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EE C245 - ME C218 Introduction to MEMS Design Fall 2009

Prof. Clark T.-C. Nguyen

Dept. of Electrical Engineering & Computer Sciences
University of California at Berkeley
Berkeley, CA 94720

Lecture Module 3: Oxidation & Film Deposition

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Lecture Outline

- Reading: Senturia, Chpt. 3; Jaeger, Chpt. 2, 3, 6
 - ↳ Example MEMS fabrication processes
 - ↳ Oxidation
 - ↳ Film Deposition
 - Evaporation
 - Sputter deposition
 - Chemical vapor deposition (CVD)
 - Plasma enhanced chemical vapor deposition (PECVD)
 - Epitaxy
 - Atomic layer deposition (ALD)
 - Electroplating

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MEMS Fabrication

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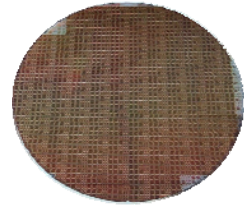
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Making Mechanical Devices

- How best does one make a mechanical product?
- Assembly line production?
 - ↳ Pick and place parts
 - ↳ Used for many macroscopic mechanical products
 - ↳ Robotic automation greatly reduces cost
- **Problem:** difficult to do this with MEMS-scale parts (but not impossible, as we'll soon see ...)
- **Solution:** borrow from integrated circuit (IC) transistor technology
 - ↳ Use monolithic wafer-level fabrication methods
 - ↳ Harness IC's batch methods, where multiple devices are achieved all at once



Automobile Assembly Line



CMOS Integrated Circuit Wafer

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Polysilicon Surface-Micromachining

- Uses IC fabrication instrumentation exclusively
- *Variations*: sacrificial layer thickness, fine- vs. large-grained polysilicon, *in situ* vs. POCL_3 -doping

300 kHz Folded-Beam Micromechanical Resonator

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Electroplating: Metal MEMS

- Use electroplating to obtain metal μ structures
- When thick: call it "LIGA"
- *Pros*: fast low temp deposition, very conductive
- *Cons*: drift, low mech. Q but may be solvable?

RF Switch

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Bulk Micromachining and Bonding

- Use the wafer itself as the structural material
- *Adv*: very large aspect ratios, thick structures
- *Example*: deep etching and wafer bonding

1 mm

[Najafi, Michigan]

Microrotor (for a microengine)

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Oxidation

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Thermal Oxidation of Silicon

- Achieved by heating the silicon wafer to a high temperature (~900°C to 1200°C) in an atmosphere containing pure oxygen or water vapor
- Enabling reactions:

For dry oxygen:

$$\text{Si} + \text{O}_2 \rightarrow \text{SiO}_2$$

For water vapor:

$$\text{Si} + 2\text{H}_2\text{O} \rightarrow \text{SiO}_2 + 2\text{H}_2$$

Schematically:

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Oxidation Modeling

(1) **Initially:** (no oxide @ surface)

↪ Growth rate determined by reaction rate @ the surface

(2) **As oxide builds up:**

Reactant must diffuse to Si surface where the oxidation reaction takes place

↪ Growth rate governed more by rate of diffusion to the silicon-oxide interface

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Oxidation Modeling (cont.)

N_0 = reactant conc. at oxide surface [in cm^{-2}]
 N_i = reactant conc. at Si-SiO₂ interface
 J = reactant flux = $-D \frac{\partial N(x,t)}{\partial x}$ [Fick's 1st Law of Diffusion]
 Diffusion coeff. [in $\mu\text{m/hr}$ or m/s]

In the SiO₂:

$$J = D \frac{(N_o - N_i)}{X_{ox}} = \text{constant} \quad (1)$$

[in # particles/(cm²·s)] Assumption that the reactant does not accumulate in the oxide.

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Oxidation Modeling (cont.)

