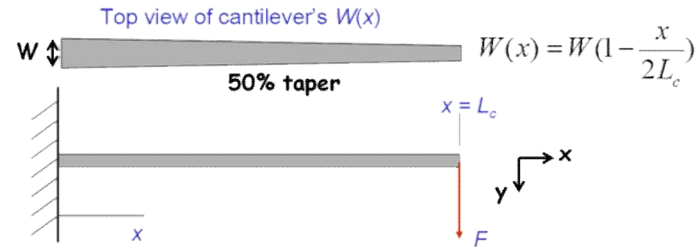


**Lecture 17: Resonance Frequency**

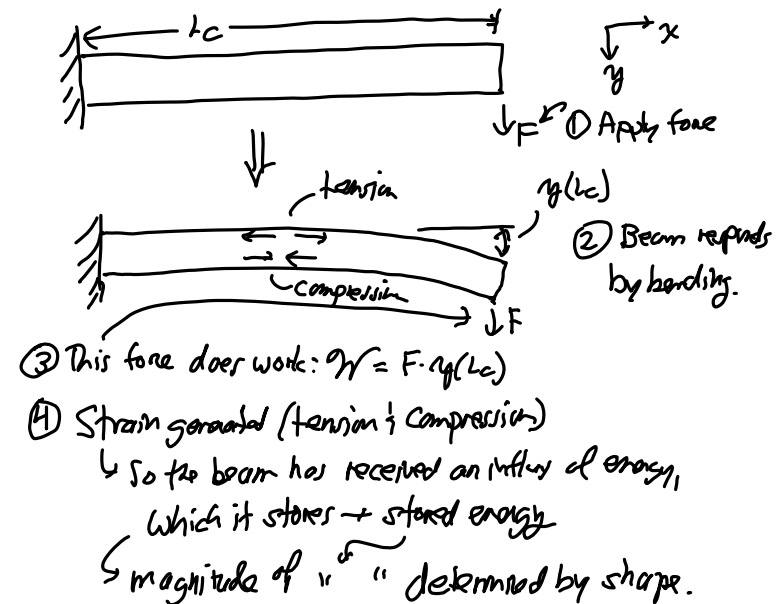
- **Announcements:**
- Module 9 on Energy Methods online
- Module 10 on Resonance Frequency online soon
- Midterm Exam, Thursday, March 17, 5:10-7 p.m. in 3107 Etcheverry
- Passed out old midterm solutions and went through midterm info sheet last time - the info sheet is in the Quizzes/Midterm/Final link
- Graded homework in tray outside my office
- 
- Reading: Senturia, Chpt. 10
- Lecture Topics:
  - ↳ Energy Methods
  - ↳ Virtual Work
  - ↳ Energy Formulations
  - ↳ Tapered Beam Example
  - ↳ Estimating Resonance Frequency
- 
- Reading: Senturia, Chpt. 10: §10.5, Chpt. 19
- Lecture Topics:
  - ↳ Estimating Resonance Frequency
  - ↳ Lumped Mass-Spring Approximation
  - ↳ ADXL-50 Resonance Frequency
  - ↳ Distributed Mass & Stiffness
  - ↳ Folded-Beam Resonator
  - ↳ Resonance Frequency Via Differential Equations
- 
- **Last Time:**
- Started energy-based solutions to bending problems

**More General Geometries**

- Euler-Bernoulli beam theory works well for simple geometries
- But how can we handle more complicated ones?
- **Example:** tapered cantilever beam
- **Objective:** Find an expression for displacement as a function of location  $x$  under a point load  $F$  applied at the tip of the free end of a cantilever with tapered width  $W(x)$



Same problem as before: Take a beam, apply force.



