

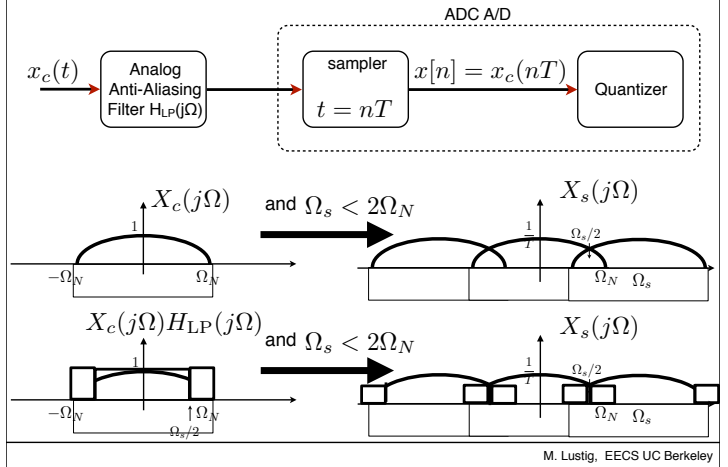
EE123

# Digital Signal Processing

## Lecture 19 Practical ADC/DAC

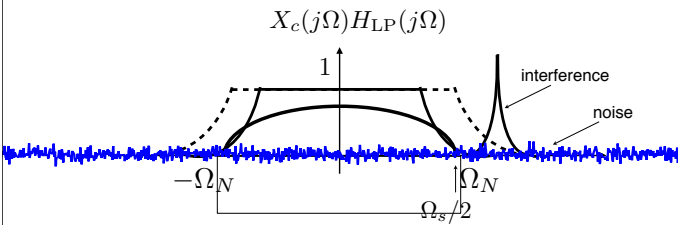
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### Ideal Anti-Aliasing



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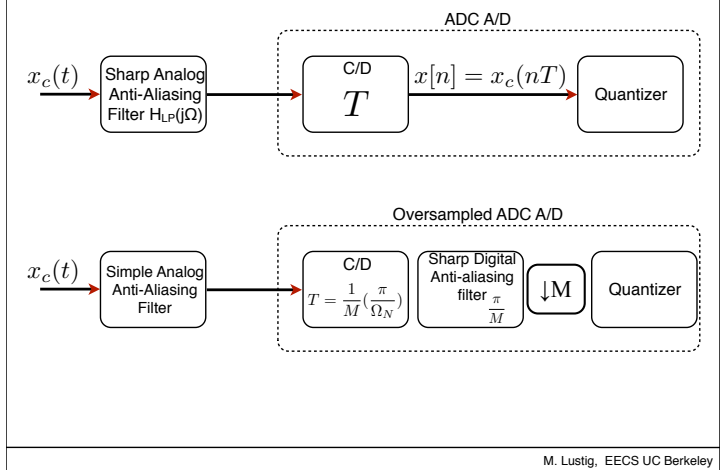
### Non Ideal Anti-Aliasing



- Problem: Hard to implement sharp analog filter
- Tradeoff:
  - Crop part of the signal
  - Suffer from noise and interference (See lab II !)

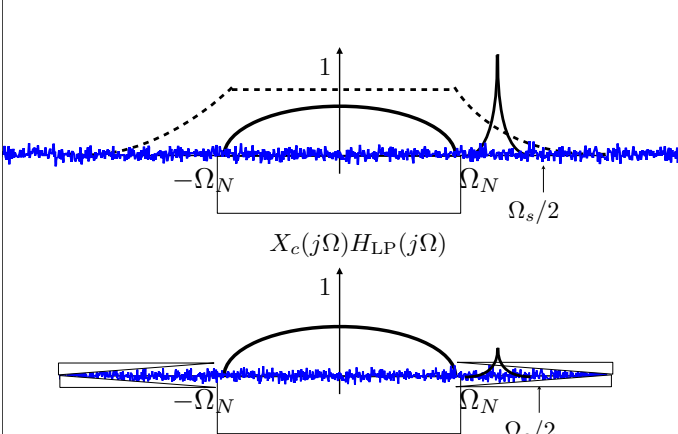
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### Oversampled ADC



