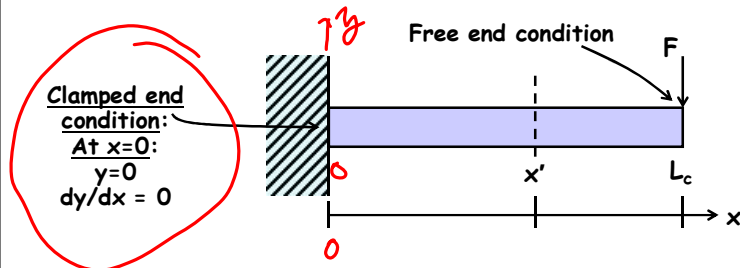


Lecture 13: Beam Bending II

- Announcements:
- HW#3 due Wednesday morning
- HW#4 online soon
- Midterm Exam two weeks away, Thursday, March 17, 5:10-7 p.m. in 3107 Etcheverry
-
- Reading: Senturia, Chpt. 9
- Lecture Topics:
 - ↳ Bending of beams
 - ↳ Cantilever beam under small deflections
 - ↳ Combining cantilevers in series and parallel
 - ↳ Folded suspensions
 - ↳ Design implications of residual stress and stress gradients

• Last Time:

Problem: Bending a Cantilever Beam



- Objective: Find relation between tip deflection $y(x=L_c)$ and applied load F
- Assumptions:
 1. Tip deflection is small compared with beam length
 2. Plane sections (normal to beam's axis) remain plane and normal during bending, i.e., "pure bending"
 3. Shear stresses are negligible

Forces & Moments

Moment due to F_i here = $M_i = FL$

Reaction Force (to maintain equilibrium)

equal & opposite to

Moment due to $F_i = M_2 = F_i(L-x')$

$F_{x'i} = F$

$M_{x'i} = F_i(L-x')$

$M_{x'r} = M_{x'i} = F_i(L-x')$

$F_{x'r} = F_i$

Total Force: $-F_R + F_{x'i} = -F + F = 0 \checkmark$

Total Moment: $-M_R + M_{x'i} + x'F_{x'i}$
 $= -FL + F(L-x') + x'F = 0 \checkmark$

Bent Beam (bent by applied force)
 ⇒ cantilever

Fixed Free
 tension compression
 neutral axis
 F
 h
 dx
 $d\theta$
 above the neutral axis
 Tension Neutral Axis
 M_0 M_0
 R $d\theta$ h
 below neutral axis
 Compression
 Combine to generate forces → moments
 that against the moment due to force F
 ↓
 This is how stiffness is generated!
 ↳ k_c → we want this!

Beam Segment in Pure Bending

⇒ Consider the segment bounded by the dashed lines defining $d\theta$

At $z=0$: neutral axis → segment length = $dx = R d\theta$ (1)

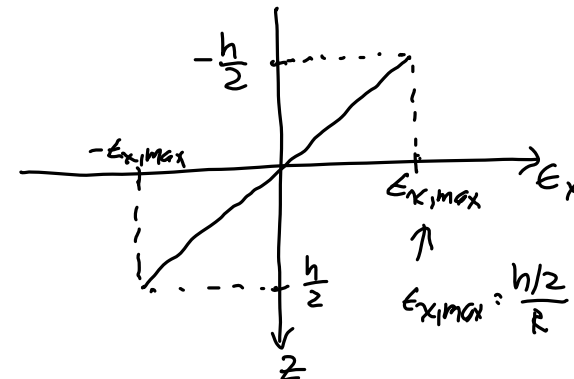
At any z : segment length = $dL = (R-z) d\theta$ (2)

Combine (1) & (2): $dL = dx - z d\theta = dx - \frac{z}{R} dx$

Thus, the axial strain @ z : $\epsilon_x = \frac{dL - dx}{dx} = -\frac{z}{R}$

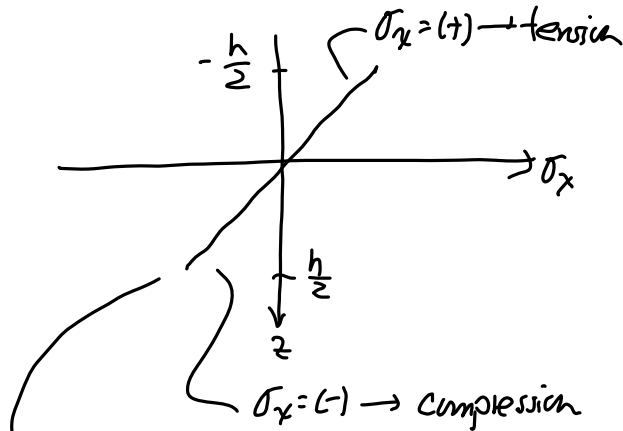
$$\epsilon_x = -\frac{z}{R}$$

Thus, the strain varies linearly along beam thickness:



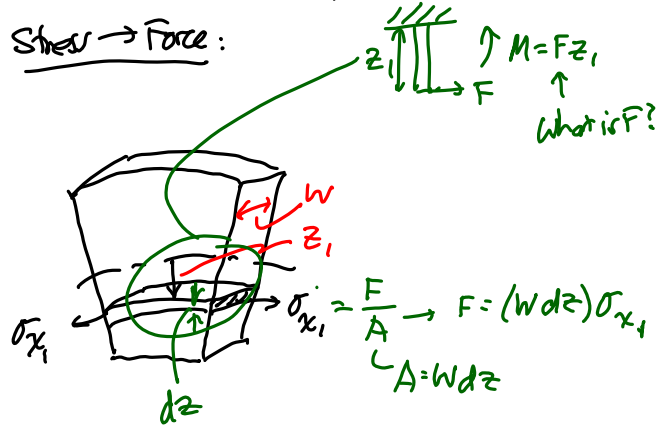
Of course, there is a corresponding axial stress:

$$\sigma_x = \epsilon_x E = \boxed{-\frac{zE}{R} = \sigma_x}$$



This gradient of stress generates a bending moment! → in response to the original applied moment (from F)

Stress → Force:



⇒ integrate stress through thickness of the beam:

$$M = \int_{-\frac{h}{2}}^{\frac{h}{2}} \underbrace{[w dz \sigma_x]}_{\text{force}} \cdot z$$

$$= - \int_{-\frac{h}{2}}^{\frac{h}{2}} \frac{E w z^2}{R} dz \Rightarrow \boxed{M = - \left(\frac{1}{12} w h^3 \right) \frac{E}{R}}$$

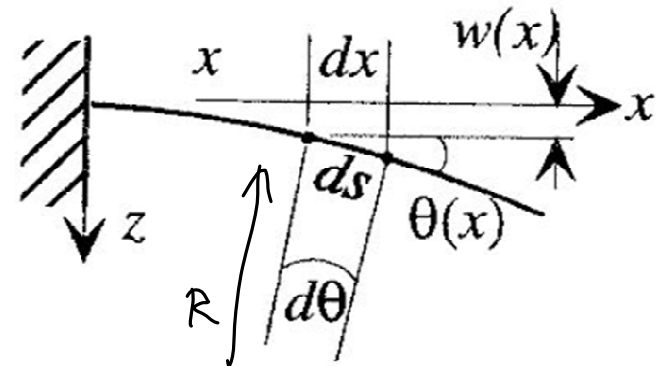
$$\left[\sigma_x = -\frac{zE}{R} \right]$$

$\frac{1}{12} w h^3 = I \triangleq$ Moment of Inertia

$$\boxed{\frac{1}{R} = -\frac{M}{EI}}$$

Note: (+) radius of curvature
↓
(-) internal bending moment

Differential Equation for Beam Bending



Write out some geometric relationships:

(then use small approximations)

$$\cos\theta = \frac{dx}{ds} \rightarrow ds = \frac{dx}{\cos\theta} \rightarrow ds \approx dx$$

$$\tan\theta = \frac{dw}{dx} = \text{slope of the beam @ this pt.} \rightarrow \theta \approx \frac{dw}{dx} \quad (1)$$

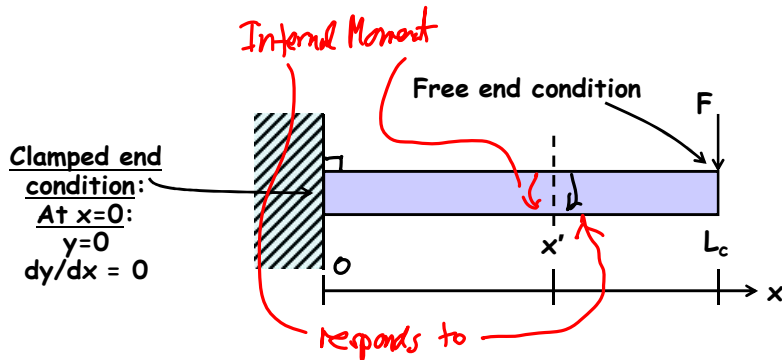
$$ds = R d\theta \rightarrow \frac{1}{R} = \frac{d\theta}{ds} \rightarrow \frac{1}{R} = \frac{d^2w}{dx^2} \quad (2)$$

