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Dry Etching

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Dry Etching

- Physical sputtering
- Plasma etching
- Reactive ion etching

All based upon plasma processes.

RF (also, could be μ wave)

Develop (-) bias

Plasma (partially ionized gas composed of ions, e-'s, and highly reactive neutral species)

E-field

wafer

Develops (+) charge to compensate for -

\therefore (+) ions will be accelerated to the wafer

(+) ions generated by inelastic collisions with energetic e-'s
 Get avalanche effect because more e-'s come out as each ion is generated.

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Physical Sputtering (Ion Milling)

- Bombard substrate w/ energetic ions \rightarrow etching via physical momentum transfer
- Give ions energy and directionality using E-fields
- Highly directional \rightarrow very anisotropic

ions

plasma

PR

PR

film

Si

Steep vertical wall

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Problems With Ion Milling

PR etched down to here

PR

PR

PR

film

Si

grass

Once through the film, the etch will start barreling through the Si

- PR or other masking material etched at almost the same rate as the film to be etched \rightarrow very poor selectivity!
- Ejected species not inherently volatile \rightarrow get redeposition \rightarrow non-uniform etch \rightarrow grass!

- Because of these problems, ion milling is not used often (very rare)

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Plasma Etching

- Plasma (gas glow discharge) creates reactive species that chemically react w/ the film in question
- Result:** much better selectivity, but get an isotropic etch

Plasma Etching Mechanism:

- Reactive species generated in a plasma.
- Reactive species diffuse to the surface of material to be etched.
- Species adsorbed on the surface.
- Chemical reaction.
- By-product desorbed from surface.
- Desorbed species diffuse into the bulk of the gas

MOST IMPORTANT STEP! (determines whether plasma etching is possible or not.)

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Ex: Polysilicon Etching w/ CF₄ and O₂

$$CF_4 \xrightarrow{\text{plasma}} CF_4^+ + CF_3^+ + CF_2^+ + CF^+ + F^+ + F^0 + CF_2^+ + \dots$$

Neutral radical (highly reactive!)

$$e^- + CF_4 \rightarrow CF_3 + F + e^-$$

SiCF₆, SiF₄ ← both volatile ∴ dry etching is possible.

- F⁰ is the dominant reactant → but it can't be given a direction → thus, get isotropic etch!

isotropic component → F⁰ → PR → polySi → SiF₄

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Ex: Polysilicon Etching w/ CF₄ and O₂

Problems:

- Isotropic etching
- Formation of polymer because of C in CF₄
 - ↳ **Solution:** add O₂ to remove the polymer (but note that this reduces the selectivity, S_{poly/PR})

Solution:

- ↳ Use Reactive Ion Etching (RIE)

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Reactive Ion Etching (RIE)

- Use ion bombardment to aid and enhance reactive etching in a particular direction
 - ↳ **Result:** directional, anisotropic etching!
- RIE is somewhat of a misnomer
 - ↳ It's not ions that react ... rather, it's still the neutral species that dominate reaction
 - ↳ Ions just enhance reaction of these neutral radicals in a specific direction
- Two principle postulated mechanisms behind RIE
 - Surface damage mechanism
 - Surface inhibitor mechanism

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RIE: Surface Damage Mechanism

- Relatively high energy impinging ions (>50 eV) produce lattice damage at surface
- Reaction at these damaged sites is enhanced compared to reactions at undamaged areas

Handwritten note: Rely on damage to specify a preferred etch direction (downwards)

Result: E.R. at surface >> E.R. on sidewalls

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RIE: Surface Inhibitor Mechanism

- Non-volatile polymer layers are a product of reaction
- They are removed by high energy directional ions on the horizontal surface, but not removed from sidewalls

Handwritten notes: (+) ions breakup the polymer layer, get reaction

Result: E.R. @ surface >> E.R. on sidewalls

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Deep Reactive-Ion Etching (DRIE)

The Bosch process:

- Inductively-coupled plasma
- Etch Rate: 1.5-4 $\mu\text{m}/\text{min}$
- Two main cycles in the etch:
 - Etch cycle (5-15 s): SF_6 (SF_x^+) etches Si
 - Deposition cycle: (5-15 s): C_4F_8 deposits fluorocarbon protective polymer (CF_2^-)_n
- Etch mask selectivity:
 - $\text{SiO}_2 \sim 200:1$
 - Photoresist $\sim 100:1$
- Issue:** finite sidewall roughness
 - scalloping < 50 nm
- Sidewall angle: $90^\circ \pm 2^\circ$

Handwritten notes: scallops, Maluf

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DRIE Issues: Etch Rate Variance

- Etch rate is diffusion-limited and drops for narrow trenches
 - Adjust mask layout to eliminate large disparities
 - Adjust process parameters (slow down the etch rate to that governed by the slowest feature)

Etch rate decreases with trench width

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Semiconductor Doping

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Doping of Semiconductors

- Semiconductors are not intrinsically conductive
- To make them conductive, replace silicon atoms in the lattice with dopant atoms that have valence bands with fewer or more e⁻s than the 4 of Si
- If more e⁻s, then the dopant is a donor: P, As
 - ↳ The extra e⁻ is effectively released from the bonded atoms to join a cloud of free e⁻s, free to move like e⁻s in a metal

- ↳ The larger the # of donor atoms, the larger the # of free e⁻s → the higher the conductivity

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Doping of Semiconductors (cont.)