⑤ Then:

$U = \text{Stored Energy} - \text{Work Done} \rightarrow 0$

when we choose the right shape  
This is how we get the beam's response to F.

transfer fn  
 $y(x) = f(x)$

**Fundamentals of Energy Density**

General Definition of Work:

$W(q_1) = \int_0^{q_1} e(q) dq$   $q = \text{displacement}$   
 $e = \text{effort}$

for EC:  $W(Q) = \int_0^Q \frac{Q}{C} dQ$   
 $\uparrow$  charge

**Strain Energy Density** value of strain @ position  $(x, y, z)$

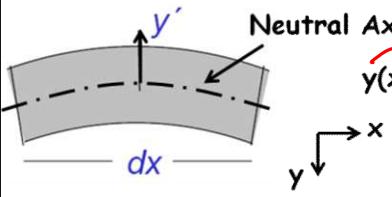
$w = \int_0^{\epsilon_x} \sigma_x d\epsilon_x$   
 $\uparrow$   $\sigma_x(\epsilon_x)$  relates stress to strain @ position  $(x, y, z)$

$\{\sigma_x = E\epsilon_x\}$   
 $w = \int_0^{\epsilon_x} E\epsilon_x d\epsilon_x = \frac{1}{2} E \epsilon_x^2$

Total Strain Energy [J]:

$W = \iiint \left\{ \frac{1}{2} E (\epsilon_x^2 + \epsilon_y^2 + \epsilon_z^2) + \frac{1}{2} G (\gamma_{xy}^2 + \gamma_{xz}^2 + \gamma_{yz}^2) \right\} dV$

**Bending Energy Density**



Neutral Axis *same as z before*  
 $y(x) = \text{transverse displacement of neutral axis}$

First, find the bending energy  $dW_{\text{bend}}$  in an infinitesimal length  $dx$ :

$dW_{\text{bend}} = W dx \int_{-\frac{h}{2}}^{\frac{h}{2}} \frac{1}{2} E \epsilon_x^2(y') dy'$   
width  
"fn of"

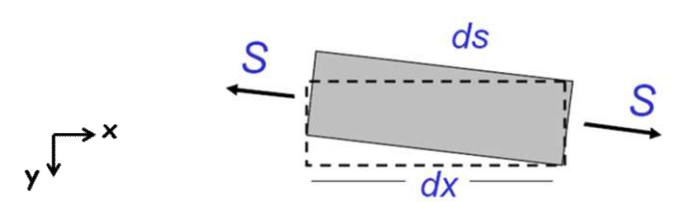
$\left[ \frac{1}{R} = \frac{d^2 y}{dx^2}, \epsilon_x = \frac{y'}{R} \right] \rightarrow \epsilon_x(y') = y' \frac{d^2 y}{dx^2}$

$dW_{\text{bend}} = W dx \int_{-\frac{h}{2}}^{\frac{h}{2}} \frac{1}{2} E \left[ y' \frac{d^2 y}{dx^2} \right]^2 dy'$

$= \frac{E}{2} \left( \frac{Wh^3}{12} \right) \left( \frac{d^2 y}{dx^2} \right)^2 dx$   
 $\underbrace{\hspace{2cm}}_{I_2}$

$\therefore W_{\text{bend}} = \frac{1}{2} E I_2 \int_0^L \left( \frac{d^2 y}{dx^2} \right)^2 dx$

**Energy Due to Axial Load**



$\Rightarrow$  Energy related to lengthening

$$ds = [(dx)^2 + (dy)^2]^{1/2} = dx \left[ 1 + \left( \frac{dy}{dx} \right)^2 \right]^{1/2}$$

bincomial theorem  $\rightarrow \approx dx \left[ 1 + \frac{1}{2} \left( \frac{dy}{dx} \right)^2 \right]$

$$\therefore \epsilon_x = \frac{ds - dx}{dx} = \frac{1}{2} \left( \frac{dy}{dx} \right)^2$$

$$dW_{axial} = S \epsilon_x dx = \frac{1}{2} S \left( \frac{dy}{dx} \right)^2 dx$$


$$W_{axial} = \frac{1}{2} S \int_0^L \left( \frac{dy}{dx} \right)^2 dx$$

Axial Strain Energy

$\Rightarrow$  Look @ shear strain energy in your module.

