

**PROBLEM SET #6**

*Issued: Tuesday, Oct. 30, 2012*

*Due (at 7 p.m.): Tuesday Nov. 20, 2012, in the EE C245 HW box near 125 Cory.*

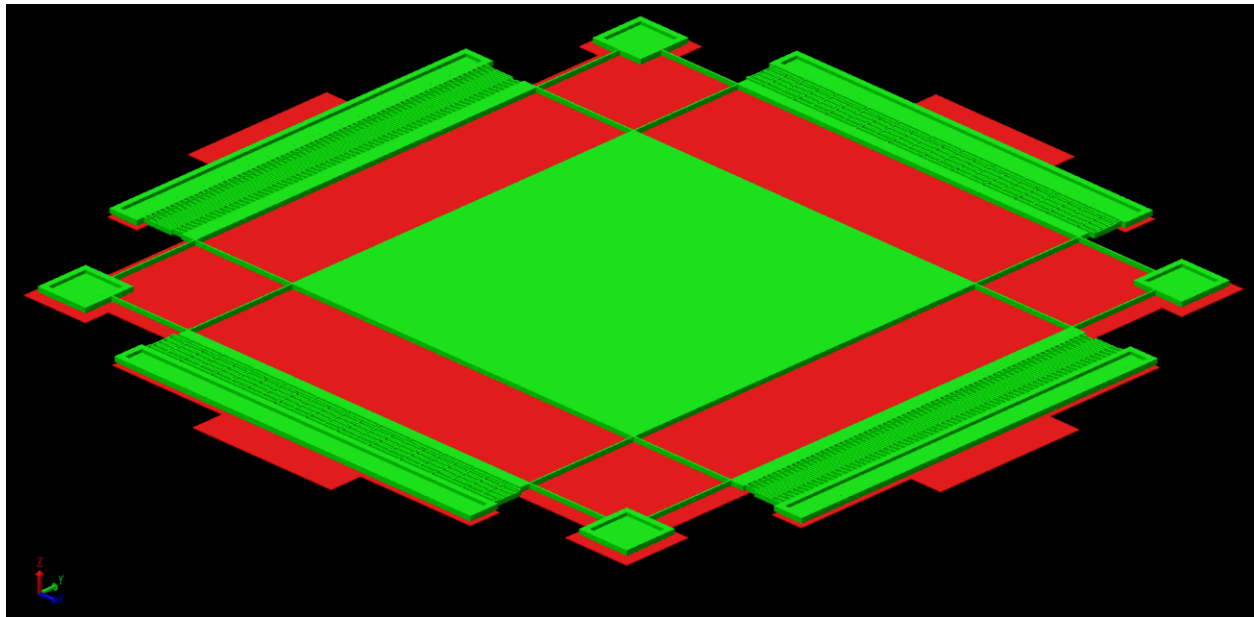
Figures PS6.1-6 show a dual-axis  $x$ - $y$  accelerometer manufactured via the following 3-mask surface micromachining process:

- i) Deposit 1.0  $\mu\text{m}$  of  $\text{SiO}_2$  on a Silicon wafer
- ii) Deposit 300 nm of  $\text{SiN}_3$  via LPCVD
- iii) Deposit 200 nm of in-situ doped polysilicon
- iv) Lithographically define and etch polysilicon interconnects (anisotropic)
- v) Deposit 2.0  $\mu\text{m}$  of  $\text{SiO}_2$  (LTO)
- vi) Lithographically define and then etch anchor openings in  $\text{SiO}_2$  (anisotropic)
- vii) Deposit 3.0  $\mu\text{m}$  of in-situ doped polysilicon
- viii) Lithographically define and then etch the polysilicon structure (anisotropic)
- ix) Etch  $\text{SiO}_2$  completely using an HF etch, releasing structure (isotropic)

Assume all materials are stress-free at room temperature and have the material properties listed in Table PS6.1.