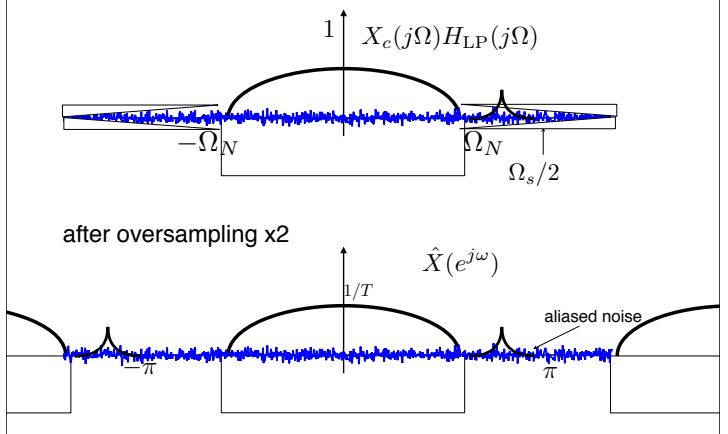
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### Oversampled ADC

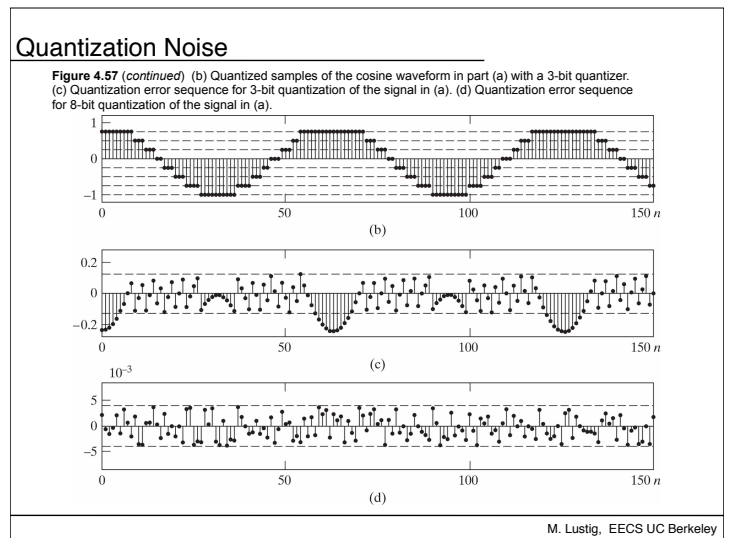
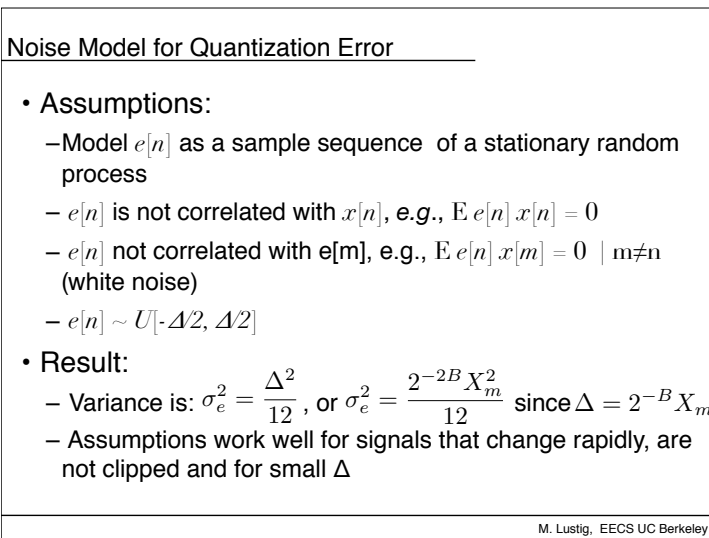