- Go to Module 9, pg. 10, and look at shear strain energy
- Then, finish off Module 9

**Estimating Resonance Frequency**



$x(t) = X_0 \cos \omega t$

**Potential Energy**

$$W(t) = \frac{1}{2} k x^2(t) = \frac{1}{2} k X_0^2 \cos^2 \omega t$$

**Kinetic Energy**

$$K(t) = \frac{1}{2} M \dot{x}^2(t) = \frac{1}{2} M X_0^2 \omega^2 \sin^2 \omega t$$

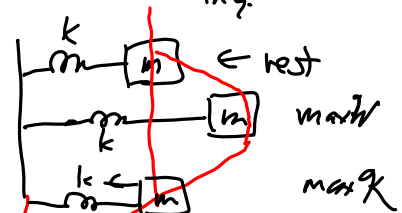
$\dot{x} = \frac{dx}{dt} = \text{velocity}$

**Remarks.**

- Energy must be conserved.
- Total Energy = Potential Energy + Kinetic Energy at all times & location on the structure

$$W_{max} = \frac{1}{2} k X_0^2 = K_{max} = \frac{1}{2} M \omega^2 X_0^2$$

↑ maximum potential energy      ↑ peak displacement      ↑ radian freq.

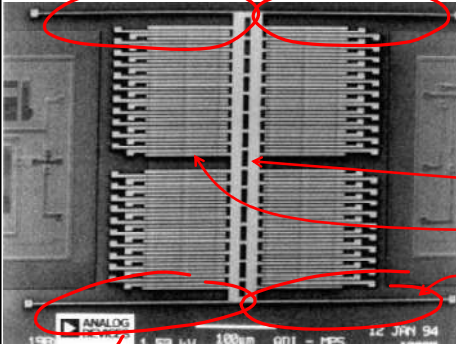
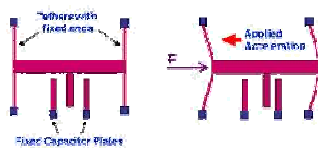


rest       $X_0$        $X_0/2$        $X_0/4$

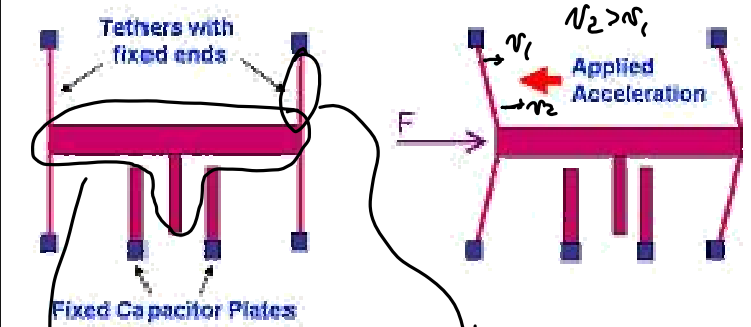
$\omega_0 = \sqrt{\frac{K}{M}}$ 
 ⇒ good for problems where mass & stiffness can be separated; i.e., where they are distinct.

**Good Example: ADXL50 Accelerometer**

- The proof mass of the ADXL-50 is many times larger than the effective mass of its suspension beams
  - Can ignore the mass of the suspension beams (which greatly simplifies the analysis)
- Suspension Beam:  $L = 260 \mu\text{m}$ ,  $h = 2.3 \mu\text{m}$ ,  $W = 2 \mu\text{m}$

In fabrication: purposely introduce a tensile stress in the beams!  
 a fairly large one → okay, for an air bag accelerometer



