

Avoiding Stiction

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- Reduce droplet area via mechanical design approaches
Beam: cantilever → clamp-stroke → raises stiffness: First: $k \propto$

 Standoff Bumps Meniscus-Shaping Features
- Avoid liquid-vapor meniscus formation
 - Use solvents that sublime
 - Use vapor-phase sacrificial layer etch
- Modify surfaces to change the meniscus shape from concave (small contact angle) to convex (large contact angle)
 - Use teflon-like films
 - Use hydrophobic self-assembled monolayers (SAMs)

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Supercritical CO₂ Drying

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- A method for stictionless drying of released microstructures by immersing them in CO₂ at its supercritical point
- Basic Strategy:** Eliminate surface tension-derived sticking by avoiding a liquid-vapor meniscus
- Procedure:**
 - Etch oxide in solution of HF
 - Rinse thoroughly in DI water, but do not dry
 - Transfer the wafer from water to methanol
 - Displace methanol w/ liquid CO₂
 - Apply heat & pressure to take the CO₂ past its critical pt.
 - Vent to lower pressure and allow the supercritical CO₂ to revert to gas → liquid-to-gas transition in supercritical region means no capillary forces to cause stiction

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Hydrophilic Versus Hydrophobic

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contact angle

- Hydrophilic:**
 - A surface that invites wetting by water
 - Get stiction
 - Occurs when the contact angle $\theta_{\text{water}} < 90^\circ$
- Hydrophobic:**
 - A surface that repels wetting by water
 - Avoids stiction
 - Occurs when the contact angle $\theta_{\text{water}} > 90^\circ$

Lotus Surface [Univ. Mainz]

Hydrophilic case Hydrophobic case

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Tailoring Contact Angle Via SAM's

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- Can reduce stiction by tailoring surfaces so that they induce a water contact angle $> 90^\circ$
- Self-Assembled Monolayers (SAM's):**
 - Monolayers of "stringy" molecules covalently bonded to the surface that then raise the contact angle
- Beneficial characteristics:**
 - Conformal, ultrathin
 - Low surface energy
 - Covalent bonding makes them wear resistant
 - Thermally stable (to a point)

Substrate Substrate

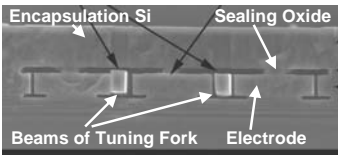
OTS
CH3(CH2)17SiCl3

	θ_{water}
ODT SAM	$112 \pm 0.7^\circ$
SiO ₂	$< 10^\circ$

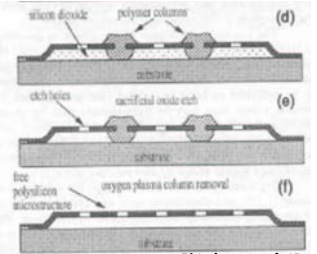
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Dry Release

- Another way to avoid stiction is to use a dry sacrificial layer etch
- For an oxide sacrificial layer
 - use HF vapor phase etching
 - Additional advantage: gas can more easily get into tiny gaps
 - Issue: not always completely dry → moisture can still condense → stiction → soln: add alcohol
- For a polymer sacrificial layer
 - Use an O₂ plasma etch (isotropic, so it can undercut well)
 - Issues:
 - Cannot be used when structural material requires high temperature for deposition
 - If all the polymer is not removed, polymer under the suspended structure can still promote stiction



Released via vapor phase HF
[Kenny, et al., Stanford]



[Kobayashi]

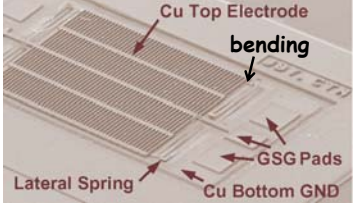
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Residual Stress

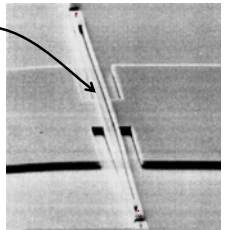
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Residual Stress in Thin Films

- After release, poorly designed microstructures might buckle, bend, or warp → often caused by residual film stress
- Origins of residual stress, σ
 - Growth processes
 - Non-equilibrium deposition
 - Grain morphology change
 - Gas entrapment
 - Doping
 - Thermal stresses
 - Thermal expansion mismatch of materials → introduce stress during cool-down after deposition
 - Annealing



Tunable Dielectric Capacitor
[Yoon, et al., U. Michigan]



Buckled Double-Ended Tuning Fork

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Need to Control Film Stress

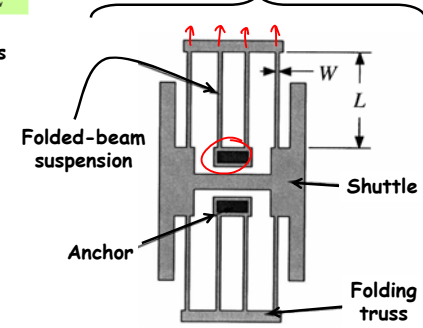
- Resonance frequency expression for a lateral resonator:

$$f_0 \approx \frac{1}{2\pi} \sqrt{\frac{4E_y t W^3}{M L^3} + \frac{24 \sigma_r t W}{5 M L}}$$

