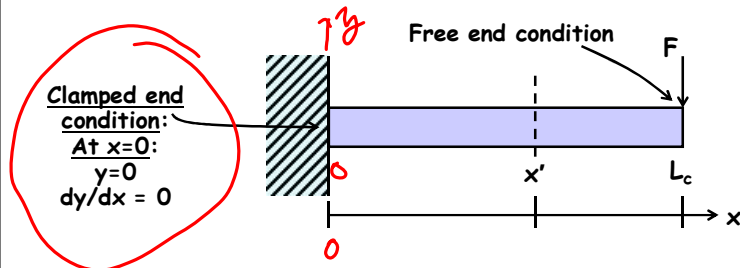


Lecture 14: Beam Combos

- Announcements:
- HW#4 online and due Friday, March 11, 8 a.m.
- Midterm Exam two weeks away, Thursday, March 17, 5:10-7 p.m. in 3107 Etcheverry
- -----
- Reading: Senturia, Chpt. 9
- Lecture Topics:
 - ↳ Bending of beams
 - ↳ Cantilever beam under small deflections
 - ↳ Combining cantilevers in series and parallel
 - ↳ Folded suspensions
 - ↳ Design implications of residual stress and stress gradients

• Last Time:

Problem: Bending a Cantilever Beam

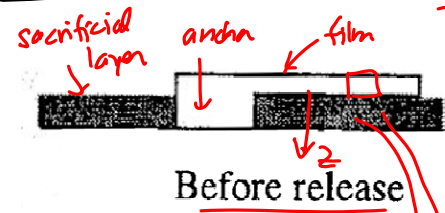


- **Objective:** Find relation between tip deflection $y(x=L_c)$ and applied load F
- **Assumptions:**
 1. Tip deflection is small compared with beam length
 2. Plane sections (normal to beam's axis) remain plane and normal during bending, i.e., "pure bending"
 3. Shear stresses are negligible

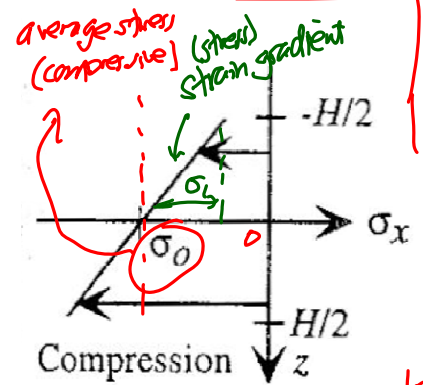
$$w = \frac{FL}{2EI} x^2 \left(1 - \frac{x}{3L}\right)$$

Deflection w due to a point load F applied @ $x=L$

Stress Gradients in Cantilevers



- Process Flow
- ① Deposit film @ high temp
 - ② Cool it down
 - ⋮
 - ③ Release.



After release, but before bending

Intermediate State

① Removed the sac. layer
beam free to do what it wants...

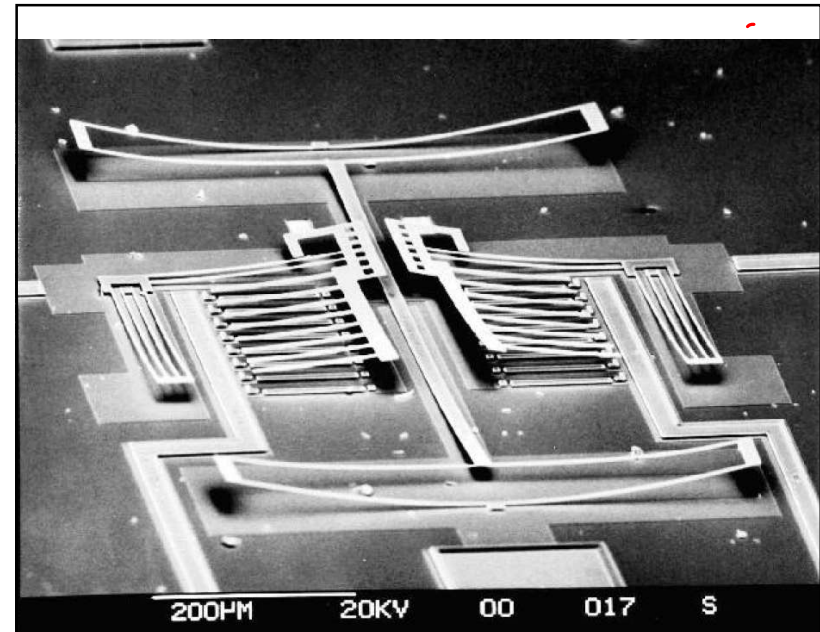
② beam stretches
↓ removes average axial stress

③ Bends to relieve stress gradient
↓ R=?