- **Conductivity Equation:**

$$\sigma = q\mu_n n + q\mu_p p$$

conductivity ← σ ← charge magnitude on an electron
 electron mobility ← μ_n ← electron density ← n ← hole density
 hole mobility ← μ_p ← hole density ← p

- If fewer e⁻s, then the dopant is an acceptor: B

- ↳ Lack of an e⁻ = hole = h⁺
- ↳ When e⁻s move into h⁺s, the h⁺s effectively move in the opposite direction → a h⁺ is a mobile (+) charge carrier

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General Comments on Predeposition

- Higher doses only: $Q = 10^{13} - 10^{16} \text{ cm}^{-2}$ (I/I is $10^{11} - 10^{16}$)
- Dose not well controlled: $\pm 20\%$ (I/I can get $\pm 1\%$)
- Uniformity is not good
 - ↳ $\pm 10\%$ w/ gas source
 - ↳ $\pm 2\%$ w/ solid source
- Max. conc. possible limited by solid solubility
 - ↳ Limited to $\sim 10^{20} \text{ cm}^{-3}$
 - ↳ No limit for I/I → you force it in here!
- For these reasons, I/I is usually the preferred method for introduction of dopants in transistor devices
- But I/I is not necessarily the best choice for MEMS
 - ↳ I/I cannot dope the underside of a suspended beam
 - ↳ I/I yields one-sided doping → introduces unbalanced stress → warping of structures
 - ↳ I/I can do physical damage → problem if annealing is not permitted
- Thus, predeposition is often preferred when doping MEMS

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Diffusion Modeling

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Modeling $N(x)$ $\rightarrow J$

\Rightarrow Dopants from points of high conc. move to points of low conc. w/ flux J
 \Rightarrow Question: What's $N(x,t)$?
 ? fn of time

Fick's Law of Diffusion - (1st law)
 $J(x,t) = -D \frac{\partial N(x,t)}{\partial x}$ (1)
 Flux [$\#/cm^2 \cdot s$] \leftarrow Diffusion Coefficient

Continuity Equation for Particle Flux -
 General Form: $\frac{\partial N(x,t)}{\partial t} = -\nabla \cdot \vec{J}$
 rate of increase of conc. w/ time \leftarrow negative of the divergence of particle flux

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Diffusion Modeling (cont.)

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\Rightarrow We're interested for now in the one-dimensional form:

$$\frac{\partial N(x,t)}{\partial t} = -\frac{\partial J}{\partial x}$$
 (2)

$\left[\frac{\partial}{\partial x} (1) \text{ and substitute (2) in (1)} \Rightarrow \frac{\partial N(x,t)}{\partial t} = D \frac{\partial^2 N(x,t)}{\partial x^2} \right]$ [Fick's 2nd Law of Diffusion in 1-D]

Solutions: \rightarrow dependent upon boundary conditions
 \rightarrow use variable separation or Laplace Xform techniques

Case 1: Predeposition \rightarrow constant source diffusion: surface concentration stays the same during the diffusion $t_1 < t_2 < t_3$

surface conc. stays constant $\rightarrow N_0$ \leftarrow impurity conc
 background conc. $\rightarrow N_B$
 x , distance ff. surface

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Diffusion Modeling (Predeposition)

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\Rightarrow if plotted on a linear scale, would look like this:

Boundary Conditions:
 (i) $N(0,t) = N_0$
 (ii) $N(\infty,t) = 0$
 $\left. \begin{array}{l} \text{(i)} \\ \text{(ii)} \end{array} \right\} N(x,t) = N_0 \left[1 - \frac{1}{\sqrt{\pi}} \int_0^{\frac{x}{\sqrt{Dt}}} e^{-y^2} dy \right]$

$N(x,t) = N_0 \operatorname{erfc} \left(\frac{x}{\sqrt{Dt}} \right)$ \Rightarrow again, complementary error function (read tables or graph)

Done, $Q \cong$ total # of impurity atoms per unit area in the Si
 = area under the curve

$$Q = \int_0^{\infty} N(x,t) dx \Rightarrow Q(t) = N_0 \frac{2\sqrt{Dt}}{\sqrt{\pi}} \text{ cm}^{-2}$$

$2\sqrt{Dt} \cong$ characteristic diffusion length

$N(x,t)$ \leftarrow linear scale
 area under this square is same as under the curve!
 $2\sqrt{Dt}/\sqrt{\pi}$

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