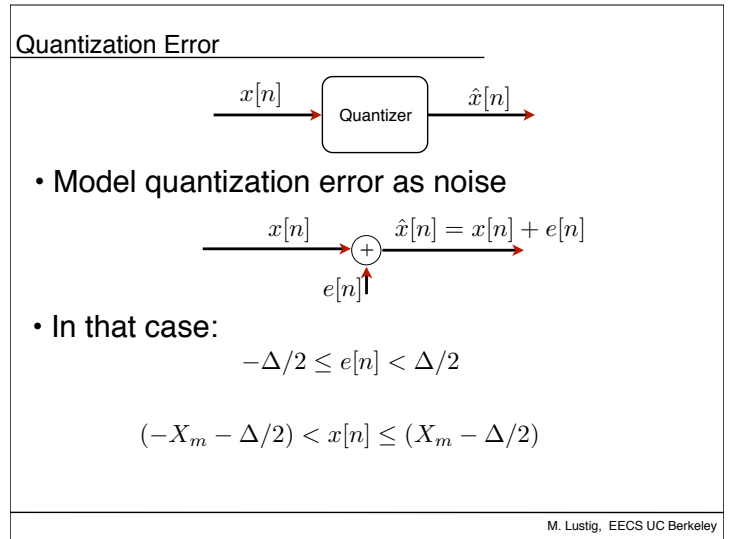
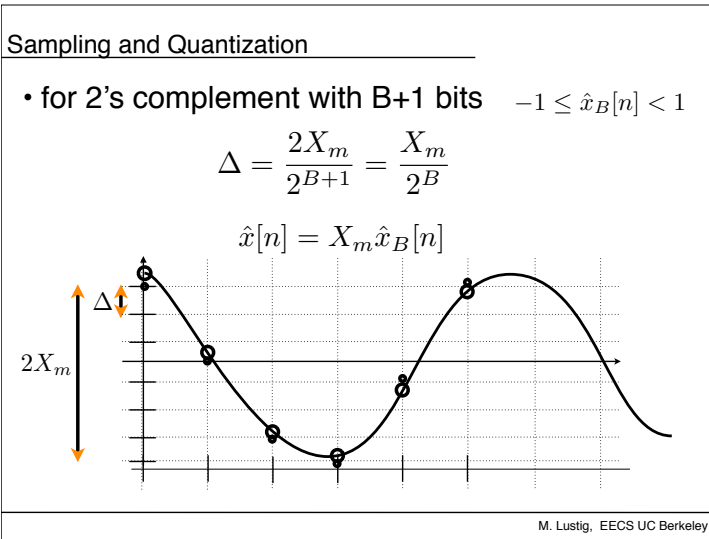
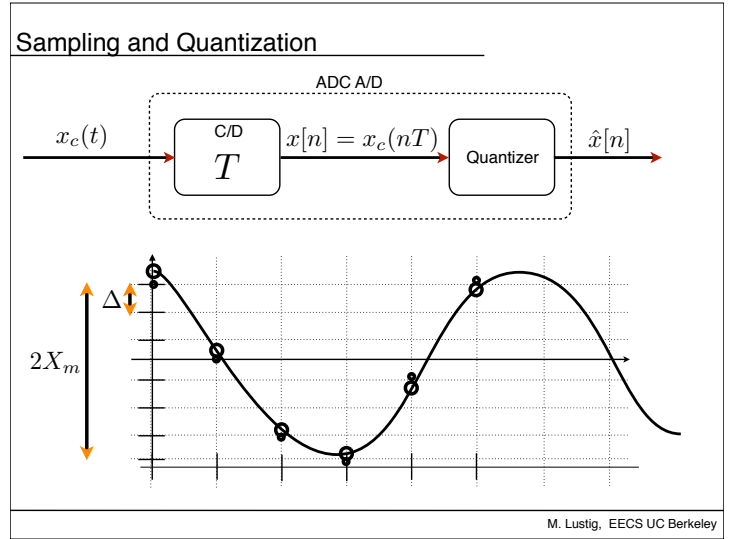
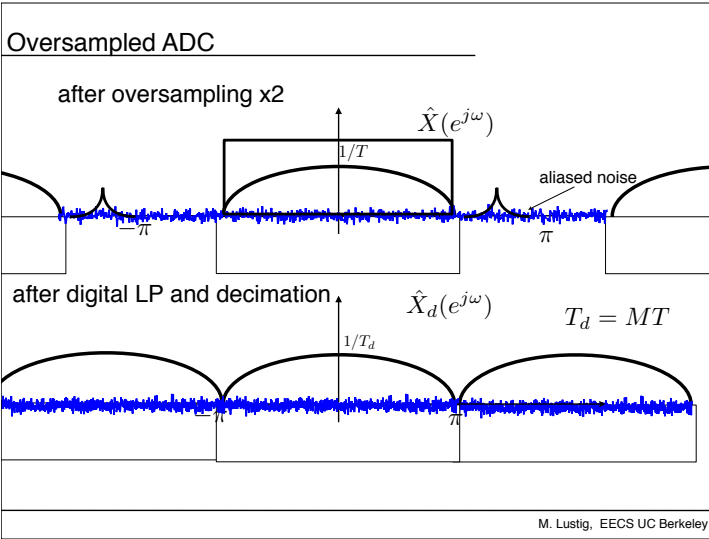


