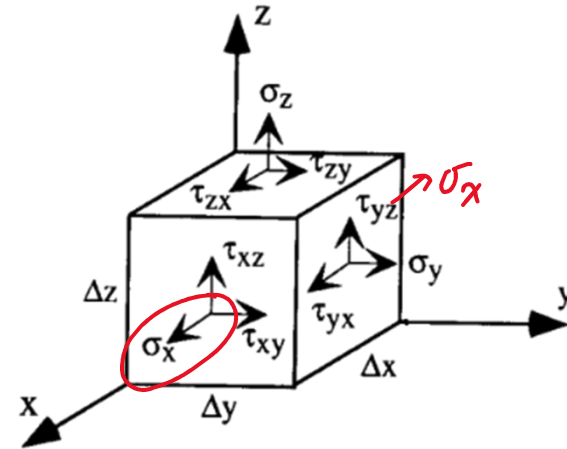


Lecture 11: Mechanics of Materials I

- Announcements:
- Module 7 on "Mechanics of Materials" online
- HW#3 due Tuesday, 3/5, at 9 a.m.
- Note: The hdmi projector interface was broken
  - ↳ Had to spend time setting up the VGA interface
  - ↳ Lost about 15 minutes, which we'll make up in a video lecture the next time I travel
- 
- Reading: Senturia, Chpt. 8
- Lecture Topics:
  - ↳ Stress, strain, etc., for isotropic materials
  - ↳ Thin films: thermal stress, residual stress, and stress gradients
  - ↳ Internal dissipation
  - ↳ MEMS material properties and performance metrics
- 
- Last Time:
- Started Module 7 on "Mechanics of Materials"
- Now, continue with this ...

Example. Exercice de "terms"

⇒ determine the volume change  $\Delta V$  for a uniaxial stress (along the x-direction)



Upon application of  $\sigma_x$ , what is the volume change  $\Delta V$ ?

Before  $\sigma_x$  → After  $\sigma_x$

$$\left. \begin{array}{l} \Delta x \rightarrow \Delta x(1 + \epsilon_x) \\ \Delta y \rightarrow \Delta y(1 - \nu \epsilon_x) \\ \Delta z \rightarrow \Delta z(1 - \nu \epsilon_x) \end{array} \right\} \begin{array}{l} \text{assuming} \\ \text{isotropic} \\ \text{material} \\ \downarrow \\ \text{same } \nu \text{ along } x \text{ \& } y \end{array}$$

The resulting volume change:

$$\Delta V = \underbrace{\Delta x \Delta y \Delta z (1 + \epsilon_x)(1 - \nu \epsilon_x)^2}_{\text{volume after applying } \sigma_x} - \Delta x \Delta y \Delta z$$

$$= \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - \nu \epsilon_x)^2 - 1]$$

[Assume small strains]  $\Rightarrow (1 + \epsilon_x)^n \approx 1 + n\epsilon_x$   
Binomial Theorem

$$\Delta V = \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - 2\nu \epsilon_x) - 1]$$

$$\Delta V = \Delta x \Delta y \Delta z (1 - 2\nu) \epsilon_x$$

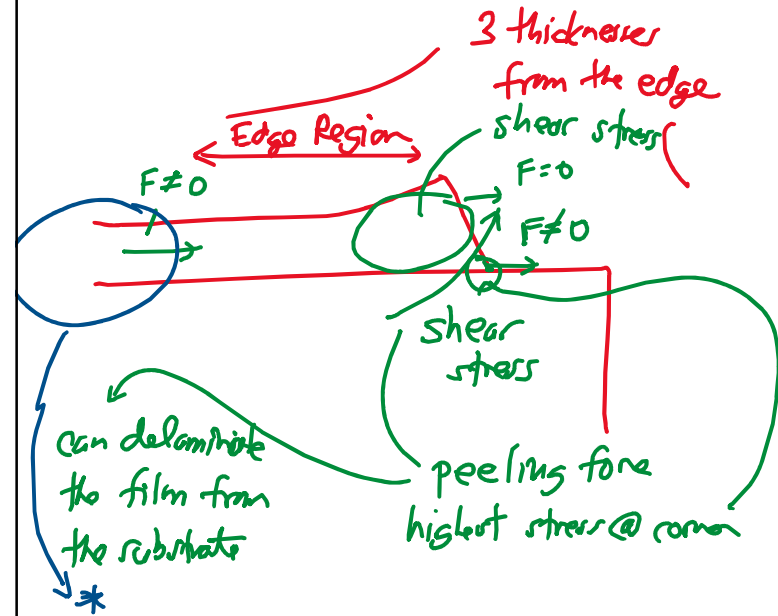
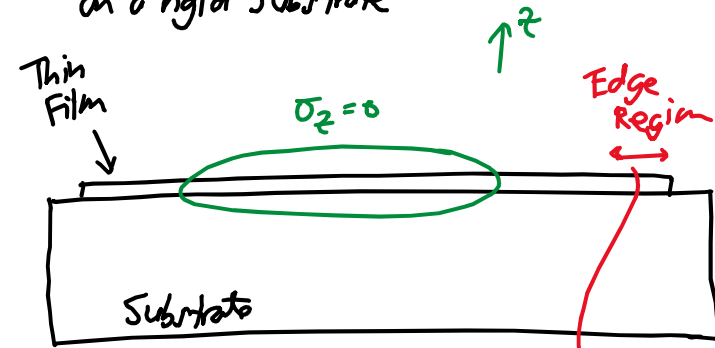
For  $\nu = 0.5$  (rubber)  $\rightarrow \Delta V = 0$ , no volume change! ✓