At the Si-SiO₂ interface:
 Oxidation rate $\propto N_i \therefore J \propto N_i \Rightarrow J = k_s N_i$ (2)

Reaction rate constant @ Si-SiO₂ interface

Combining (1) and (2):

$$\left[N_i = \frac{J}{k_s} \right] \Rightarrow J = D \left(\frac{N_o - J/k_s}{X_{ox}} \right)$$

$$JX_{ox} = DN_o - \frac{DJ}{k_s} \rightarrow J \left(X_{ox} + \frac{D}{k_s} \right) = DN_o$$

$$\therefore J = \frac{DN_o}{X_{ox} + \frac{D}{k_s}} = \text{Flux of reactants}$$

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Oxidation Modeling (cont.)

Find an expression for $X_{OX}(t)$:

Rate of change of oxide layer thickness w/time $\left\} = \frac{dX_{OX}}{dt} = \frac{J}{M} = \frac{DN_O/M}{X_{OX} + D/k_s} \quad (3)$

oxidizing flux J

of molecules of oxidizing species incorporated into a unit volume of oxide $\left\} \begin{aligned} &= 2.2 \times 10^{22} \text{ cm}^{-3} \text{ for } O_2 \\ &= 4.4 \times 10^{22} \text{ cm}^{-3} \text{ for } H_2O \end{aligned} \right.$

Solve (3) for $X_{OX}(t)$: [Initial condition $X_{OX}(t=0) = X_i$]

$$\frac{dX_{OX}}{dt} = \frac{DN_O/M}{X_{OX} + D/k_s} \Rightarrow \int_{X_i}^{X_{OX}} \left(X_{OX} + \frac{D}{k_s} \right) dX_{OX} = \int_0^t \frac{DN_O}{M} dt$$

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Oxide Thickness Versus Time

Result:

additional time required to go from $X_i \rightarrow X_{OX}$ $\left\} \begin{aligned} &= \frac{X_{OX}^2}{B} + \frac{X_i}{(B/A)} \\ &= \tau \end{aligned} \right.$ [X_i = initial oxide thickness]

$$X_{OX}(t) = \frac{A}{2} \left\{ \left[1 + \frac{4B}{A^2} (t + \tau) \right]^{1/2} - 1 \right\}$$

where $A = \frac{2D}{k_s}$ $\tau = \frac{X_i^2}{B} + \frac{X_i}{(B/A)}$

$$B = \frac{2DN_O}{M} \quad D = D_0 \exp\left(-\frac{E_A}{kT}\right)$$

i.e., D governed by an Arrhenius relationship \rightarrow temperature dependent

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Oxidation Modeling (cont.)

For shorter times:

$$\left[(t + \tau) \ll \frac{A^2}{4B} \right] \Rightarrow X_{OX}(t) = \left(\frac{B}{A} \right) (t + \tau) \Rightarrow \text{oxide growth limited by reaction at the Si-SiO}_2 \text{ interface}$$

Taylor expansion (first term after 1's cancel) \rightarrow linear growth rate constant

For long oxidation times: oxide growth diffusion-limited

$$\left[(t + \tau) \gg \frac{A^2}{4B} \right] \Rightarrow X_{OX}(t) = \sqrt{B(t + \tau)} \approx \sqrt{Bt}$$