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### Oversampled ADC



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### SNR of Quantization Noise

• For uniform B+1 bits quantizer:  $\sigma_e^2 = \frac{2^{-2B} X_m^2}{12}$

$$\begin{aligned} SNR_Q &= 10 \log_{10} \left( \frac{\sigma_x^2}{\sigma_e^2} \right) \\ &= 10 \log_{10} \left( \frac{12 \cdot 2^{2B} \sigma_x^2}{X_m^2} \right) \end{aligned}$$

$$SNR_Q = 6.02B + 10.8 - 20 \log_{10} \left( \frac{X_m}{\sigma_x} \right) \text{rms of amp}$$

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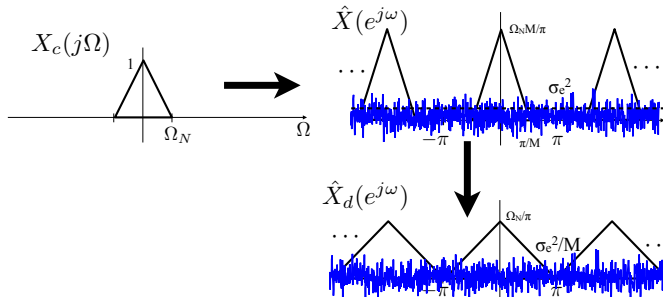
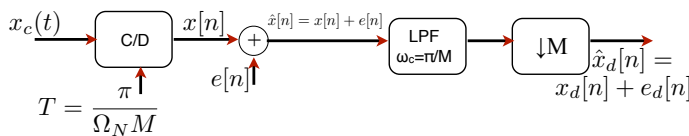
### SNR of Quantization Noise

$$SNR_Q = 6.02B + 10.8 - 20 \log_{10} \left( \frac{X_m}{\sigma_x} \right) \text{Quantizer range rms of amp}$$

- Improvement of 6dB with every bit
- The range of the quantization must be adapted to the rms amplitude of the signal
  - Tradeoff between clipping and noise!
  - Often use pre-amp
  - Sometimes use analog auto gain controller (AGC)
  - If  $\sigma_x = X_m/4$  then  $SNR_Q \approx 6B - 1.25dB$   
so SNR of 90-96 dB requires 16-bits (audio)

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### Quantization noise in Oversampled ADC



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### Quantization noise in Oversampled ADC

- Energy of  $x_d[n]$  equals energy of  $x[n]$ 
  - No filtering of signal!
- Noise std is reduced by factor of M

$$SNR_Q = 6.02B + 10.8 - 20 \log_{10} \left( \frac{X_m}{\sigma_x} \right) + 10 \log_{10} M$$

- For doubling of M we get 3dB improvement, which is the same as 1/2 a bit of accuracy
  - With oversampling of 16 with 8bit ADC we get the same quantization noise as 10bit ADC!

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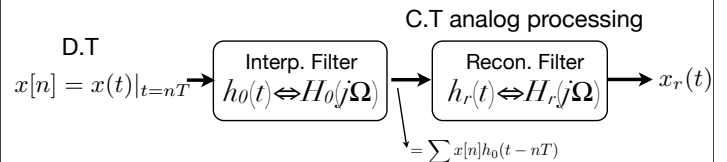
### Practical ADC (Ch. 4.8.4)

$$\text{D.T } x[n] = x(t)|_{t=nT} \rightarrow \text{sinc pulse generator} \rightarrow x_r(t) = \sum_{n=-\infty}^{\infty} x[n] \text{sinc} \left( \frac{t-nT}{T} \right) \text{C.T}$$

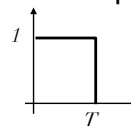
- Scaled train of sinc pulses
- Difficult to generate sinc  $\Rightarrow$  Too long!

