

Lecture 11: Mechanics of Materials II

• Announcements:

- HW#3 online and due next Wednesday morning
- Prof. Nguyen's Wednesday Office Hours have changed to 12:30-1:30 p.m.

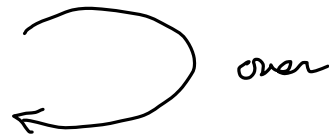
• Reading: Senturia, Chpt. 8

6 new
10 evening 5:00-7

• Lecture Topics:

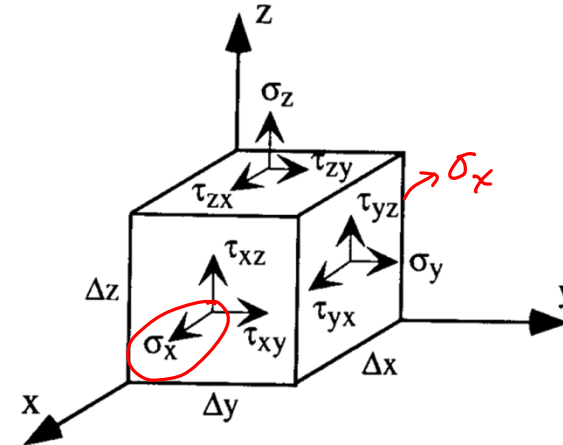
- ↳ Stress, strain, etc., for isotropic materials
- ↳ Thin films: thermal stress, residual stress, and stress gradients
- ↳ Internal dissipation
- ↳ MEMS material properties and performance metrics

• Last Time:



Example. Exercise the "terms"

⇒ Determine the volume change ΔV for a uniaxial stress (along the x-direction)



Upon application of σ_x , what is ΔV ?

$$\begin{aligned} \Delta x &\rightarrow \Delta x(1 + \epsilon_x) && \text{(as a result of application of } \sigma_x) \\ \Delta y &\rightarrow \Delta y(1 - \nu \epsilon_x) \\ \Delta z &\rightarrow \Delta z(1 - \nu \epsilon_x) \end{aligned} \left. \begin{array}{l} \\ \\ \end{array} \right\} \begin{array}{l} \text{assuming isotropic} \\ \text{material} \rightarrow \text{same } \nu \\ \text{along } y \text{ \& } z \end{array}$$

The resulting change in volume: ΔV

$$\Delta V = \underbrace{\Delta x \Delta y \Delta z (1 + \epsilon_x) (1 - \nu \epsilon_x)^2}_{\text{volume after application of } \sigma_x} - \Delta x \Delta y \Delta z$$

$$= \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - \nu \epsilon_x)^2 - 1]$$

[Assume small strains] $\Rightarrow (1 + m\epsilon)^n \approx 1 + nm\epsilon$

$$\Delta V = \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - 2\nu \epsilon_x) - 1]$$

$$\Delta V = \Delta x \Delta y \Delta z (1 - 2\nu) \epsilon_x$$

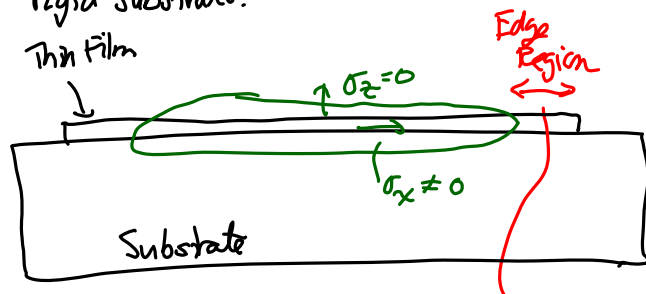
For $\nu = 0.5$ (rubber) \rightarrow no ΔV

$\nu < 0.5 \rightarrow$ finite ΔV

Module 7, pg. (13)

Important Case: Plane Stress

\Rightarrow common case for a thin-film coating on a rigid substrate:



3 thicknesses from the edge
Zoom-in *

where $E' \triangleq$ Biaxial Modulus $= \frac{E}{1-\nu^2}$

Linear Thermal Expansion

temperature \uparrow \rightarrow solids expand in volume

Definition. Linear Thermal Expansion Coefficient

Linear Thermal Expansion Coeff. $\triangleq \alpha_T = \frac{d\epsilon_x}{dT}$ [Kelvin⁻¹]

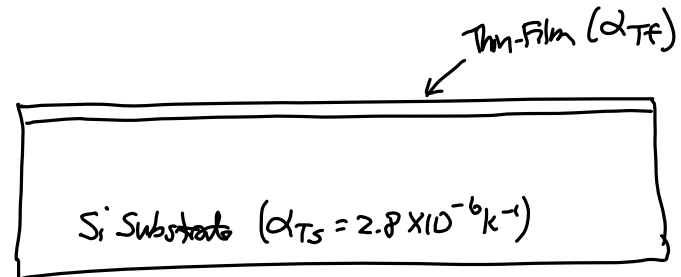
Remarks.

- ① α_T values tend to be in the 10^{-6} to 10^{-7} range.
- ② $10^{-6} \text{ K}^{-1} = 1 \mu\text{strain/K}$
- ③ In 3D, get a volume thermal expansion coeff.

$$\frac{\Delta V}{V} = 3\alpha_T \Delta T$$

- ④ For moderate ΔT 's $\rightarrow \alpha_T \approx$ constant
 \downarrow
 for large ΔT , then $\alpha_T = f(T)$

Example. Thin-Film Thermal Stress



Assume.

- ① Substrate is much thicker than the film.
- ② Film is deposited stress free @ $T_d \leftarrow$ deposition temperature
- ③ Then, the whole thing is cooled to room temperature: T_r

Thermal Strain of the Substrate: (in one plane dimension)

$$\epsilon_s = -\alpha_{TS} \Delta T, \text{ where } \Delta T = T_d - T_r$$

If the film were not attached to the substrate

$$\epsilon_{f, \text{free}} = -\alpha_{TF} \Delta T$$

But if the film is attached to the substrate:

thickness substrate \Rightarrow thickness of the film

\therefore substrate wins!

\hookrightarrow the substrate dictates the actual strain experienced by the film:

$$\epsilon_{f, \text{attached}} = -\alpha_{TS} \Delta T$$

Thus.

$$\text{Thermal Mismatch Strain} = \epsilon_{f, \text{mismatch}} \\ = (\alpha_{Tf} - \alpha_{Ts}) \Delta T$$

Note: This is biaxial strain (assuming the film is deposited isotropically onto the substrate)

$$\sigma_{f, \text{mismatch}} = \underbrace{\left(\frac{E}{1-\nu} \right)}_{E'} \epsilon_{f, \text{mismatch}}$$

Ex. Thin film is polyimide $\rightarrow \alpha_{Tf} = 70 \times 10^{-6} \text{ K}^{-1}$

$$E' = 46 \text{ GPa}$$

deposited @ 250°C, then cool to room temp = 25°C

$$\Delta T = 225 \text{ K}$$

$$\epsilon_{f, \text{mismatch}} = (70 - 2.8) \mu (225) = 1.5 \times 10^{-2}$$

$$[\mu = 10^{-6}, m = 10^{-3}, k = 10^3, G = 10^9]$$

$$\sigma_{f, \text{mismatch}} = (46) (1.5 \times 10^2) = 60.5 \text{ MPa}$$

\uparrow
10⁹

stress is (+) \rightarrow tensile

[-] would be compressive