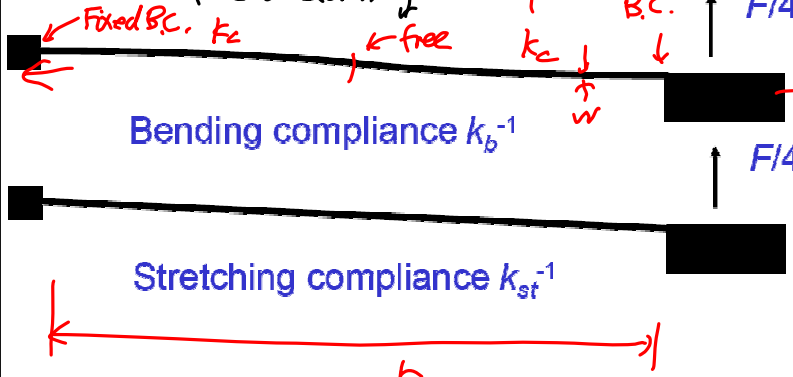
$N_2 > N_1$   
 Applied Acceleration

Mass of <sup>proof m</sup>structure  $\gg$  mass of springs  
 ∴ ignore the mass of the springs

Stiffness of <sup>proof m</sup>structure  $\gg$  stiff of springs  
 ∴ ignore the stiffness of the ~~structure~~ <sup>proof m</sup>

For the ADXL-50:  $M = 162 \text{ ng}$   
 (60% of the mass from fingers)

Suspension: Four tensioned beams  
 ⇒ for each beam:




Bending compliance  $k_b^{-1}$   
 Stretching compliance  $k_{st}^{-1}$

Bending Contribution

$$k_b^{-1} = \left(\frac{1}{k_c} + \frac{1}{k_e}\right) = 2 \left(\frac{(L/2)^3}{3 E (hw^3/12)}\right) = \frac{L^3}{Ehw^3}$$

↑ thickness  
↑ width

Stretching Contribution



$$F_y = s \sin \theta \approx s \theta = s \left(\frac{h}{L}\right) = \left(\frac{s}{L}\right) h$$

[assume small displacements]  $k_{st}$

$$k_{st}^{-1} = \frac{L}{s} = \frac{L}{\sigma_r w h} = 1.14 \text{ m/N}$$

stretching stiffness

To get the total spring constant  
↳ add the bending & stretching stiffnesses

$$k = 4(k_b + k_{st}) = 4(0.24 + 0.88) = 4.5 \text{ N/m}$$

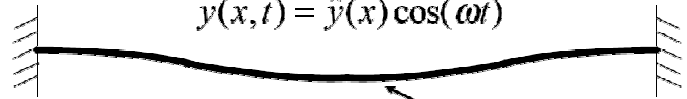
Now, get resonance freq.:

$$f_0 = \frac{1}{2\pi} \sqrt{\frac{K}{M}} = \frac{1}{2\pi} \sqrt{\frac{4.48 \text{ N/m}}{162 \times 10^{-9} \text{ kg}}} = 26.5 \text{ kHz}$$


ADXL-50 Data Sheet:  $f_0 = 24 \text{ kHz}$  ← difference?

↳ Capacitive transducer  
↳ electrical stiffness!

Find the Resonance Frequency When Mass & Stiffness are Distributed

- Vibrating structure displacement function:
 
$$y(x, t) = \hat{y}(x) \cos(\omega t)$$


Maximum displacement function (i.e., mode shape function)  $\hat{y}(x)$   
Seen when velocity  $\dot{y}(x, t) = 0$
- Procedure for determining resonance frequency:
  - Use the static displacement of the structure as a trial function and find the strain energy  $W_{max}$  at the point of maximum displacement (e.g., when  $t=0, \pi/\omega, \dots$ )
  - Determine the maximum kinetic energy when the beam is at zero displacement (e.g., when it experiences its maximum velocity)
  - Equate energies and solve for frequency



$y(x, t) = 0$

Velocity topographical mapping