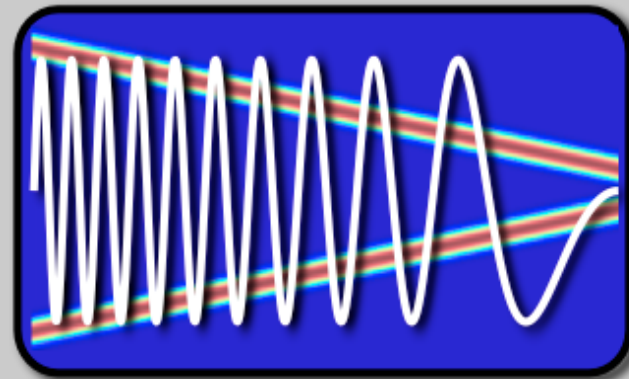


EE123



Digital Signal Processing

Lecture 31 Generalized Linear Phase Systems

Project

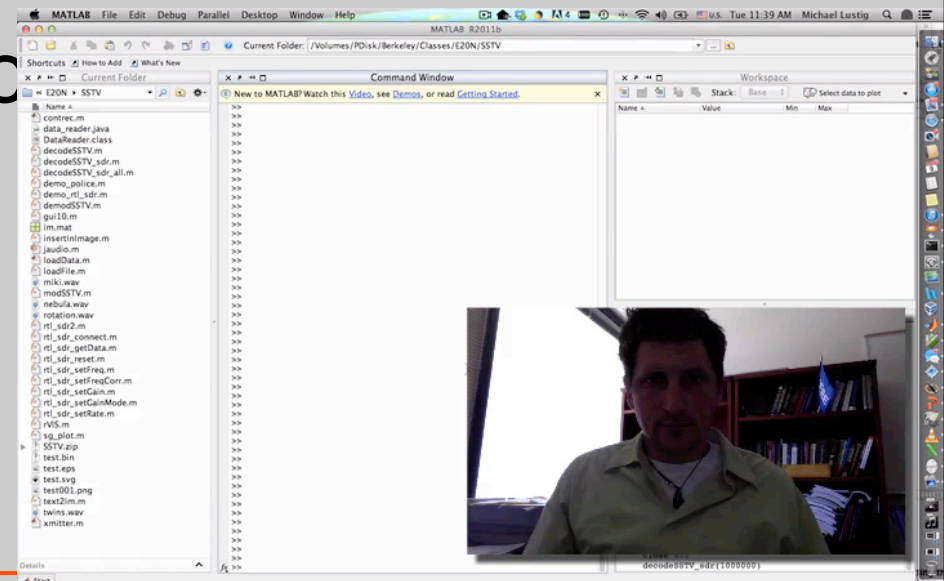
- Select a project by next Friday
 - Submit 2 paragraphs project proposal in bcourses
 - Includes partners and idea of approach
- Project Deliverables
 - Software
 - Demo
 - A few slides / Poster

Default Project

- Image communication
 - We will give you an image
 - You will need to transmit it with the best quality over a limited amount of time (1 min)
 - Evaluation is based on PICSNR and visual quality score
- You can use ANY method you write yourself
 - Compression
 - Filtering, image recovery....
 - Modulation (digital or analog), detection,

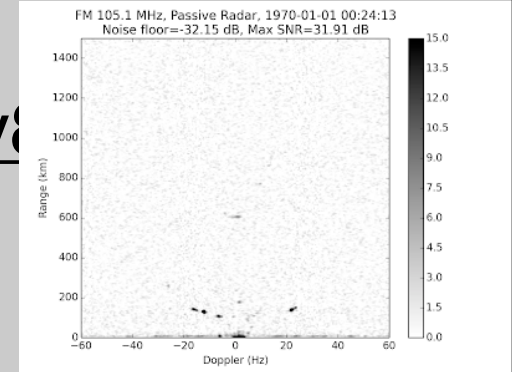
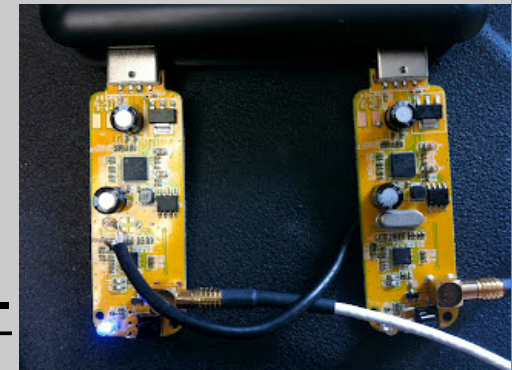
Default project