\uparrow Basic term \uparrow Stress term

Since $W \ll L$, the stress term will dominate if $\sigma_r \sim E_y$

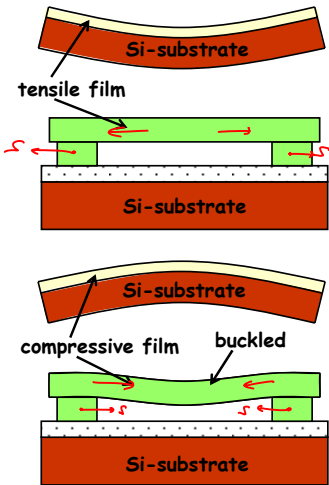
E_y = Young's modulus
 σ_r = stress
 t = thickness
 W = beam width
 L = beam length
 M = mass



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Tensile Versus Compressive Stress

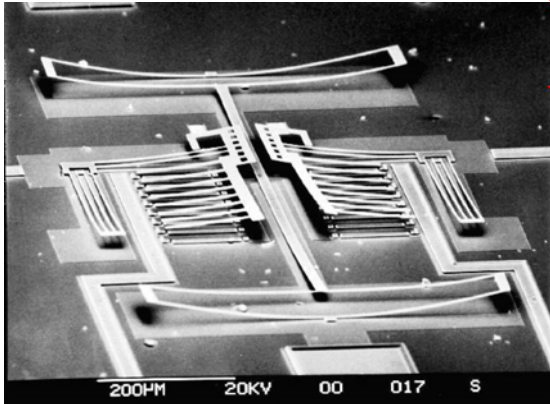
- Under **tensile stress**, a film wants to shrink w/r to its substrate
 - Caused, e.g., by differences in film vs. substrate thermal expansion coefficients
 - If suspended above a substrate and anchored to it at two points, the film will be "stretched" by the substrate
- Under **compressive stress**, a film wants to expand w/r to its substrate
 - If suspended above a substrate and anchored to it at two points, the film will buckle over the substrate



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Vertical Stress Gradients


- Variation of residual stress in the direction of film growth
- Can warp released structures in z-direction



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Stress in Polysilicon Films

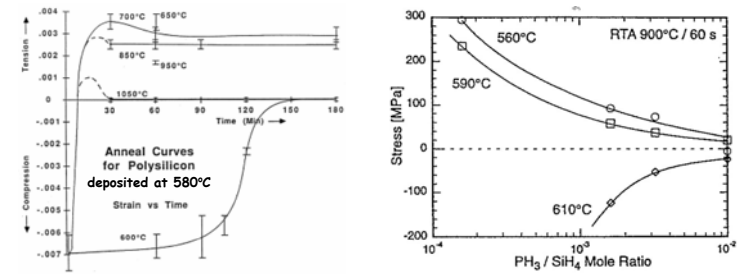
- Stress depends on crystal structure, which in turn depends upon the deposition temperature
- Temperature $\leq 600^\circ\text{C}$
 - Films are initially amorphous, then crystallize
 - Get equiaxed crystals, largely isotropic
 - Crystals have higher density \rightarrow tensile stress
 - Small stress gradient
- Temperature $\geq 600^\circ\text{C}$
 - Columnar crystals grow during deposition
 - As crystals grow vertically and in-plane they push on neighbors \rightarrow compressive stress
 - Positive stress gradient



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Annealing Out Polysilicon Stress

- Control polySi stress by annealing at high temperatures
 - Typical anneal temperatures: $900\text{--}1150^\circ\text{C}$
 - Grain boundaries move, relax
 - Can dope while annealing by sandwiching the polysilicon between similarly doped oxides (symmetric dopant drive-in), e.g. using 10–15 wt. % PSG
- Rapid thermal anneal (RTA) also effective (surprisingly)



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Topography Issues

- Degradation of lithographic resolution
 - ↳ PR step coverage, streaking
- Stringers
 - ↳ Problematic when using anisotropic etching, e.g., RIE

Thickness differences pose problems for reduction steppers

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Nickel Surface-Micromachining Process Flow

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Electroplating: Metal MEMS

- Use electroplating to obtain metal μ structures
- When thick: call it "LIGA"
- Pros: fast low temp deposition, very conductive
- Cons: drift, low mech. Q but may be solvable?