$t \gg \tau$ Parabolic rate constant

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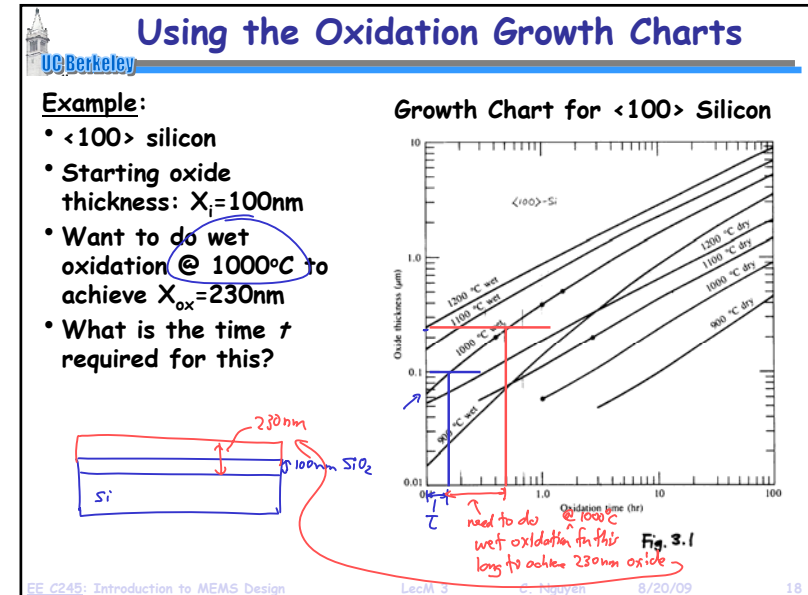
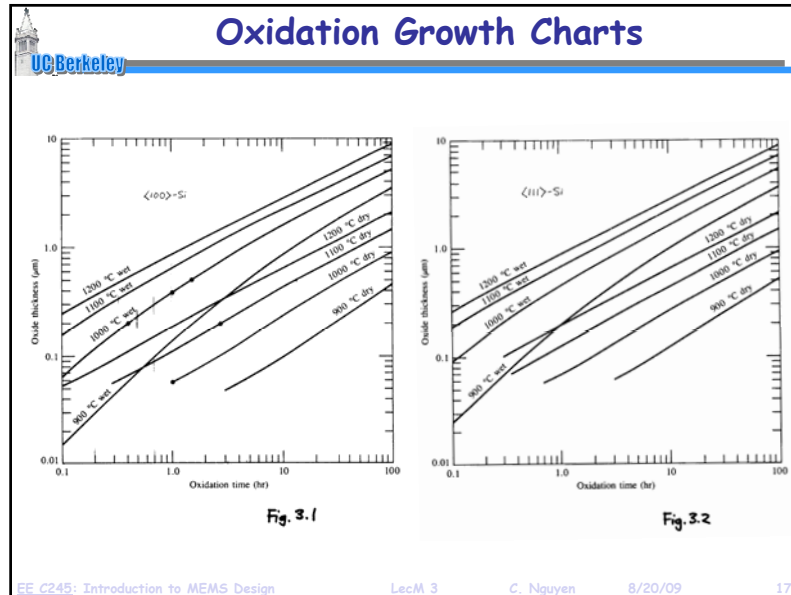
Oxidation Rate Constants

Table 6-2 Rate constants describing (111) silicon oxidation kinetics at 1 Atm total pressure. For the corresponding values for (100) silicon, all C_2 values should be divided by 1.68.

Ambient	B	B/A
Dry O ₂	$C_1 = 7.72 \times 10^2 \mu\text{m}^2 \text{ hr}^{-1}$ $E_1 = 1.23 \text{ eV}$	$C_2 = 6.23 \times 10^6 \mu\text{m hr}^{-1}$ $E_2 = 2.0 \text{ eV}$
Wet O ₂	$C_1 = 2.14 \times 10^2 \mu\text{m}^2 \text{ hr}^{-1}$ $E_1 = 0.71 \text{ eV}$	$C_2 = 8.95 \times 10^7 \mu\text{m hr}^{-1}$ $E_2 = 2.05 \text{ eV}$
H ₂ O	$C_1 = 3.86 \times 10^2 \mu\text{m}^2 \text{ hr}^{-1}$ $E_1 = 0.78 \text{ eV}$	$C_2 = 1.63 \times 10^8 \mu\text{m hr}^{-1}$ $E_2 = 2.05 \text{ eV}$

• Above theory is great ... but usually, the equations are not used in practice, since measured data is available
 ↳ Rather, oxidation growth charts are used