- Evaluation based on
 - Comparison to a baseline implementation with packet APRS -- slow and low res
 - Scope
 - Creativity
 - Presentation
- Winner gets a prize: radio

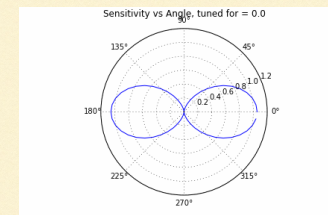


Other projects

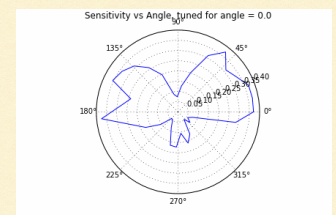
- If you REALLY want to do something else...
- Phased array passive radar
 - <http://kaira.sgo.fi/2013/09/passive-radar-with-16-dual-coherent.html>
 - <https://www.youtube.com/watch?v=6WivkA>
- Electronically steerable antenna
 - (Gabe Buckmater EE123 2014)



Simulated



Measured



Other projects

- Weak Signal communications with OOK and incoherent codes
 - Inspired by JT65
 - Used for telemetry low-rate
- <http://physics.princeton.edu/pulsar/K1JT/JT65.pdf>

```
1,0,0,1,1,0,0,0,1,1,1,1,1,1,0,1,0,1,0,0,0,1,0,1,1,0,0,1,0,0,  
0,1,1,1,0,0,1,1,1,1,0,1,1,0,1,1,1,1,0,0,0,1,1,0,1,0,1,0,1,1,  
0,0,1,1,0,1,0,1,0,1,0,0,1,0,0,0,0,0,1,1,0,0,0,0,0,0,0,1,1,  
0,1,0,0,1,0,1,1,0,1,0,1,0,1,0,0,1,1,0,0,1,0,0,1,0,0,0,0,1,1,  
1,1,1,1,1,1
```