**Table PS6.1**

Material	$\rho_m$ $\text{kg/m}^3$	$E$ GPa	$\nu$	$\alpha_T$ $\mu\text{strain/K}$	$\sigma_0$ MPa	Comment
Polysilicon	2300	150	0.2	2.8	Varies	Random Grains
Silicon Dioxide	2200	69	0.17	0.7	-300	Amorphous
Silicon Nitride	3170	270	0.27	2.3	1100	Stoichiometric



**Figure PS6.1 – Perspective view of the accelerometer.**

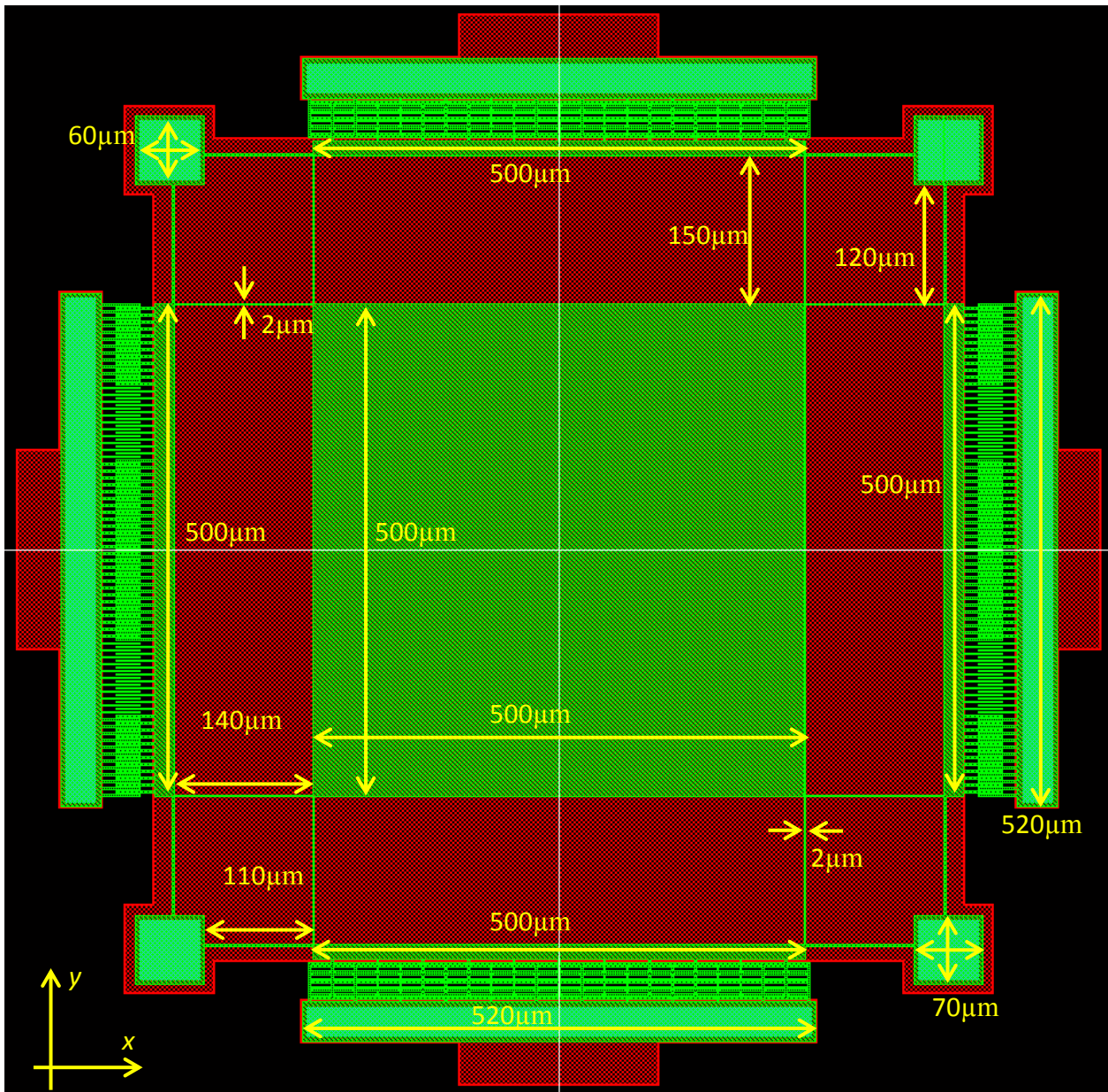


Figure PS6.2 – Top view of the accelerometer.