Inserting (1) into (2):

$$\frac{1}{R} = \frac{d^2w}{dx^2} = -\frac{M}{EI}$$

Diff. Eq. for Small Angle Beam Bending

Cantilever Beam w/ Concentrated Load



Internal Moment @ position x : $M = -F(L-x)$

Thus:

$$\frac{d^2w}{dx^2} = \frac{F}{EI} (L-x)$$

$$w \begin{cases} \text{Clamped End B.C.: } w(x=0) = 0, \frac{dw}{dx}(x=0) = 0 \\ \text{Free End B.C.: none} \end{cases}$$

Solve for w :

\Rightarrow Use Laplace; or a trial solution:

$w = A + Bx + Cx^2 + Dx^3$, then apply B.C.'s

$$w = \frac{FL}{2EI} x^2 \left(1 - \frac{x}{3L}\right)$$

Deflection @ x due to a point load F applied @ $x=L$

Maximum Deflection \rightarrow occurs @ $x=L$:

$$w_{max} = \left(\frac{L^3}{3EI}\right) F \rightarrow F = \left(\frac{3EI}{L^3}\right) w(x=L)$$

$$= k_c w(x=L)$$

\downarrow
stiffness $\triangleq k_c$

where $k_c = \frac{3EI}{L^3}$

$$\left[I = \frac{1}{12} W h^3 \right] \rightarrow \boxed{k_c = \frac{1}{4} E W \frac{h^3}{L^3}}$$

Ex. $L = 100 \mu\text{m}, W = 2 \mu\text{m}, h = 2 \mu\text{m}$
 polysilicon $\rightarrow E = 150 \text{ GPa}$
 $k_c = \frac{1}{4} (150 \text{ G}) (2 \mu)^3 \left(\frac{2 \mu}{100 \mu} \right)^3 = \underline{\underline{0.6 \text{ N/m}}}$

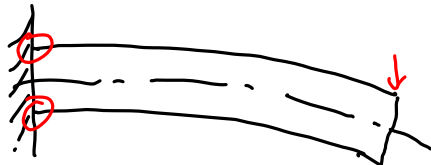
Maximum Stress in a Bent Cantilever

From before, the radius of curvature is given by

$$\frac{1}{R} = \frac{d^2 w}{dx^2} = \frac{F}{EI} (L-x)$$

$\Rightarrow \frac{1}{R}$ is maximized (i.e., R is minimized) when

$x=0:$
 $[x=0] \Rightarrow \frac{1}{R} = \frac{d^2 w}{dx^2} = \frac{FL}{EI}$



Strain is maximized: (@ $x=0$)

- ① At top surface \rightarrow tensile
- ② At bottom surface \rightarrow compressive

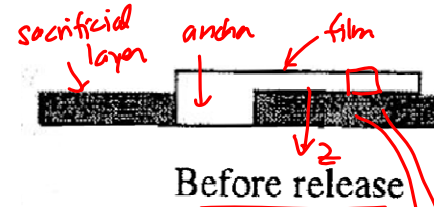
$$\epsilon_{\text{max}} = \frac{z}{R} = \frac{h}{2} \frac{1}{R} = \left(\frac{h}{2} \frac{FL}{EI} \right) = \epsilon_{\text{max}}$$

$$\left[I = \frac{1}{12} Wh^3 \right] \rightarrow \epsilon_{\text{max}} = \frac{k FL}{2 EI} \left(\frac{12}{Wh^3} \right) = \frac{6L}{EWh^2} F$$

$$\sigma_{\text{max}} = \epsilon_{\text{max}} E = \frac{6L}{Wh^2} F$$

(maximum stress in a bent cantilever subjected to a force F at its tip)

Stress Gradients in Cantilevers



- Process Flow
- ① Deposit film @ high temp
 - ② Cool it down
 - ⋮
 - ③ Release.