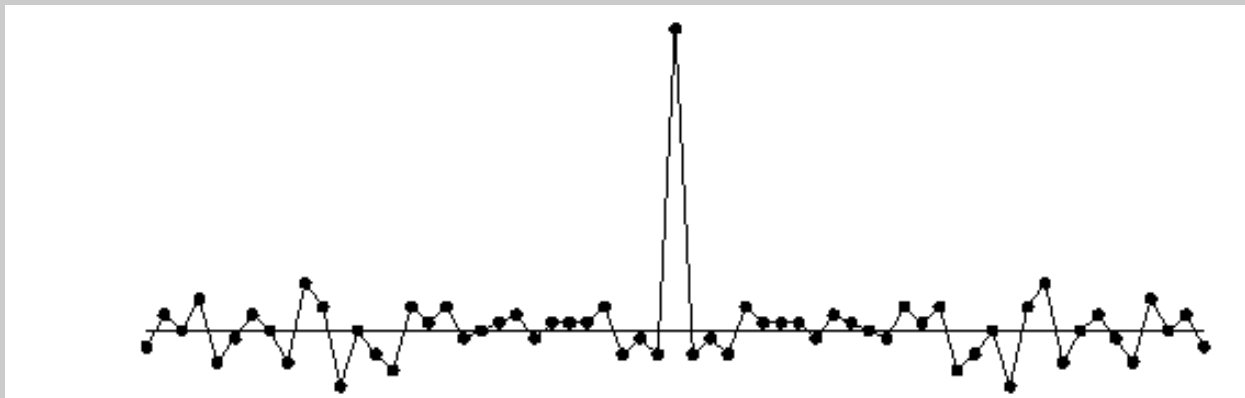
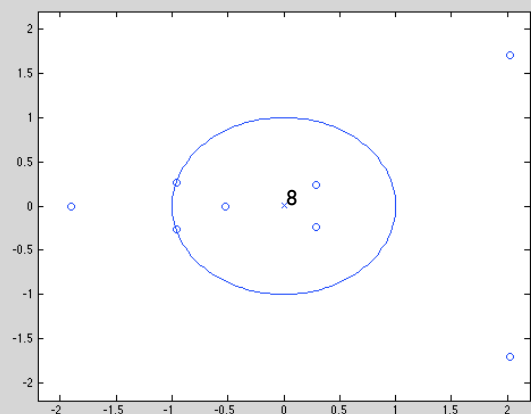
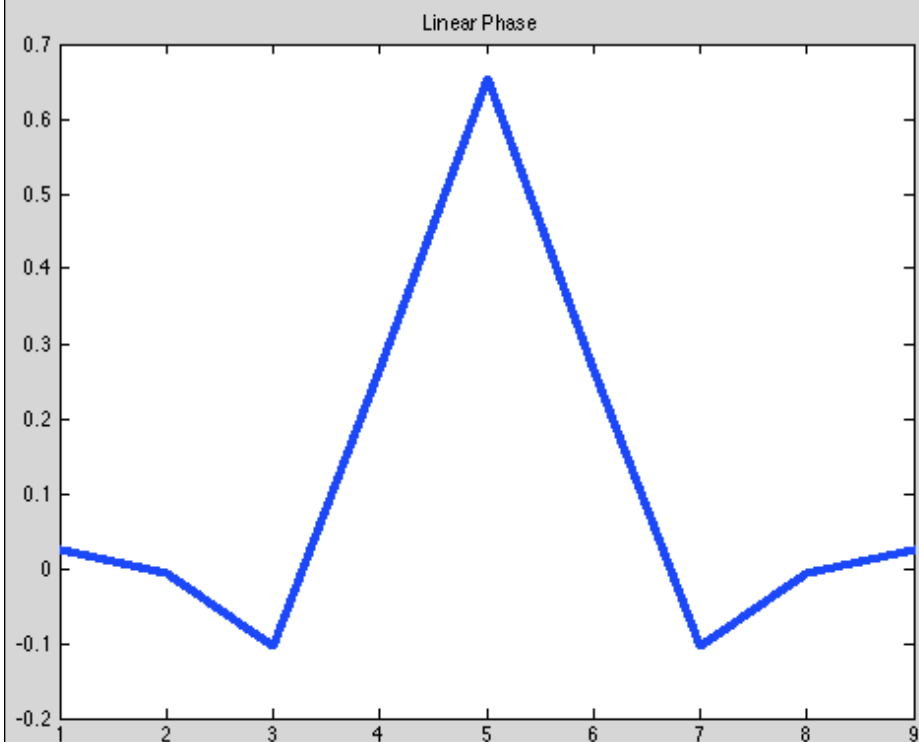


