

HW12 Solutions

1. (10 points)

(a)

In the saturation region, $V_{DS} \geq V_{GS} - V_{t0} = 2V$

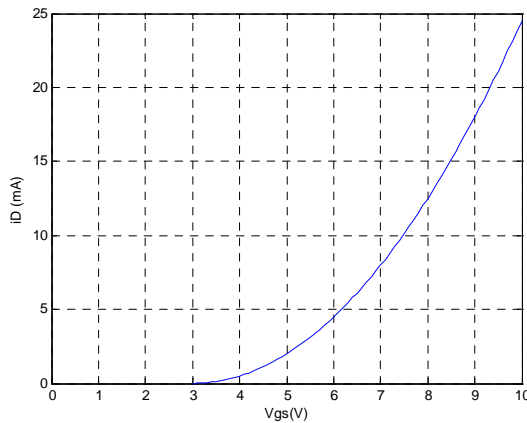
In the triode region, $V_{DS} \leq V_{GS} - V_{t0} = 2V$

Also check $V_{GS} \geq V_{t0}$ so it's not operated in the cutoff region

(b)

In the saturation region,

$$i_D = K(V_{GS} - V_{t0})^2 = 0.5(V_{GS} - 2)^2$$



2. (10 points)

When $V_{GS} = V_{DS} = 5V$, the transistor is operated in the saturation region.

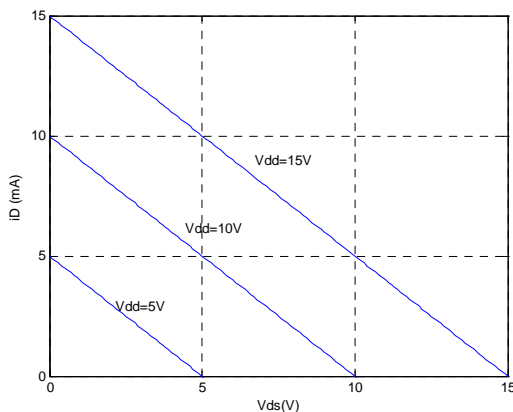
$$i_D = \left(\frac{W}{L}\right) \frac{KP}{2} (V_{GS} - V_{t0})^2$$

Substitute all the values into the equation and we can solve $W/L=1.25$.

For $L=2\mu m$, we need $W=2.5\mu m$.

3. (10 points)

The load-line equation is $V_{DD} = R_D i_D + V_{DS}$, and the plots are:



4. (10 points)

(a) The 1.7M Ω and 300k Ω resistors act as a voltage divider that gives a dc voltage $V_{GSQ} = 3V$. The capacitor is treated as a short for the ac signal, so we have,

$$V_{GS}(t) = 3 + \sin(2000\pi t)$$

(b) –(d)

Three operation regions:

Cutoff: $V_{GS} \leq V_{t0}$

$$i_D = 0$$

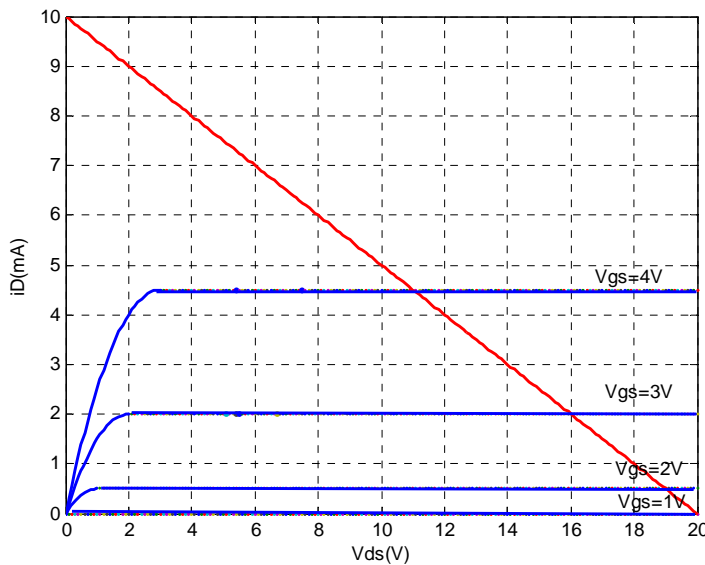
Triode: $V_{GS} \geq V_{t0}, V_{DS} \leq V_{GS} - V_{t0}$