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Nickel Metal Surface-Micromachining

- Deposit isolation LTO:
 - ↳ Target = $2\mu\text{m}$
 - ↳ 1 hr. 40 min. LPCVD @ 450°C
- Densify the LTO
 - ↳ Anneal @ 950°C for 30 min.
- Define metal interconnect via lift-off
 - ↳ Spin photoresist and pattern lithographically to open areas where interconnect will stay
 - ↳ Evaporate a Ti/Au layer
 - Target = 30nm Ti
 - Target = 270nm Au
 - ↳ Remove photoresist in PRS2000 \rightarrow Ti/Au atop the photoresist also removed

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Nickel Metal Surface-Micromachining

- Evaporate Al to serve as a sacrificial layer
↳ Target = $1\mu\text{m}$
- Lithography to define anchor openings
- Wet etch the aluminum to form anchor vias
↳ Use solution of $\text{H}_3\text{PO}_4/\text{HNO}_3/\text{H}_2\text{O}$
- Remove photoresist in PRS2000
- Electroplate nickel to fill the anchor vias
↳ Use solution of nickel sulfamate @ 50°C
↳ Time the electroplating to planarize the surface

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Nickel Metal Surface-Micromachining

- Evaporate a thin film of nickel to serve as a seed layer for subsequent Ni electroplating
↳ Target = 20nm
- Form a photoresist mold for subsequent electroplating
↳ Spin $6\mu\text{m}$ -thick AZ 9260 photoresist
↳ Lithographically pattern the photoresist to delineate areas where nickel structures are to be formed
- Electroplate nickel structural material through the PR mold
↳ Use a solution of nickel sulfamate @ 50°C
↳ Cathode-to-anode current density $\sim 2.5\text{ mA/cm}^2$

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Nickel Metal Surface-Micromachining

- Strip the PR in PRS2000
- Remove the Ni seed layer in Ni wet etchant
- Release the structures
↳ Use a $\text{K}_4\text{Fe}(\text{CN})_6/\text{NaOH}$ etchant that attacks Al while leaving Ni and Au intact
↳ Etch selectivity $> 100:1$ for Al:Ni and Al:Au

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Nickel Surface-Micromachining Example

- Below: Surface-micromachined in nickel using the described process flow

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3D "Pop-up" MEMS

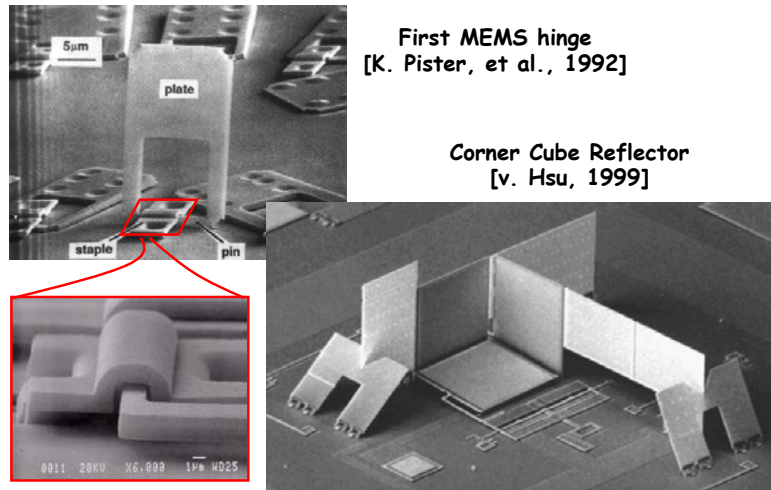
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Pop-Up MEMS

First MEMS hinge
[K. Pister, et al., 1992]

Corner Cube Reflector
[v. Hsu, 1999]

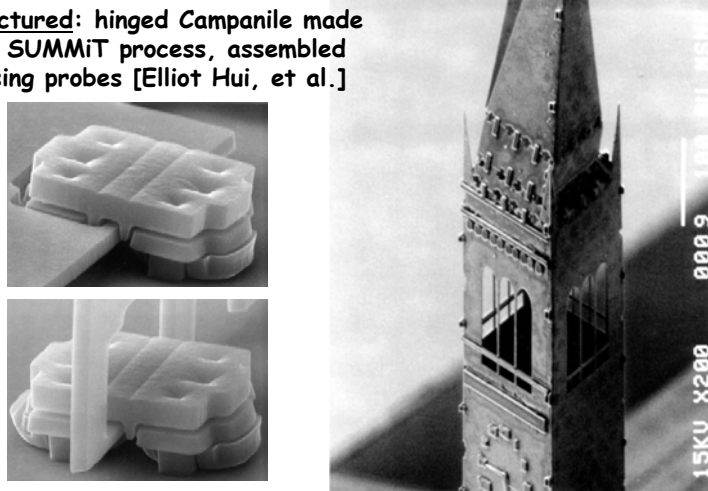


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Pop-Up MEMS

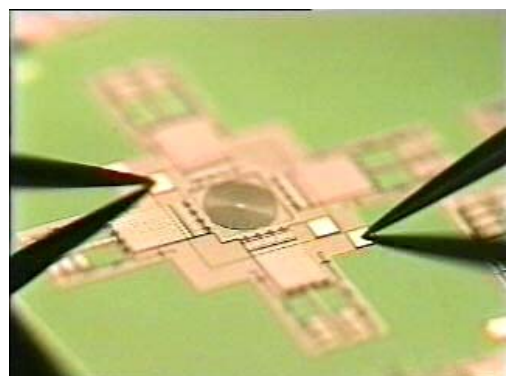
- **Pictured:** hinged Campanile made in SUMMiT process, assembled using probes [Elliot Hui, et al.]



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3D Direct-Assembled Tunable L



[Ming Wu, UCLA]

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