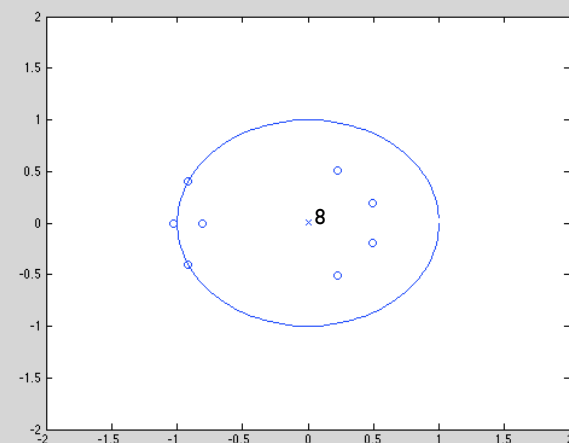
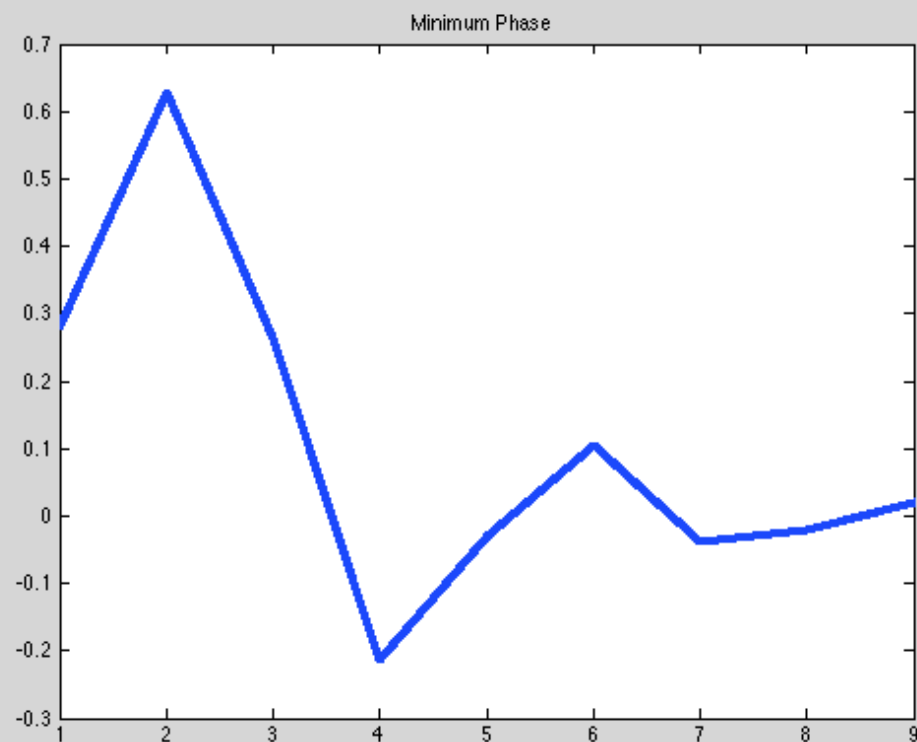
Fig. 3. – The pseudo-random sequence used in JT65 as a “synchronizing vector,” and a graphical representation of its autocorrelation function. The isolated central correlation spike serves to synchronize time and frequency between transmitting and receiving stations.