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Factors Affecting Oxidation

- In summary, oxide thickness is dependent upon:
 1. Time of oxidation
 2. Temperature of oxidation
 3. Partial pressure of oxidizing species ($\propto N_a$)
- Also dependent on:
 4. Reactant type:
 - Dry O_2
 - Water vapor \Rightarrow faster oxidation, since water has a higher solubility (i.e., D) in SiO_2 than O_2
 5. Crystal orientation:
 - <111> \leftarrow faster, because there are more bonds available at the Si-surface
 - <100> \leftarrow fewer interface traps; smaller # of unsatisfied Si-bonds at the Si- SiO_2 interface

Factors Affecting Oxidation

6. Impurity doping:
 - P: increases linear rate const.
no effect on parabolic rate constant
faster initial growth \rightarrow surface reaction rate limited
 - B: no effect on linear rate const.
increases parabolic rate const.
faster growth over an initial oxide \rightarrow diffusion faster

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Thin Film Deposition

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Thin Film Deposition

- Methods for film deposition:
 - ✦ Evaporation
 - ✦ Sputter deposition
 - ✦ Chemical vapor deposition (CVD)
 - ✦ Plasma enhanced chemical vapor deposition (PECVD)
 - ✦ Epitaxy
 - ✦ Electroplating
 - ✦ Atomic layer deposition (ALD)

Evaporation:

- Heat a metal (Al, Au) to the point of vaporization
- Evaporate to form a thin film covering the surface of the Si wafer
- Done under vacuum for better control of film composition

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Evaporation

Filament Evaporation System:

1. Pump down to vacuum → reduces film contamination and allows better thickness control
2. Heat W filament → melt Al, wet filament
3. Raise temperature → evaporate Al

mean free path = $\lambda = \frac{kT}{\sqrt{2\pi} Pd^2}$

Vacuum Pump

wafer

W filament

Al staples

k = Boltzmann Constant
T = temperature
P = pressure
d = diameter of gas molecule

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Evaporation (cont.)

- λ can be ~60m for a 4Å particle at 10^{-4} Pa ($-0.75 \mu\text{Torr}$)
 - ✦ thus, at 0.75 μTorr , get straight line path from Al staple filament to wafer

Problem: Shadowing & Step Coverage

Problem: line of sight deposition

Solns:

- i. Rotate wafer during evaporation
- ii. Etch more gradual sidewalls

Better Solution: forget evaporation → sputter deposit the film!

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Sputter Deposition

- Use an energetic plasma to dislodge atoms from a material target, allowing the atoms to settle on the wafer surface

Not as low a vacuum as evaporation (~100 Pa) (750 mTorr)

Vacuum Pump

Target (Al, SiO₂, Si₃N₄, ZnO, Ti, ...)

Ar⁺

plasma

wafer

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Sputter Deposition Process

- Step-by-step procedure:**
 - Pump down to vacuum
 $(\sim 100 \text{ Pa}) \rightarrow 1 \text{ Pa} = 9.8 \times 10^{-6} \text{ atm} \left(\frac{760 \text{ Torr}}{\text{atm}} \right) = 0.0075012 \text{ Torr}$
 \nwarrow 750 mTorr
 - Flow gas (e.g., Ar)
 - Fire up plasma (create Ar⁺ ions) → apply dc-bias (or RF for non-conductive targets)
 - Ar⁺ ions bombard target (dislodge atoms)
 - Atoms make their way to the wafer in a more random fashion, since at this higher pressure, $\lambda \sim 60 \mu\text{m}$ for a 4 Å particle; plus, the target is much bigger
- Result:** better step coverage!

