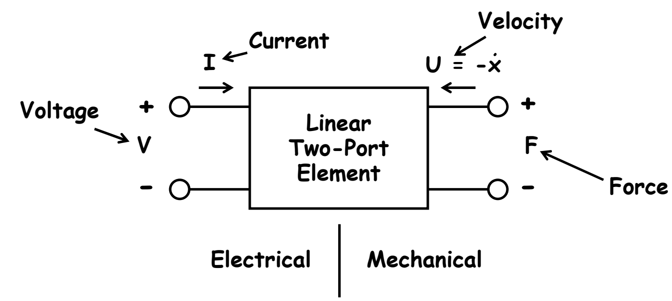
Force-to-Velocity Equiv. Ckt.

- Combine the previous lumped LCR mechanical equivalent circuit with a circuit modeling the capacitive transducer → circuit model for voltage-to-velocity

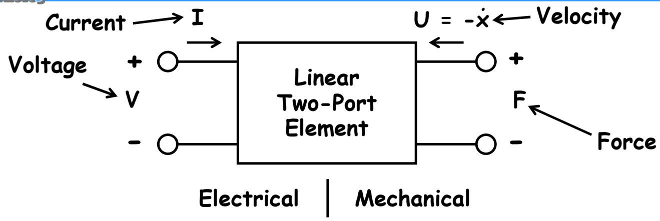


Equiv. Circuit for a Linear Transducer

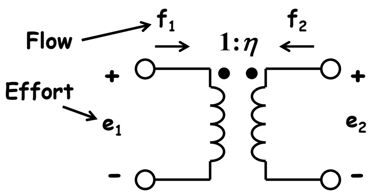
- A transducer …
  - converts energy from one domain (e.g., electrical) to another (e.g., mechanical)
  - has at least two ports
  - is not generally linear, but is virtually linear when operated with small signals (i.e., small displacements)



Equiv. Circuit for a Linear Transducer



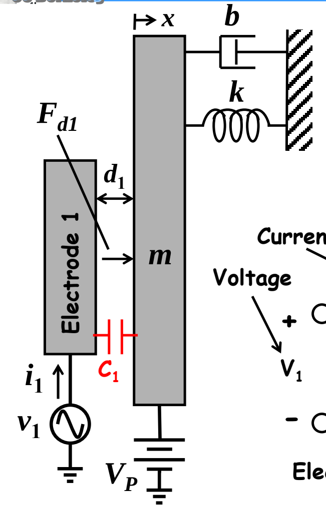
- For physical consistency, use a transformer equivalent circuit to model the energy conversion from the electrical domain to mechanical domain



$$\begin{bmatrix} e_2 \\ f_2 \end{bmatrix} = \begin{bmatrix} \eta & 0 \\ 0 & -\frac{1}{\eta} \end{bmatrix} \begin{bmatrix} e_1 \\ f_1 \end{bmatrix}$$

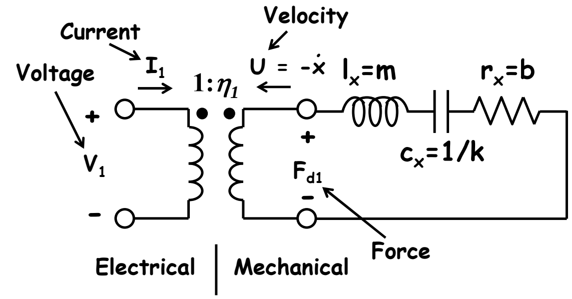
Describing Matrix

Electromechanical Equivalent Circuit

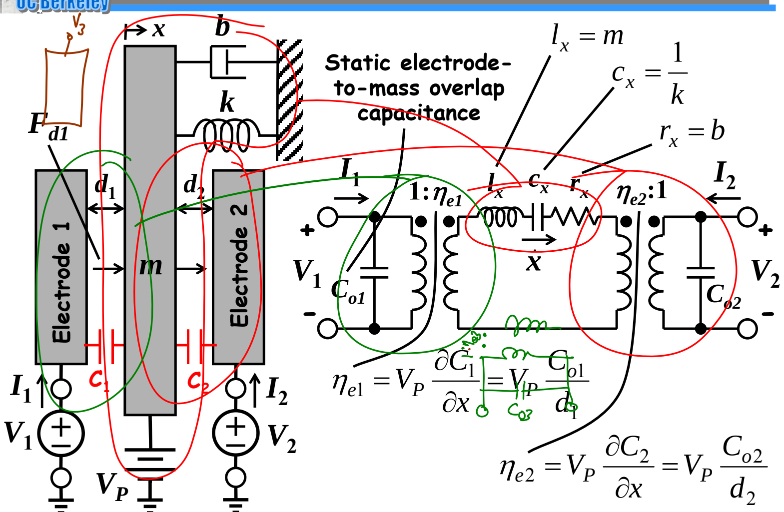


- $e_2 = F_{d1}$, $e_1 = v_1$, just need η_1:
- From the matrix: $e_2 = \eta e_1$

$$F_{d1} \approx -V_P \frac{\partial C_1}{\partial x} v_1 \longrightarrow \eta_1 = \left| V_P \frac{\partial C_1}{\partial x} \right|$$



Complete Electrical-Port Equiv. Circuit



$$\eta_{e1} = V_P \frac{\partial C_1}{\partial x} = V_P \frac{C_{o1}}{d_1}$$

$$\eta_{e2} = V_P \frac{\partial C_2}{\partial x} = V_P \frac{C_{o2}}{d_2}$$