Minimum-phase VS Linear Phase

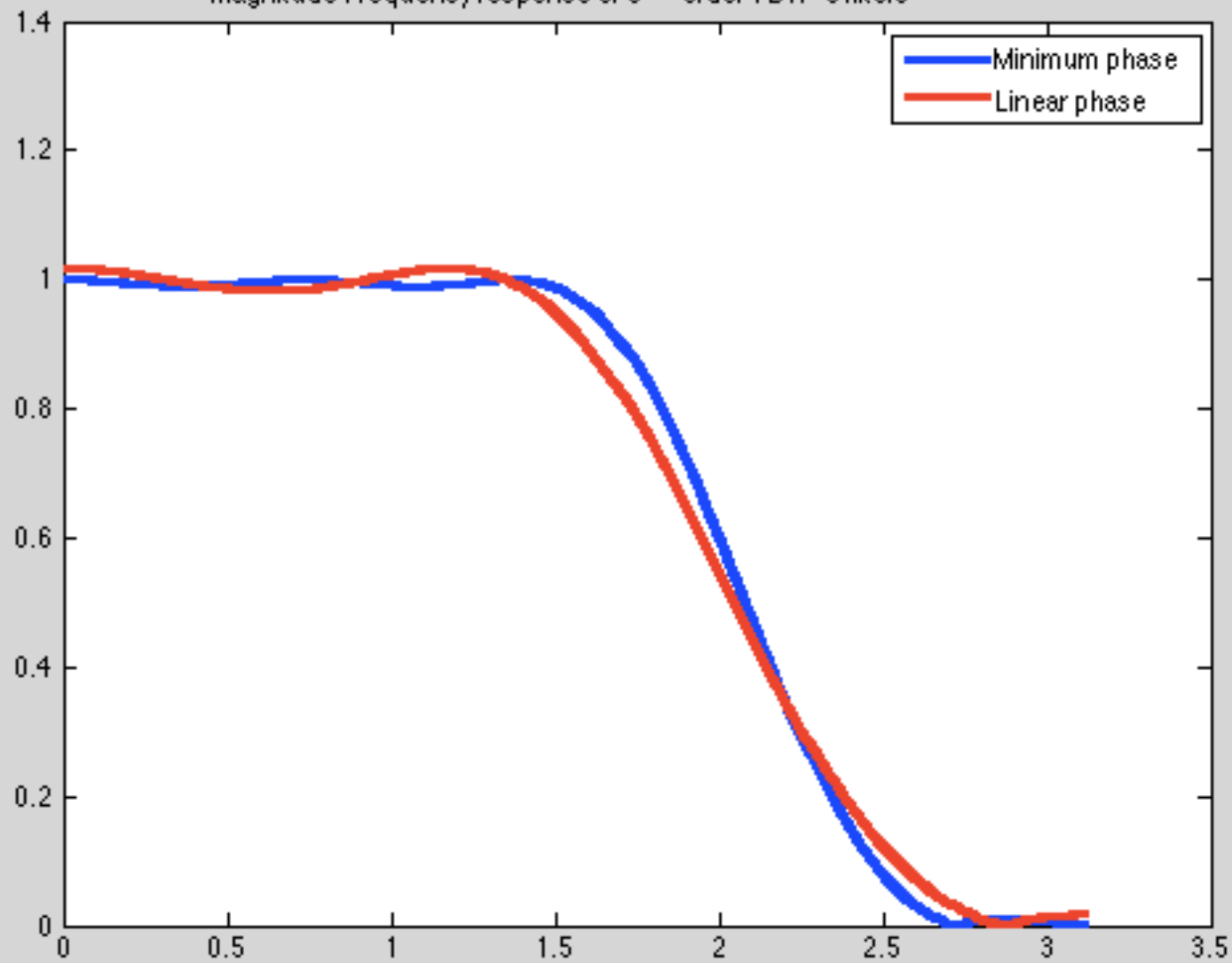
linear phase



minimum phase



Magnitude Frequency response of 9th order TBW=6 filters



Generalized linear-phase systems

$$H(e^{j\omega}) = \underbrace{A(e^{j\omega})}_{\text{Real, allow sign change}} e^{-j\alpha\omega + j\beta}$$

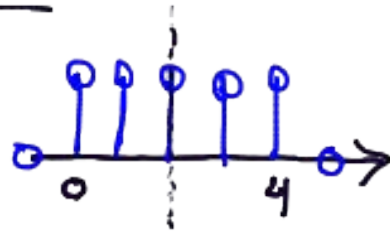
$$\text{grad}[H(e^{j\omega})] = \alpha \left(\begin{array}{l} \text{except when} \\ A(e^{j\omega}) \text{ changes} \\ \text{sign} \end{array} \right)$$

GLP for FIR \rightarrow MUST have symmetry

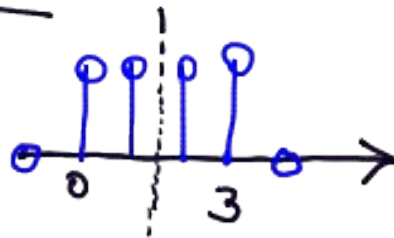
④

$$h[n] = h[M-n]:$$

Type I (M even)



Type II (M odd)

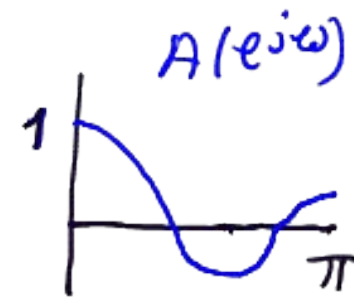
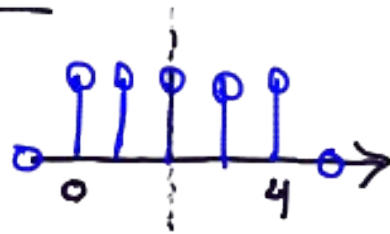