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Problems With Sputtering

- Get some Ar in the film
- Substrate can heat up
 - up to $\sim 350^\circ\text{C}$, causing nonuniformity across the wafer
 - but it still is more uniform than evaporation!
- Stress can be controlled by changing parameters (e.g., flow rate, plasma power) from pass to pass, but repeatability is an issue

• **Solution:** use Chemical Vapor Deposition (CVD)

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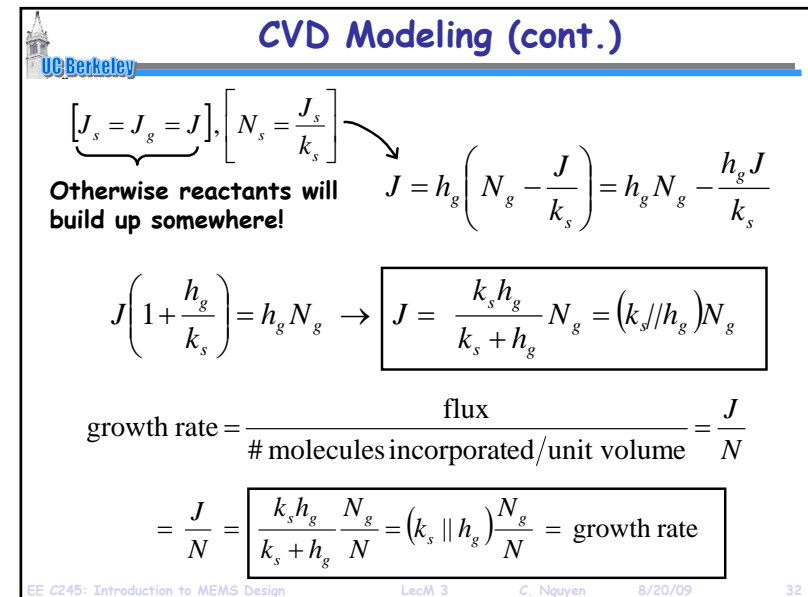
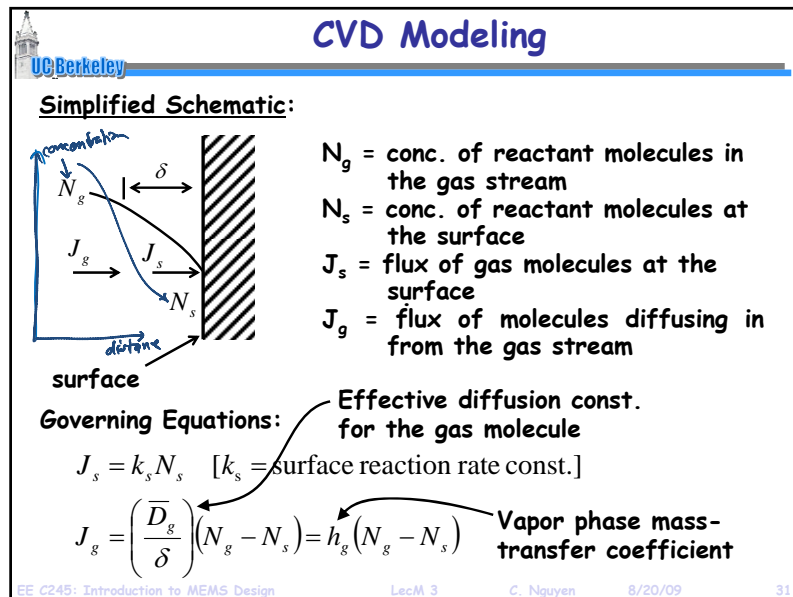
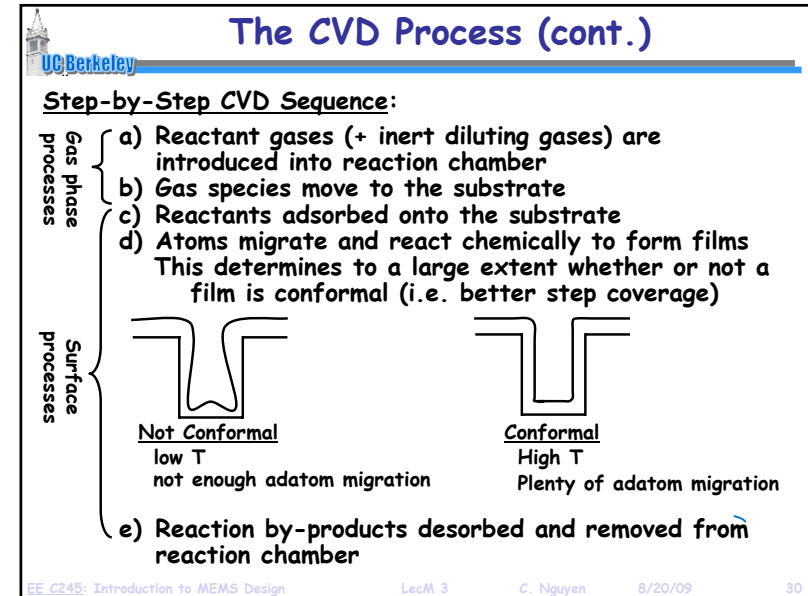
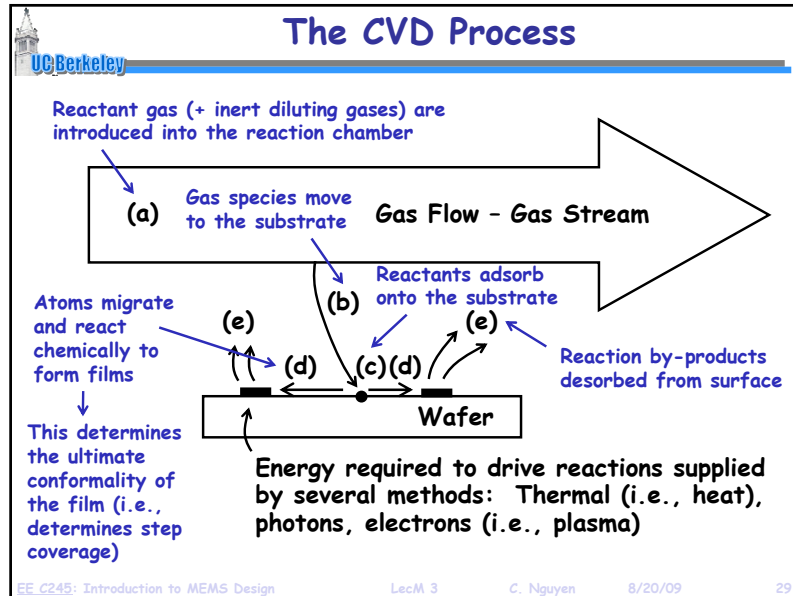
Chemical Vapor Deposition (CVD)