$\nu < 0.5 \rightarrow$  finite  $\Delta V$

for isotropic materials  $\rightarrow$  Module 7 (last 2 slides)

**Important Case: Plane Stress**

$\Rightarrow$  common case for a thin-film coating on a rigid substrate



\*  
 ↓ Take a closer look @ this region:  $\sigma_z = 0$   
 Get two components of stress (& strain)  

$$\epsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + 0)]$$

$$\epsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_x - 0)]$$
 Assume: plane stress  $\rightarrow$  isotropic:  $\sigma_x = \sigma_y = \sigma$   
 (symmetry in the xy-plane) ↓  

$$\epsilon_x = \epsilon_y = \epsilon$$

$$\epsilon_x = \frac{1}{E} [\sigma - \nu\sigma]$$

$$= \frac{\sigma}{\left(\frac{E}{1-\nu}\right)} \Rightarrow \epsilon_x = \frac{\sigma}{E'}$$
 where  $E' \triangleq$  Biaxial Modulus  $= \frac{E}{1-\nu}$

Linear Thermal Expansion

temperature  $\uparrow \rightarrow$  solids expand in volume

Definition: linear thermal expansion coefficient

Linear Thermal Exp. Coefficient  $\triangleq \alpha_T = \frac{d\epsilon_x}{dT}$  [Kelvin<sup>-1</sup>]

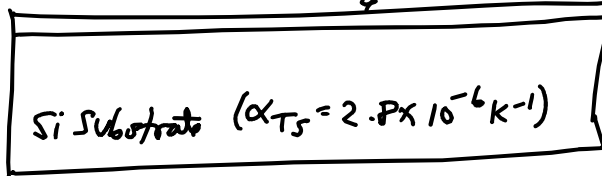
Remarks:

- ①  $\alpha_T$  values tend to be in the  $10^{-6}$  to  $10^{-7}$  range
- ②  $10^{-6} \text{K}^{-1} = 1 \mu\text{strain/K}$
- ③ In 3D, get a volume thermal exp. Coefficient:  

$$\frac{\Delta V}{V} = \frac{3\alpha_T \Delta T}{\uparrow}$$
- ④ For moderate  $\Delta T$ 's  $\rightarrow \alpha_T \approx$  constant  
 ↓ for larger  $\Delta T$ , then  $\alpha_T = f(T)$   
 ↓  
 See Module 7 slide 18

Ex. Thin-Film Thermal Stress

Thin-film ( $\alpha_{Tf}$ )



Assume.

- ① Substrate is much thicker than the film.
- ② The film deposits stress-free @  $T_d$   
↑  
deposition  
temperature
- ③ Then, the whole thing cools to room temperature,  $T_r$ .

Thermal strain of the substrate:  
(in one plane dimension)

$$\epsilon_s = -\alpha_{T_s} \Delta T, \text{ where } \Delta T = T_d - T_r$$

If the film were not attached to substrate

$$\epsilon_{f, \text{free}} = -\alpha_{Tf} \Delta T$$

But the film is attached to the substrate

↳ thickness of substrate  $\gg$  film thickness

∴ substrate wins!

Therefore, the actual strain experienced by the film is that of the substrate:

$$\epsilon_{f, \text{attached}} = -\alpha_{T_s} \Delta T$$

Thus:

$$\left. \begin{array}{l} \text{Thermal} \\ \text{Mismatch} \\ \text{Strain} \end{array} \right\} = \epsilon_{f, \text{mismatch}} = (\alpha_{Tf} - \alpha_{T_s}) \Delta T$$

↳ Note this is biaxial strain (assuming the film deposits isotropically on the substrate)

$$\sigma_{f, \text{mismatch}} = \underbrace{\left( \frac{E}{1-\nu} \right)}_{E'} \epsilon_{f, \text{mismatch}}$$

Ex. Thin-film is polyimide

$$\alpha_{Tf} = 70 \times 10^{-6} \text{ K}^{-1}$$

$$E = 4 \text{ GPa}$$

deposited @ 250°C, then cooled to RT = 25°C

$$\Delta T = 225 \text{ K}$$

$$\epsilon_{f, \text{mismatch}} = (70 - 2.8) \mu (225) = 1.5 \times 10^{-2}$$

$$[\mu = 10^{-6}, m = 10^{-3}, k = 10^3, G = 10^9]$$

$$\sigma_{f, \text{mismatch}} = (4 \text{ G})(1.5 \times 10^{-2}) = 60.5 \text{ MPa}$$

stress is (+) → tensile

[if (-), then compressive]