GLP for FIR \rightarrow MUST have symmetry

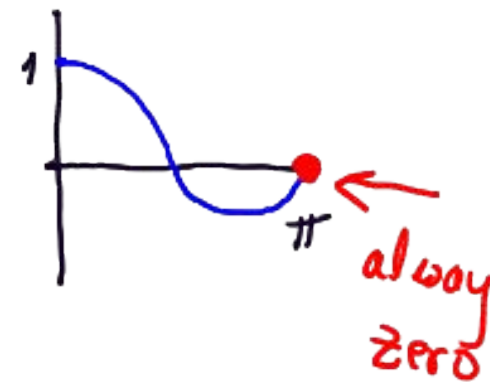
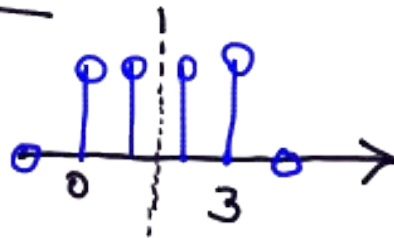
(4)

$$h[n] = h[M-n]:$$

Type I (M even)



Type II (M odd)

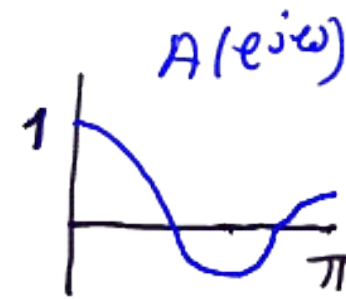
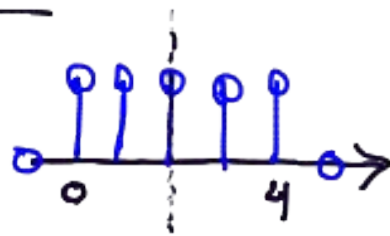


GLP for FIR \rightarrow MUST have symmetry

(4)

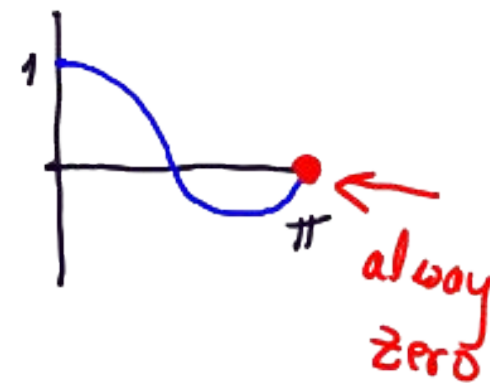
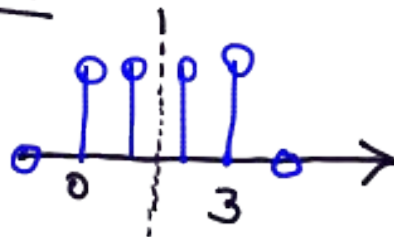
$$h[n] = h[M-n]:$$

Type I (M even)



$$A(e^{j\omega}) = h[\frac{M}{2}] + 2 \sum_{k=1}^{\frac{M}{2}} h[\frac{M}{2} - k] \cos(\omega k)$$