- Even better conformity than sputtering
- Form thin films on the surface of the substrate by thermal decomposition and/or reaction of gaseous compounds
 - Desired material is deposited directly from the gas phase onto the surface of the substrate
 - Can be performed at pressures for which λ (i.e., the mean free path) for gas molecules is small
 - This, combined with relatively high temperature leads to

Excellent Conformal Step Coverage!

- Types of films:** polysilicon, SiO₂, silicon nitride, SiGe, Tungsten (W), Molybdenum (M), Tantalum (Ta), Titanium (Ti), ...

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CVD Modeling (cont.)

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- Case: $k_s \gg h_g$
 \hookrightarrow surface reaction rate \gg mass transfer rate

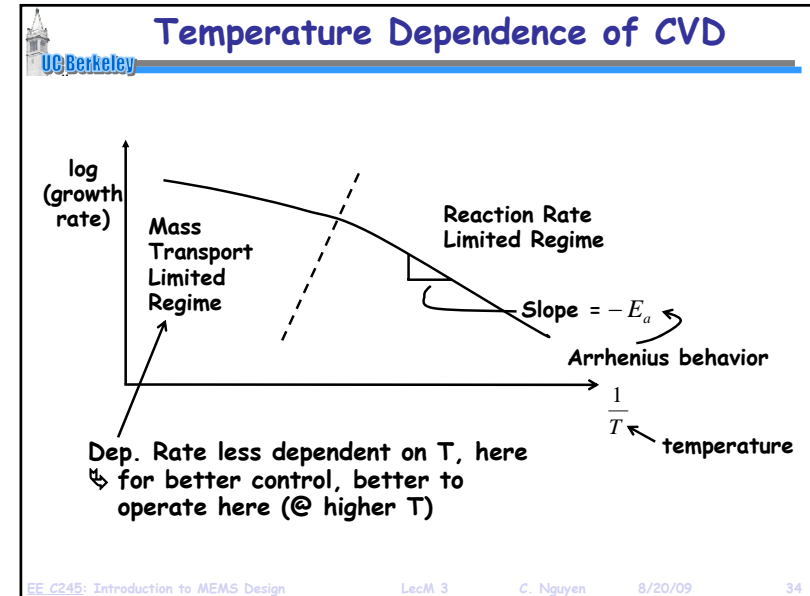
$$\text{growth rate} = h_g \frac{N_g}{N} \quad (\text{mass-transfer-limited})$$