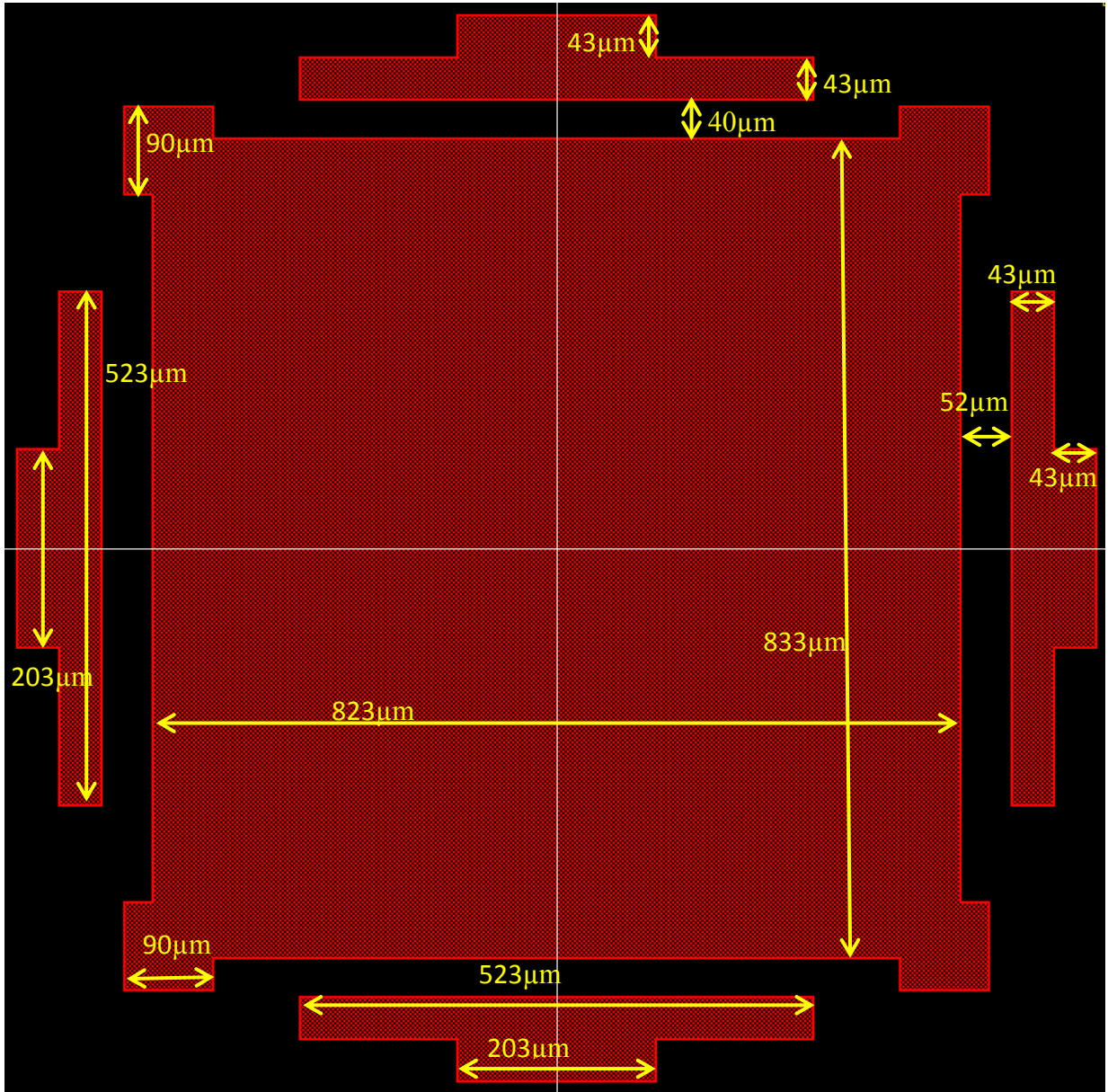


Figure PS6.3 – Top view of accelerometer showing only the interconnect layer.