Type II (M odd)



$$A(e^{j\omega}) = \text{In the text}$$

Least Squares

$$\operatorname{argmin}_{\tilde{h}} \quad ||A\tilde{h} - b||^2$$

Solution:

$$\tilde{h} = (A^* A)^{-1} A^* b$$

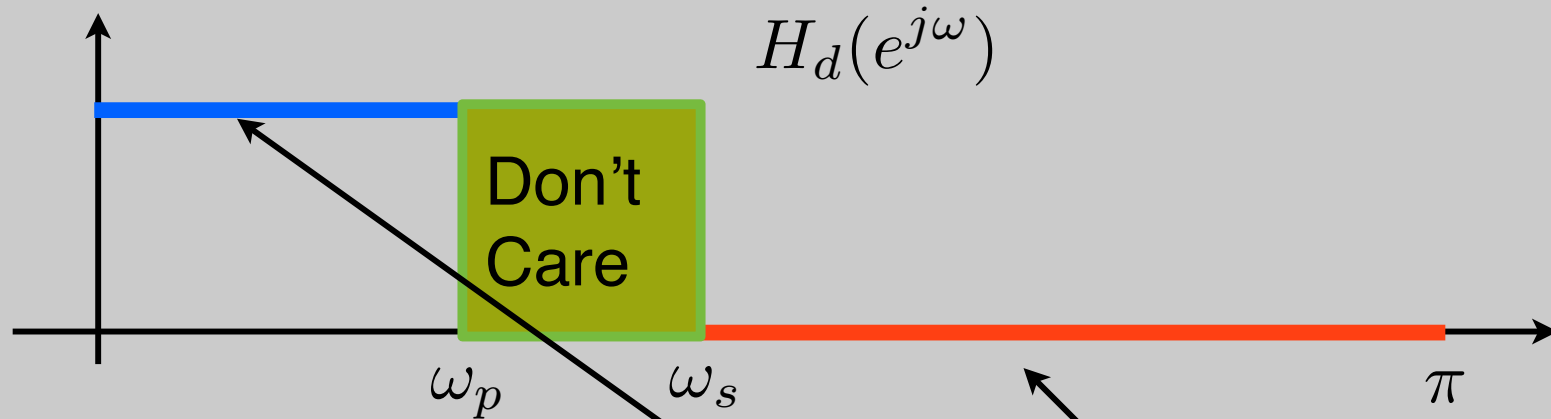
- Result will generally be non-symmetric and complex valued.
- However, if $\tilde{H}(e^{j\omega})$ is real, $\tilde{h}[n]$ should have symmetry!

Design of Linear-Phase L.P Filter

- Suppose:
 - $\tilde{H}(e^{j\omega})$ is real-symmetric
 - M is even ($M+1$ taps)
- Then:
 - $\tilde{h}[n]$ is real-symmetric around midpoint
- So:

$$\begin{aligned}\tilde{H}(e^{j\omega}) &= \tilde{h}[0] + \tilde{h}[1]e^{-j\omega} + \tilde{h}[-1]e^{+j\omega} \\ &\quad + \tilde{h}[2]e^{-j2\omega} + \tilde{h}[-2]e^{+j2\omega} \dots \\ &= \tilde{h}[0] + 2\cos(\omega)\tilde{h}[1] + 2\cos(2\omega)\tilde{h}[2] + \dots\end{aligned}$$

Least-Squares Linear-Phase Filter



Given M , ω_P , ω_s find the best LS filter:

$$A = \begin{bmatrix} 1 & \cdots & 2 \cos\left(\frac{M}{2}\omega_1\right) \\ \vdots & & \\ 1 & \cdots & 2 \cos\left(\frac{M}{2}\omega_p\right) \\ 1 & \cdots & 2 \cos\left(\frac{M}{2}\omega_s\right) \\ \vdots & & \\ 1 & \cdots & 2 \cos\left(\frac{M}{2}\omega_P\right) \end{bmatrix}$$

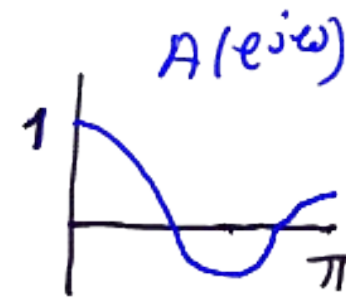
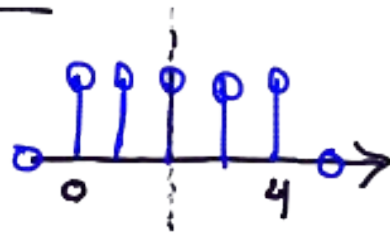
$$b = [1, 1, \cdots, 1, 0, 0, \cdots, 0]^T$$

