

Lecture 9: Mechanics of Materials I

- Announcements:
- Module 6 on Bulk Micromachining online
- Module 7 on Mechanics of Materials online
- HW#2 due this coming Friday morning
- Wednesday Office Hours will change to 2:30-3:30 p.m. starting this week

- Reading: Senturia Chpt. 3, Jaeger Chpt. 11, Handouts: "Bulk Micromachining of Silicon"

• Lecture Topics:

- ↳ Bulk Micromachining
- ↳ Anisotropic Etching of Silicon
- ↳ Boron-Doped Etch Stop
- ↳ Electrochemical Etch Stop
- ↳ Isotropic Etching of Silicon
- ↳ Deep Reactive Ion Etching (DRIE)
- ↳ Wafer Bonding

- Reading: Senturia, Chpt. 8

• Lecture Topics:

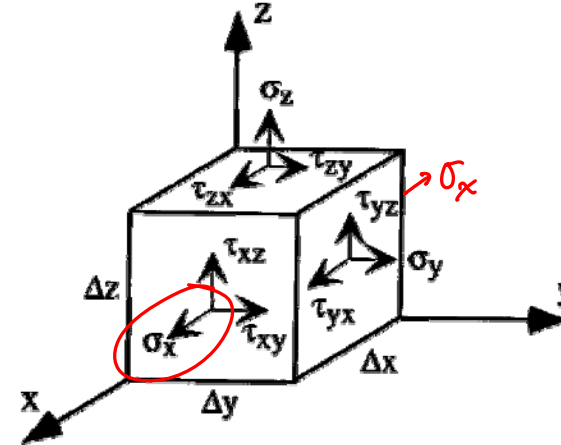
- ↳ Stress, strain, etc., for isotropic materials
- ↳ Thin films: thermal stress, residual stress, and stress gradients
- ↳ Internal dissipation
- ↳ MEMS material properties and performance metrics

- Last Time: Going thru Module 6 ... finish this

- Move on to Module 7

Example. Exercise the "terms"

⇒ determine the volume change ΔV for a uniaxial stress (along the x-direction)



Upon application of σ_x , what is ΔV ?

$$\left. \begin{aligned} \Delta x &\rightarrow \Delta x(1 + \epsilon_x) \\ \Delta y &\rightarrow \Delta y(1 - \nu \epsilon_x) \\ \Delta z &\rightarrow \Delta z(1 - \nu \epsilon_x) \end{aligned} \right\} \begin{array}{l} \text{assuming isotropic} \\ \text{material} \\ \downarrow \\ \text{same } \nu \text{ along } y \text{ \& } z \end{array}$$

The resulting change in volume: ΔV

$$\Delta V = \underbrace{\Delta x \Delta y \Delta z}_{\text{volume after application of } \sigma_x} (1 + \epsilon_x)(1 - \nu \epsilon_x)^2 - \Delta x \Delta y \Delta z$$

$$= \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - \nu \epsilon_x)^2 - 1]$$

[Assume small strains] $\Rightarrow (1 + m x)^n \approx 1 + n m x$

$$\Delta V = \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - 2\nu \epsilon_x) - 1]$$

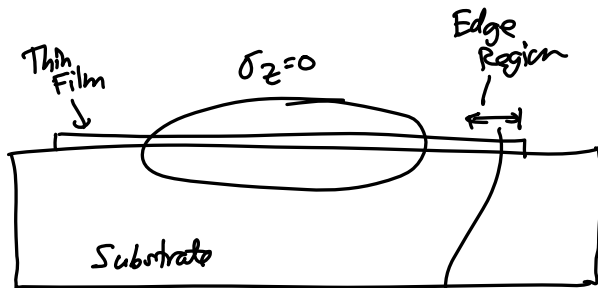
$$\Delta V = \Delta x \Delta y \Delta z (1 - 2\nu) \epsilon_x$$

For $\nu = 0.5$ (rubber) \rightarrow no ΔV !

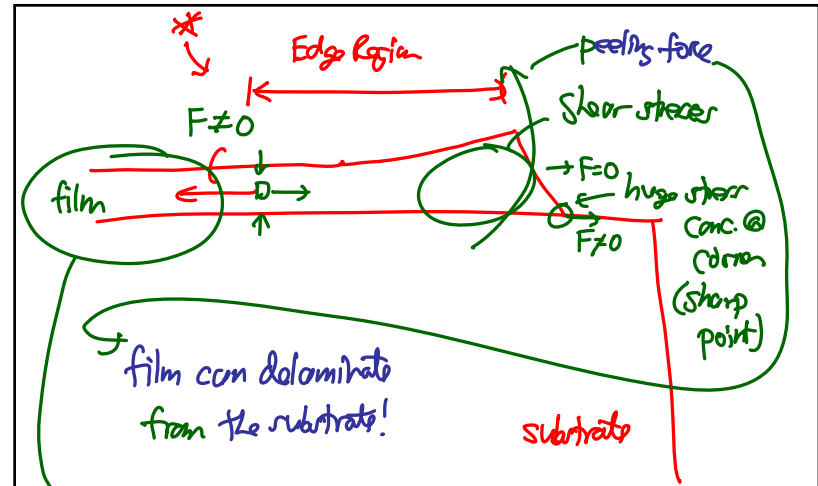
$\nu < 0.5 \rightarrow$ finite ΔV

Important Case: Plane Stress

\Rightarrow common case for a thin-film coating on a rigid substrate:



3 thicknesses from the edge
 Zoom-in
 *



Take a closer look @ this region: $\sigma_z = 0$
 Get two components of stress:

$$\epsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + 0)]$$

$$\epsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x + 0)]$$

Assume: Plane Stress \rightarrow isotropic $\rightarrow \sigma_x = \sigma_y = \sigma$
 (symmetry in the xy-plane)

$$\epsilon_x = \frac{1}{E} [\sigma - \nu\sigma]$$

$$\epsilon_x = \epsilon_y = \epsilon$$

$$= \frac{\sigma}{\left(\frac{E}{1-\nu}\right)} \Rightarrow \epsilon_x = \frac{\sigma}{E'}$$

where $E' \triangleq$ Biaxial Modulus $= \frac{E}{1-\nu}$

Linear Thermal Expansion

temperature $T \rightarrow$ solids (generally) expand in volume

Definition. Linear Thermal Expansion Coefficient

$$\left. \begin{array}{l} \text{Linear Thermal} \\ \text{Exp. Coefficient} \end{array} \right\} \triangleq \alpha_T = \frac{d\epsilon_x}{dT} \quad [\text{kelvin}^{-1}]$$

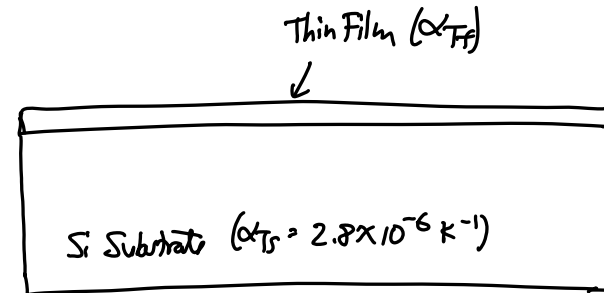
Remarks:

- ① α_T values tend to be in the 10^{-6} to 10^{-3} range.
- ② $10^{-6} \text{ K}^{-1} = 1 \mu\text{strain/K}$ \rightarrow
- ③ In 3D, get a volume thermal exp. coefficient

$$\frac{\Delta V}{V} = 3\alpha_T \Delta T$$

- ④ For moderate ΔT 's $\rightarrow \alpha_T \approx \text{constant}$
 for larger ΔT , then $\alpha_T = f(T)$

Ex. Thin-film Thermal Stress



Assume:

- ① Substrate is much thicker than the film.
- ② Film is deposited stress free @ $T_d \leftarrow$ deposition temperature
- ③ Then the whole thing is cooled to room temperature, T_r .

Thermal Strain of the Substrate: (in one plane dimension)

$$\epsilon_s = -\alpha_{TS} \Delta T, \text{ where } \Delta T = T_d - T_r$$

If the film were not attached to the substrate:

$$\epsilon_{f, \text{free}} = -\alpha_{TF} \Delta T$$

But the film is attached to the substrate

\Rightarrow thickness sub \gg thickness film

\therefore substrate wins!



*
 Thus, the actual strain experienced by the film is that of the substrate:

$$\epsilon_{f, attached} = -\alpha_{TS} \Delta T$$

Thus:

Thermal Mismatch Strain: $\epsilon_{f, mismatch}$
 $= (\alpha_{TF} - \alpha_{TS}) \Delta T$

↳ Note this is biaxial strain (assuming the film is deposited isotropically onto the substrate)

$$\sigma_{f, mismatch} = \underbrace{\left(\frac{E}{1-\nu} \right)}_{E'} \epsilon_{f, mismatch}$$

Ex. Thin film is polyimide $\rightarrow \alpha_{TF} = 70 \times 10^{-6} \text{ K}^{-1}$
 $E' = 4 \text{ GPa}$
 deposited @ 250°C , film cooled to $RT = 25^\circ\text{C}$
 $\Delta T = 225 \text{ K}$

$$\epsilon_{f, mismatch} = (70 - 2.8) \mu (225) = 1.5 \times 10^{-2}$$

[$\mu = 10^{-6}$, $m = 10^{-3}$, $k = 10^3$, $G = 10^9$]

$$\sigma_{f, mismatch} = (4G)(1.5 \times 10^{-2}) = 60.5 \text{ MPa}$$

$\text{SiO}_2 \rightarrow$ stress is (+) \rightarrow tensile
 (-) would be compressive