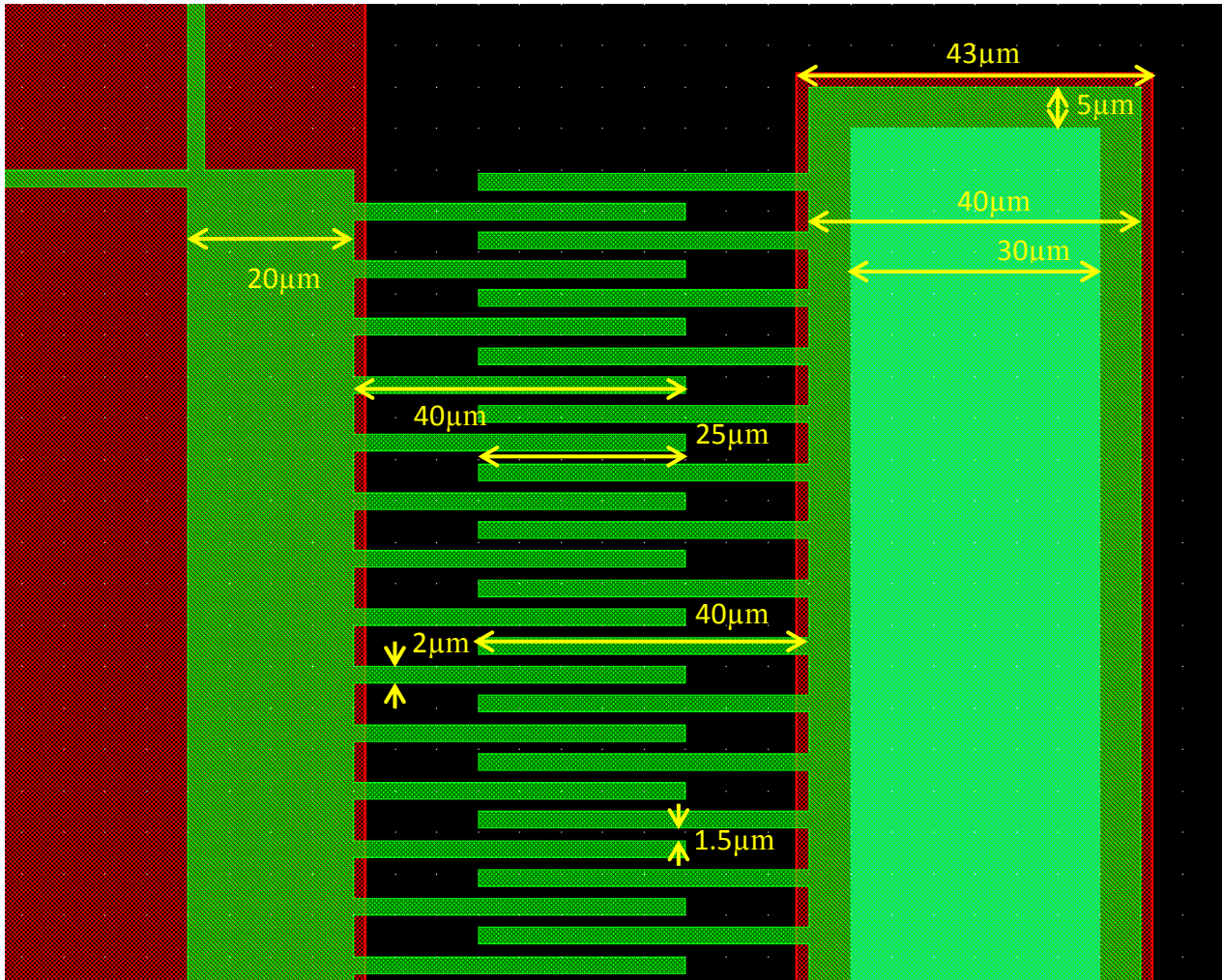


Figure PS6.4 – Zoom-in view of the x-direction interdigital comb finger structure. There are 71 fingers