- Case: $h_g \gg k_s$
 \hookrightarrow mass transfer rate \gg surface reaction rate

$$\text{growth rate} = k_s \frac{N_g}{N} \quad (\text{surface-reaction-limited})$$

$\sim R_o^{-E_a/kT}$ (Arrhenius character)

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Atmospheric Pressure Reactor (APCVD)

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The schematic shows a cross-section of a reactor where wafers are fed continuously on a conveyor belt through a chamber containing a heater. Gases (N₂ and Gas) are introduced from the top, and exhaust is removed from the bottom.

- Once used for silicon dioxide passivation in integrated circuits
- Substrates fed continuously
- Large diameter wafers
- Need high gas flow rates
- Mass transport-limited regime (high pressure, so tougher for gas to get to the wafer surface)

Problems/Issues:

- Wafers lay flat, and thus, incorporate foreign particles
- Poor step coverage

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Low Pressure Reactor (LPCVD)

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- Many films available: polysilicon, SiGe, Si₃N₄, SiO₂, phosphosilicate glass (PSG), BPSG, W
- Temp.: 300 \rightarrow 1150°C
- Press.: 30 \rightarrow 250 Pa (200mTorr \rightarrow 2Torr)
- Reaction rate limited; reduced pressure gives gas molecular high diffusivity; can supply reactants very fast!
- Can handle several hundred wafers at a time
- Excellent uniformity

The schematic shows a cross-section of a reactor with a 'Three-zone furnace' and 'Wafers' inside a 'Quartz tube'. A 'Gas inlet' and 'Load door' are on the left, and a 'Pressure sensor' and 'Pump' are on the right.

Problems:

- Low dep. rate (compared to atm.)
- Higher T (than atmospheric)
- In hot wall reactors, get deposition on tube walls (must clean)

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Plasma-Enhanced CVD Reactor (PECVD)

- RF-induced glow discharge + thermal energy to drive reactions → allows lower temperature deposition with decent conformability
- Still low pressure

Problems:

- Pin-holes
- Non-stoichiometric films
- Incorporation of H_2 , N_2 , O_2 contaminants in film; can lead to outgassing or bubbling in later steps

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Polysilicon CVD

Polysilicon Deposition:

$SiH_4 \xrightarrow{600^\circ C} Si + 2H_2$ (thermal decomposition of silane)
(conformal → high T)

LPCVD (25 to 150 Pa) → 100-200 Å/min

- In situ doping of polysilicon:**
 - n-type: add PH_3 (phosphine) or Arsine gases (but greatly reduces dep. rate)
 - p-type: add diborane gas (greatly increases dep. Rate)

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Silicon Oxide CVD

Silicon Dioxide Deposition:

- After metallization** (e.g., over aluminum)
 - Temperature cannot exceed the Si-Al eutectic pt.: $577^\circ C$
 - Actually, need lower than this ($<500^\circ C$) to prevent hillocks from growing on Al surfaces
 - Similar issues for copper (Cu) metallization
- Low temperature reactions:

LPCVD LTO Reactions

$$\begin{aligned} SiH_4 + O_2 &\xrightarrow{300-500^\circ C} SiO_2 + 2H_2 \quad (\text{silane}) \\ 4PH_3 + 5O_2 &\xrightarrow{300-500^\circ C} 2P_2O_5 + 6H_2 \quad (\text{phosphine}) \end{aligned}$$

Phosphosilicate glass (PSG)

- Above reactions: not very conformal step coverage → need higher T for this

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Silicon Oxide CVD (cont.)

