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## EE C245 - ME C218 Introduction to MEMS Design Fall 2012

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Lecture Module 7: Mechanics of Materials

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## Outline

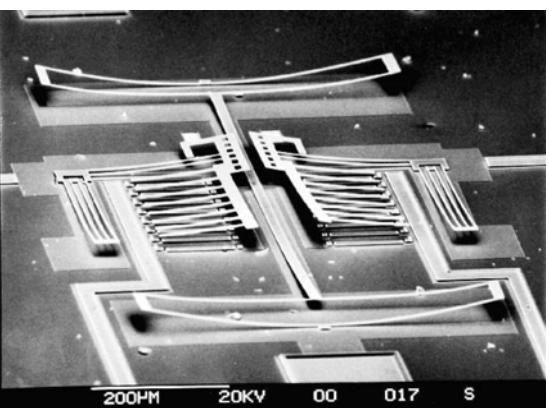
- Reading: Senturia, Chpt. 8
- Lecture Topics:
  - ↳ Stress, strain, etc., for isotropic materials
  - ↳ Thin films: thermal stress, residual stress, and stress gradients
  - ↳ Internal dissipation
  - ↳ MEMS material properties and performance metrics

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## Vertical Stress Gradients

- Variation of residual stress in the direction of film growth
- Can warp released structures in z-direction



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## Elasticity

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## Lecture 12m2: Mechanics of Materials

### Normal Stress (1D)

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If the force acts normal to a surface, then the stress is called a **normal stress**.

Force assumed uniform over the whole area A

Standard mks unit:  $\text{N/m}^2 = \text{Pa}$

**Microscopic Definition:** force per unit area acting on the surface of a differential volume element of a solid body.

**Note:** assume stress acts uniformly across the entire surface of the element, not at just a point.

Differential volume element:  $\Delta V = \Delta x \Delta y \Delta z$

Stress:  $\sigma = \frac{F}{A}$  [N/m<sup>2</sup> : Pa]

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### Strain (1D)

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stretch (length) / initial length

Sometimes a unit called the "microstrain" is used, where  $1\mu\varepsilon = \frac{\Delta L}{L} \text{ or } 1\mu\varepsilon = \frac{L'-L}{L}$

Strain:  $\varepsilon = \frac{L'-L}{L} = \frac{\Delta L}{L}$  [unitless]

In the elastic regime (i.e., for "small" stresses at "low" temperatures), strain is found to be proportional to stress.

For solids:  $\sigma = E\varepsilon$  →  $E = \frac{\sigma}{\varepsilon}$  [unitless]

slope:  $E = \text{Young's modulus of elasticity}$

Thus, the units of  $E$  are the same as  $\sigma \rightarrow \text{Pa}$

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### The Poisson Ratio

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Apply normal stress to a free-standing object → uniaxial strain but also get contraction in directions transverse to the uniaxial strain.

⇒ contraction creates a (-) strain:

$$\varepsilon_y = \frac{W-W'}{W} = -\nu \varepsilon_x$$

$\nu$ : Poisson ratio [unitless]

Typical values:  $0 \rightarrow 0.5$

⇒ inorganic solids:  $0.2 \rightarrow 0.3$

⇒ elastomers (e.g., rubber):  $\sim 0.5$

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### Shear Stress & Strain (1D)

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Note: Assume compensating forces are applied to the vertical faces to avoid a net torque. (This by convention.) nothing rotates

Shear Stress:  $\tau = \frac{F}{A}$  [Pa]

Generates a shear strain:

$$\theta = \frac{\tau}{G}$$

$G \triangleq \text{shear modulus}$

$$G = \frac{E}{2(1+\nu)}$$

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## Lecture 12m2: Mechanics of Materials

## 2D and 3D Considerations

**Important assumption:** the differential volume element is in static equilibrium  $\rightarrow$  no net forces or torques (i.e., rotational movements)

- Every  $\sigma$  must have an equal  $\sigma$  in the opposite direction on the other side of the element
- For no net torque, the shear forces on different faces must also be matched as follows:

$$\tau_{xy} = \tau_{yx} \quad \tau_{xz} = \tau_{zx} \quad \tau_{yz} = \tau_{zy}$$

Stresses acting on a differential volume element

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## 2D Strain

- In general, motion consists of
  - rigid-body displacement (motion of the center of mass)
  - rigid-body rotation (rotation about the center of mass)
  - Deformation relative to displacement and rotation

Area element experiences both displacement and deformation

- Must work with displacement vectors
- Differential definition of axial strain:  $\epsilon_x = \frac{u_x(x + \Delta x) - u_x(x)}{\Delta x} = \frac{\partial u_x}{\partial x}$

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## 2D Shear Strain

Rotate clockwise by  $\theta_2$

$\Rightarrow$  For shear strains, must remove any rigid body rotation that accompanies the deformation  
↳ use a symmetric definition of shear strain:

$$\gamma_{xy} = \theta_2 + \theta_1 \approx \left( \frac{\Delta u_x}{\Delta y} + \frac{\Delta u_y}{\Delta x} \right) = \left( \frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right)$$

For small amplitude deformations.

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## Volume Change for a Uniaxial Stress

Given an  $x$ -directed uniaxial stress,  $\sigma_x$ :

$$\begin{aligned} \Delta x &\rightarrow \Delta x(1 + \epsilon_x) \\ \Delta y &\rightarrow \Delta y(1 - \gamma \epsilon_x) \\ \Delta z &\rightarrow \Delta z(1 - \gamma \epsilon_x) \end{aligned}$$

The resulting change in volume  $\Delta V$

$$\Delta V = \Delta x \Delta y \Delta z (1 + \epsilon_x)(1 - \gamma \epsilon_x)^2 - \Delta x \Delta y \Delta z = \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - \gamma \epsilon_x)^2 - 1]$$

{Assume small strains}  $\Rightarrow \Delta V = \Delta x \Delta y \Delta z [(1 + \epsilon_x)(1 - 2\gamma \epsilon_x) - 1] \approx \Delta x \Delta y \Delta z [1 + \epsilon_x - 2\gamma \epsilon_x - 2\epsilon_x^2]$

$$\Delta V \approx \Delta x \Delta y \Delta z (1 - 2\gamma) \epsilon_x$$

For  $\gamma = 0.5$  (rubber)  $\rightarrow$  no  $\Delta V$ !  
 $\gamma < 0.5 \rightarrow$  finite  $\Delta V$

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## Isotropic Elasticity in 3D

- Isotropic = same in all directions
- The complete stress-strain relations for an isotropic elastic solid in 3D: (i.e., a generalized Hooke's Law)

$$\varepsilon_x = \frac{1}{E} [\sigma_x - \nu(\sigma_y + \sigma_z)] \quad \gamma_{xy} = \frac{1}{G} \tau_{xy}$$
$$\varepsilon_y = \frac{1}{E} [\sigma_y - \nu(\sigma_z + \sigma_x)] \quad \gamma_{yz} = \frac{1}{G} \tau_{yz}$$
$$\varepsilon_z = \frac{1}{E} [\sigma_z - \underbrace{\nu(\sigma_x + \sigma_y)}_{\text{Basically, add in off-axis strains from normal stresses in other directions}}] \quad \gamma_{zx} = \frac{1}{G} \tau_{zx}$$

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