on each side of the proof mass.

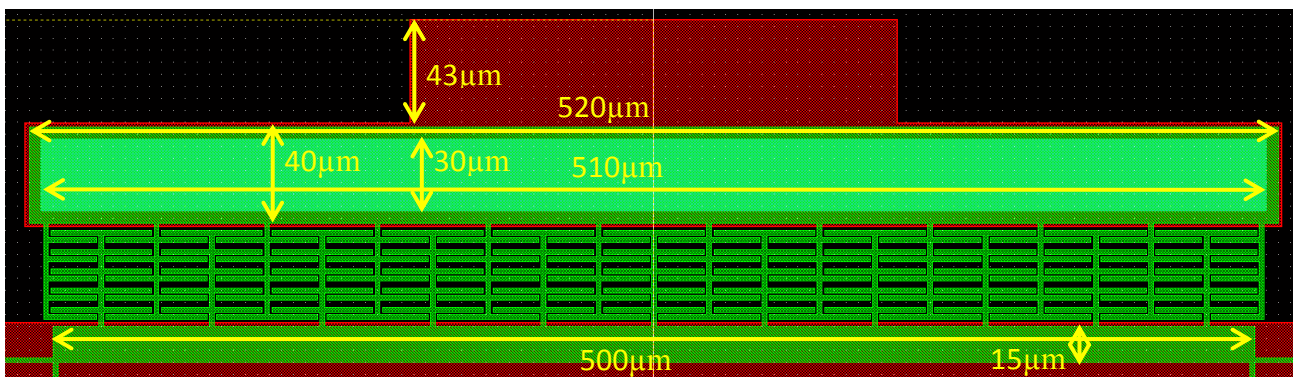


Figure PS6.5 – Top view showing the y-direction capacitor structure.