- Phosphosilicate glass can be reflow
 - 6-8 wt. % allows reflow @ $1000-1100^\circ C$
 - Very useful to achieve smoother topography
 - Lower concentration → won't reflow
 - Higher concentration → corrodes Al if moisture is present
 - 5-15% P can be used as a diffusion source to dope Si
- Before metallization:**
 - Can use higher temperature → better uniformity and step coverage

HTO

$$SiCl_2H_2 + 2N_2O \xrightarrow{\sim 900^\circ C} SiO_2 + 2N_2 + 2HCl$$

(dichlorosilane) (Nitrous oxide) (nice conformal step coverage)

or ...

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Silicon Oxide CVD (cont.)

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$$\text{Si}(\text{OC}_2\text{H}_5)_4 \xrightarrow{650-750^\circ\text{C}} \text{SiO}_2 + \text{by-products}$$

(Tetraethylorthosilicate) (TEOS) (excellent uniformity & conformal step coverage)

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Silicon Nitride CVD

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Silicon Nitride Deposition:

- First, note that thermal growth is possible:
 - Si in NH_3 @ $1000-1100^\circ\text{C}$
 - But very slow growth rate, thus, impractical
- LPCVD reactions:

Silane reaction: $3\text{SiH}_4 + 4\text{NH}_3 \xrightarrow[700-900^\circ\text{C}]{\text{(Atm. Press.)}} \text{Si}_3\text{N}_4 + 12\text{H}_2$

Dichlorosilane reaction: $3\text{SiCl}_2\text{H}_2 + 4\text{NH}_3 \xrightarrow[700-800^\circ\text{C}]{\text{(LPCVD)}} \text{Si}_3\text{N}_4 + 6\text{HCl} + 6\text{H}_2$

↪ Increase and T = 835°C → Si rich nitride → low stress

Problem: Clobbers your pumps! Expensive to maintain!

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Silicon Nitride CVD (cont.)

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- Comments on LPCVD nitride films:
 - Hydrogen rich: ~8% H_2
 - High internal tensile stresses: films $>1000\text{\AA}$ crack and peel due to excessive stress
 - Can get $2\mu\text{m}$ films with Si-rich nitride
 - LPCVD gives high resistivity ($10^{16} \Omega\text{-cm}$) and dielectric strength (10 MV/cm)

PECVD Nitride:

Nitrogen discharge

$$\text{SiH}_4 + \text{N}_2 \xrightarrow{\text{Ar plasma}} 2\text{SiNH} + 3\text{H}_2$$

or

$$\text{SiH}_4 + \text{NH}_3 \xrightarrow{\text{Ar plasma}} \text{SiNH} + 3\text{H}_3$$

PECVD films:

- Non-stoichiometric nitride
- 20-25% H_2 content
- Can control stress
- ($10^6 \Omega\text{-cm}$) resistivity

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Metal CVD

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CVD Metal Deposition:

Tungsten (W) - deposited by thermal, plasma or optically-assisted decomposition

$$\text{WF}_6 \longrightarrow \text{W} + 3\text{F}_2$$

or via reaction with H_2 :

$$\text{WF}_6 + 3\text{H}_2 \longrightarrow \text{W} + 6\text{HF}$$

Other Metals - Molybdenum (Mo), Tantalum (Ta), and Titanium (Ti)

$$2\text{MCl}_5 + 5\text{H}_2 \longrightarrow 2\text{M} + 10\text{HCl},$$

where M = Mo, Ta, or Ti

(Even Al can be CVD'ed with tri-isobutyl Al ... but other methods are better.)

(Cu is normally electroplated)

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