Stress after release but before bend

After stress relieved (State of minimum energy) → **After bending**

After bending



Bending Due to Stress Gradients

Find the radius of curvature.

Prior to release, axial stress: $\sigma = \sigma_0 \cdot \frac{\sigma_1}{(H/2)} z$

The internal moment:

$$M_x = \int_{-H/2}^{H/2} [(Wdz) \cdot \sigma] \cdot z = \int_{-H/2}^{H/2} W(z\sigma_0 - \frac{\sigma_1 z^2}{(H/2)}) dz$$

$$= W \left(\frac{1}{2} \sigma_0 z^2 - \frac{2\sigma_1 z^3}{3H} \right) \Big|_{-H/2}^{H/2}$$

$$= W \left(\frac{1}{2} \sigma_0 \frac{H^2}{4} - \frac{2}{3} \sigma_1 \frac{H^2}{8} - \frac{1}{2} \sigma_0 \frac{H^2}{4} + \frac{2}{3} \sigma_1 \frac{H^2}{8} \right)$$

$M_x = -\frac{1}{6} \sigma_1 W H^2$

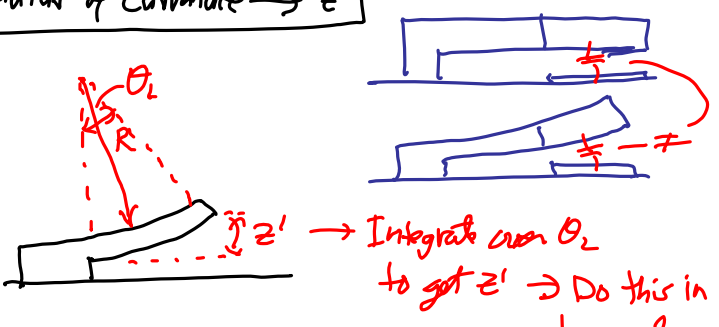
Thus, the radius of curvature:

$$\frac{1}{R} = -\frac{M_x}{E'I} \rightarrow R = \frac{E'I}{M_x} = \frac{1}{2} \frac{E'H}{\sigma_1}$$

\uparrow Biecial Modulus
 \uparrow $[I = \frac{1}{12} W H^3]$

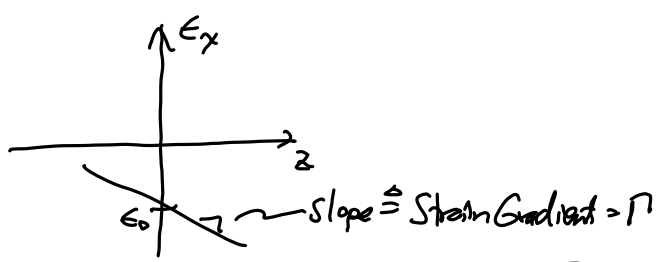
$R = \frac{1}{2} \frac{E}{(1-\nu)} \frac{H}{\sigma_1}$ } Radius of Curvature for a Cantilever w/ a Shear Gradient

Radius of Curvature $\rightarrow z'$



\rightarrow Integrate over θ_2 to get z' \rightarrow Do this in homework

Definition. Strain Gradient



Slope $\hat{=}$ Strain Gradient $= 1/R$

$$R = \frac{1}{2} \frac{E}{(1-\nu)} \frac{H}{\sigma_1} = \frac{1}{2} \frac{E'}{\sigma_1} = \frac{(H/2)}{\epsilon_1} = \frac{1}{1/R} \rightarrow \boxed{R = \frac{1}{R}} \checkmark$$

Series Combination of Springs

Just like a free boundary condition

Whos's this force? F

Series: $y_{tot} = y_1 + y_2$ } To tell if springs are in series: $y_{tot} > y_1$ ✓
 $y_{tot} > y_2$ ✓

$y_{tot} = y(L) = 2y(L_c) = 2\left(\frac{F}{k_c}\right) = F\left(\frac{1}{k_c} + \frac{1}{k_c}\right) = \frac{F}{k}$

↑ stiffness of a cantilever

$\therefore \frac{1}{k} = \frac{1}{k_c} + \frac{1}{k_c} \rightarrow k = k_c || k_c$ stiffness of whole thing

Definition for "||" $A || B = \frac{1}{\frac{1}{A} + \frac{1}{B}} = \frac{AB}{A+B}$

Parallel Combination of Springs

Parallel: $y_{tot} = y_a = y_b$

Same displacement of each constituent spring as to total displacement

$y(L) = y_{tot} = \frac{F}{k} = \frac{F_a}{k_a} = \frac{F_b}{k_b} = \left(\frac{F}{2}\right)\left(\frac{1}{F_a}\right)$

↑ of the whole thing

$\therefore k = 2k_a$

In general: $k_{tot} = k_a + k_b$

For EE's: springs combine like capacitors