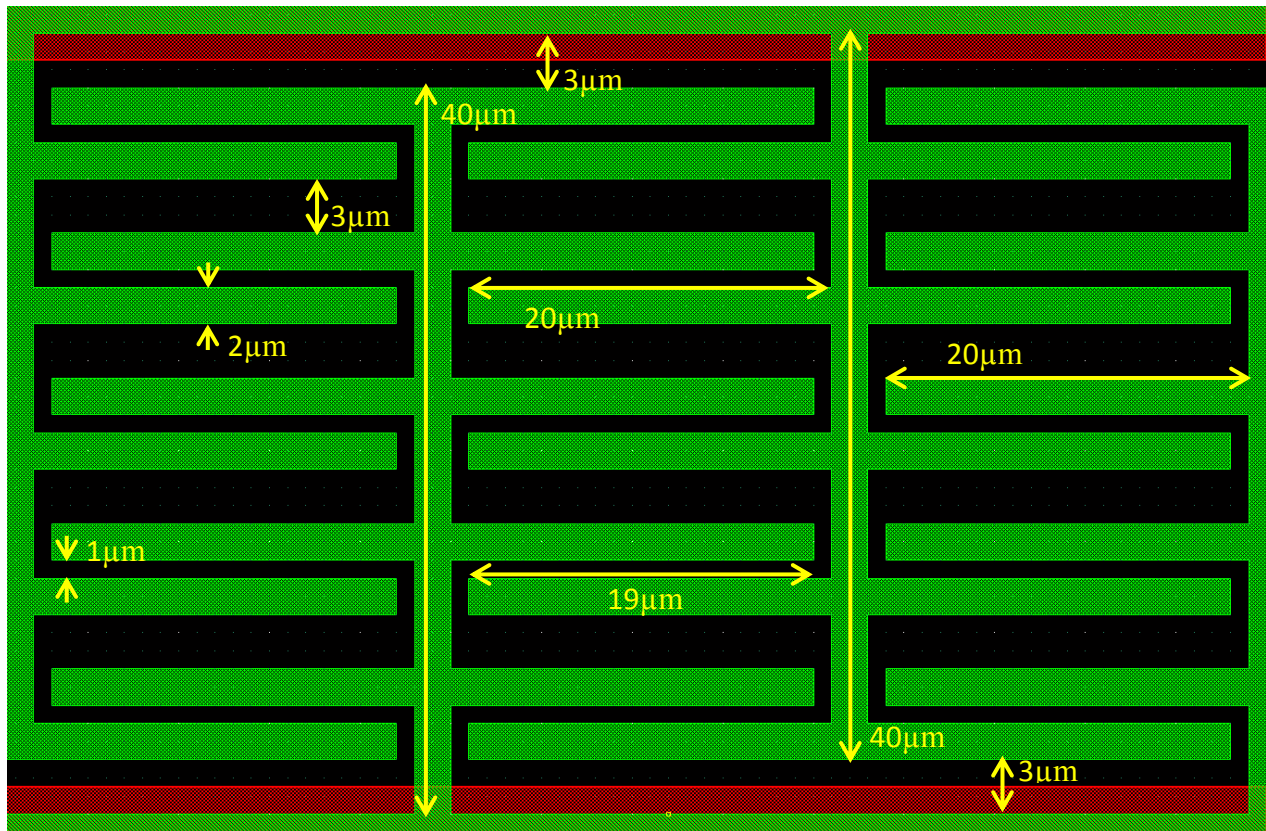


Figure PS6.6 – Zoom-in view of the y-direction capacitor structure.

1. Calculate the  $x$ - and  $y$ -directed resonance frequencies of the accelerometer structure with no applied DC bias, making simplifying assumptions as necessary. Do NOT neglect the beam masses in these calculations. Assuming a quality-factor  $Q$  of 5 in both directions, draw the frequency response for the accelerometer in both the  $x$ - and  $y$ -directions.
2. Derive an expression for the capacitance between port  $A$  and  $B$  shown in Figure PS6.7 as a function of displacement  $x$  using a parallel-plate approximation. Also, calculate the overlap capacitance between these two ports at rest.
3. Derive an expression for the capacitance between port  $A$  and  $C$  shown in Figure PS6.7 as a function of displacement  $y$  using a parallel-plate approximation. Also calculate the overlap capacitance between these two ports at rest.
4. Suppose the accelerometer is now hooked up as shown in Figure PS6.7, with a DC bias  $V_{bias}$  of 10V applied to the structure.
  - (a) Calculate the new  $x$ - and  $y$ -directed resonance frequencies with this DC bias.
  - (b) If a sinusoidal force signal is applied to the structure in the  $x$ -direction with a magnitude of  $1g$ , what will be the magnitude and phase of the resulting output current  $i_B$  as a function of frequency?

- (c) If a sinusoidal force signal is applied to the structure in the  $y$ -direction with a magnitude of  $1g$ , what will be the magnitude and phase of the resulting output current  $i_C$  as a function of frequency?