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### Practical ADC



- $h_0(t)$  is finite length pulse  $\Rightarrow$  easy to implement
- For example: zero-order hold

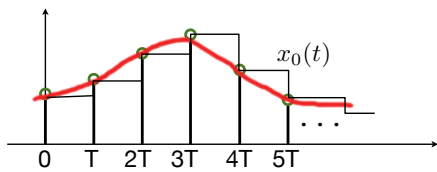


$$H_0(j\Omega) = T e^{-j\Omega \frac{T}{2}} \text{sinc} \left( \frac{\Omega}{\Omega_s} \right)$$

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### Practical ADC

Zero-Order-Hold interpolation



$$x_0(t) = \sum_{n=-\infty}^{\infty} x[n]h_0(t - nT) = x_0(t) * x_s(t)$$

Taking a FT:

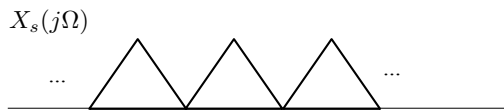
$$\begin{aligned} X(j\Omega) &= H_0(j\Omega)X_s(j\Omega) \\ &= H_0(j\Omega)\frac{1}{T}\sum_{k=-\infty}^{\infty} X(j(\Omega - k\Omega_s)) \end{aligned}$$

### Practical ADC

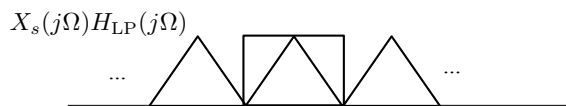
Output of the reconstruction filter:

$$\begin{aligned} X_r(j\Omega) &= H_r(j\Omega) \cdot H_0(j\Omega) \cdot X_s(j\Omega) \\ &= \underbrace{H_r(j\Omega)}_{\text{recon filter}} \cdot \underbrace{T e^{-j\Omega \frac{T}{2}} \text{sinc}\left(\frac{\Omega}{\Omega_s}\right)}_{\text{from zero-order hold}} \cdot \underbrace{\frac{1}{T} \sum_{k=-\infty}^{\infty} X(j(\Omega - k\Omega_s))}_{\text{Shifted copies from sampling}} \end{aligned}$$

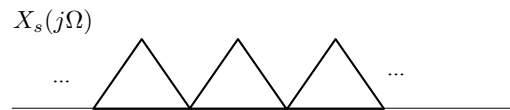
### Practical ADC



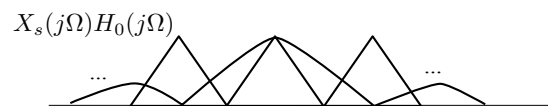
Ideally:



### Practical ADC



Practically:



### Practical ADC



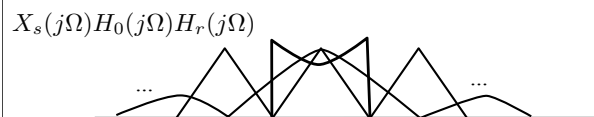
Practically:



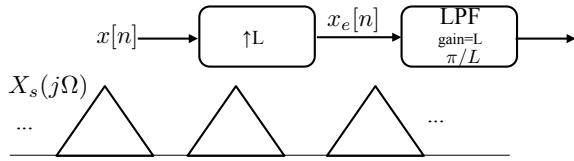
### Practical ADC



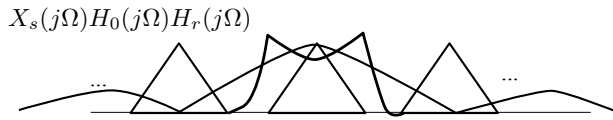
Practically:



### Easier Implementation with Digital upsampling



Practically:



### Easier Implementation with Digital upsampling