$$i_D = K[2(v_{GS} - V_{t0})v_{DS} - v_{DS}^2]$$

Saturation: $V_{GS} \geq V_{t0}, V_{DS} \geq V_{GS} - V_{t0}$

$$i_D = K(V_{GS} - V_{t0})^2$$

The load-line equation is $V_{DD} = 2k * i_D + V_{DS}$



From the load-line, we find $V_{DSQ} = 16V$, $V_{DS \max} = 19V$, and $V_{DS \min} = 11V$.

5. (10 points)

(a) Assume the FET is operated in the saturation region,

$$I_{DQ} = K(V_{GSQ} - V_{t0})^2 \quad (1)$$

$$V_G = 20 \frac{1M}{1M + 1M} = 10V \quad \text{from voltage divider.}$$

$$\text{Using KVL, we get } V_{GSQ} + I_{DQ} \times 1k\Omega = 10V \quad (2)$$

Solving equations (1) & (2), $I_{DQ} = 4mA$, $V_{GSQ} = 6V$, and

$$V_{DSQ} = 20V - I_{DQ}(1k + 1k) = 12V$$

Verification: $V_{DSQ} \geq V_{GSQ} + V_{t0}$, so it's in the saturation region.

(b) Assume the FET is operated in the saturation region. Similar to part (a), we can solve

$$I_{DQ} = 6.234\text{mA}, \quad V_{GSQ} = 3.765\text{V}, \quad \text{and} \quad V_{DSQ} = 20\text{V} - I_{DQ}(1\text{k} + 1\text{k}) = 7.53\text{V}$$

Verification: $V_{DSQ} \geq V_{GSQ} + V_{t0}$, so it's in the saturation region.

6. (10 points)

Write $V_{DD} = R_D I_{DQ} + V_{DSQ} + R_S I_{DQ}$. Substituting values and solving we obtain $R_S = 3\text{k}\Omega$. Next We have $K = 1/2 KP(W/L) = 0.2\text{mA/V}^2$.

Assuming the NMOS operates in saturation, we have $I_{DQ} = K(V_{GSQ} - V_{t0})^2$. Substituting values and solving we obtain $V_{GSQ} = -1.236\text{V}$ and $V_{GSQ} = 3.236\text{V}$. The correct root is $V_{GSQ} = 3.236\text{V}$. Then we have $V_G = V_{GSQ} + R_S I_{DQ} = 6.236\text{V}$. However we also have $V_G = V_{DD} R_2 / (R_1 + R_2)$. Substituting values and solving we obtain $R_2 = 1.082\text{M}\Omega$

7. (10 points)

We have $V_G = V_{GSQ} = 10 R_2 / (R_1 + R_2) = 2.5\text{V}$. Then we have $I_{DQ} = K(V_{GSQ} - V_{t0})^2 = 0.5625\text{mA}$.
 $V_{DSQ} = V_{DD} - R_D I_{DQ} = 4.375\text{V}$.

8. (10 points)

For constant drain current in the saturation region, we have $r_d = \infty$.

9. (10 points)

$$g_m = \left. \frac{\partial i_D}{\partial V_{GS}} \right|_{Q-\text{point}} = 9V_{GS}^{-2} \Big|_{Q-\text{point}} = 9\text{mS}$$

$$1/r_d = \left. \frac{\partial i_D}{\partial V_{DS}} \right|_{Q-\text{point}} = 0.1 \Big|_{Q-\text{point}} = 0.1\text{mS}$$

$$r_d = 10\text{k}\Omega$$

10. (10 points)

From Figure P12.41 at an operating point defined by $V_{GSQ}=2.5$ V and $V_{DSQ}=6$ V, we have

$$g_m = \frac{\Delta i_D}{\Delta V_{GS}} = \frac{(6.4 - 1.5)mA}{1V} = 4.9mS$$

$$1/r_d = \frac{\Delta i_D}{\Delta V_{GS}} \cong \frac{(4.0 - 3.1)mA}{(8 - 4)V} = 0.225 \times 10^{-3}$$

Taking the reciprocal, we find $r_d = 4.44k\Omega$