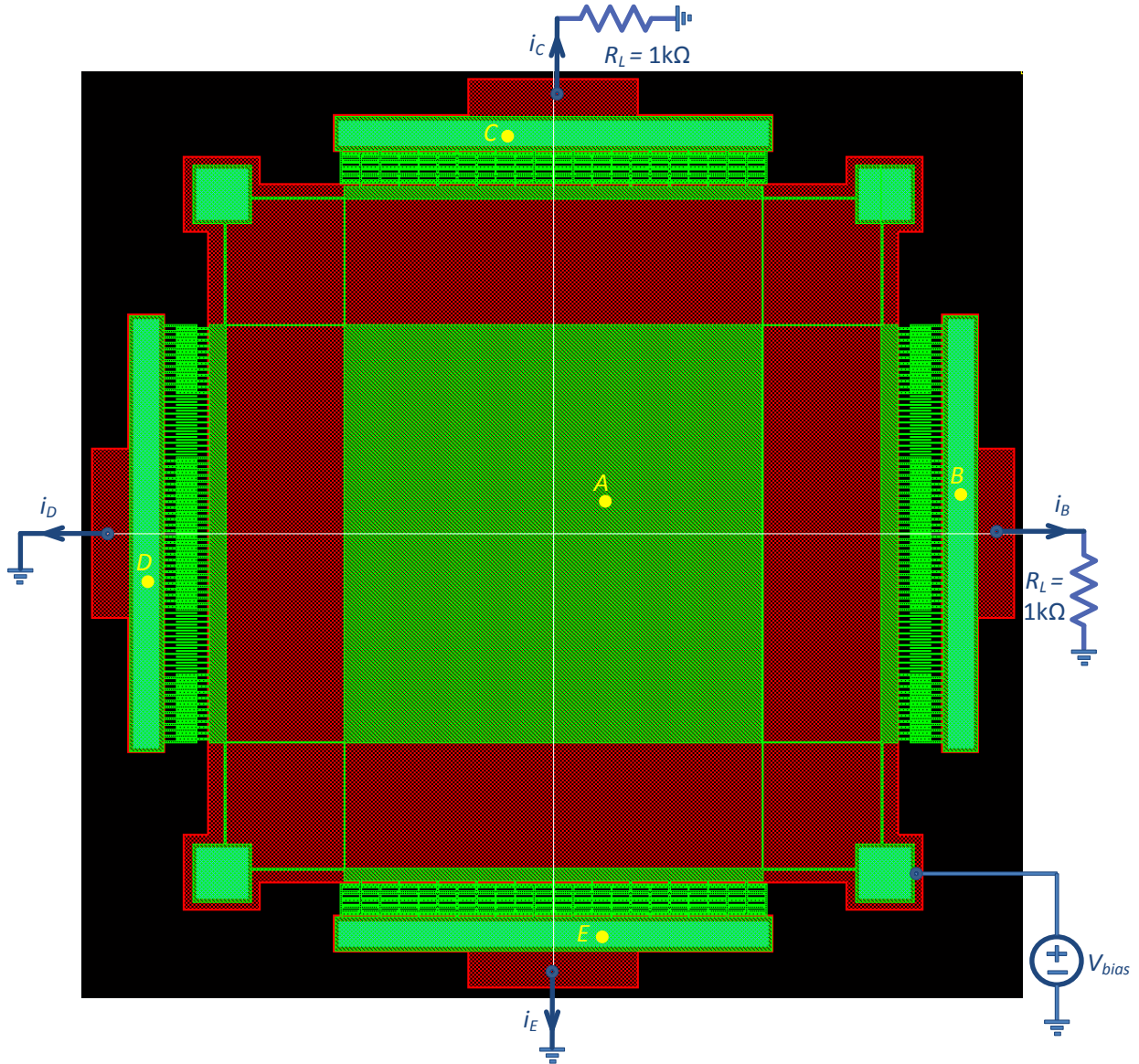


Figure PS6.7 – Top view of the accelerometer with circuit connections for problem 4.