GLP for FIR \rightarrow MUST have symmetry

(4)

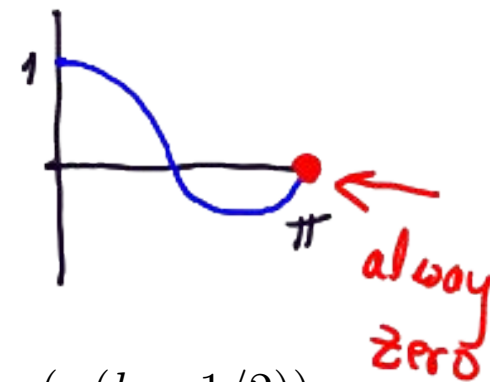
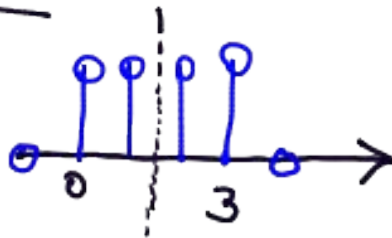
$$h[n] = h[M-n]:$$

Type I (M even)



$$A(e^{j\omega}) = h\left[\frac{M}{2}\right] + 2 \sum_{k=1}^{\frac{M}{2}} h\left[\frac{M}{2} - k\right] \cos(\omega k)$$

Type II (M odd)

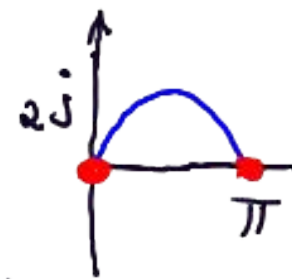
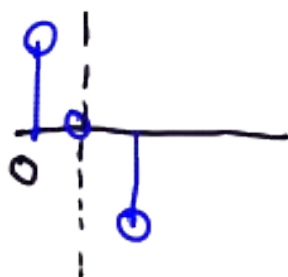


$$A(e^{j\omega}) = \sum_{k=1}^{(M+1)/2} 2h[(M+1)/2 - k] \cos(\omega(k - 1/2))$$

$$h[n] = -h[M-n]$$

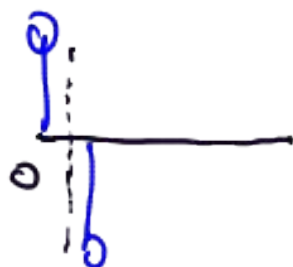
⑤

Type III (M even)



$$A(e^{j\omega}) = j 2 \sum_{k=1}^{M/2} h[\frac{M}{2}-k] \sin(\omega k)$$

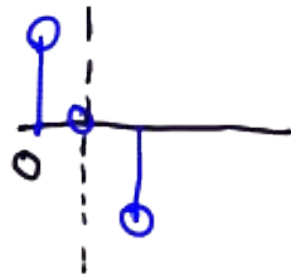
Type IV (M odd)



$$h[n] = -h[M-n]$$

⑤

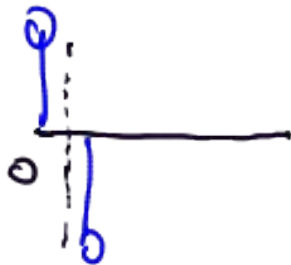
Type III (M even)



$$A(e^{j\omega}) = j 2 \sum_{k=1}^{M/2} h[\frac{M}{2}-k] \sin(\omega k)$$



Type IV (M odd)



$$A(e^{j\omega}) = \text{see text}$$



Zeros of GLP system

⑥

Type I, II: $h[n] = h[n - M]$

$$H(z) = \sum_{n=0}^M h[n] z^{-n} =$$

Zeros of GLP system

⑥

Type I, II: $h[n] = h[n-M]$

$$H(z) = \sum_{n=0}^M h[n] z^{-n} =$$

$$= \sum_{n=0}^M h[M-n] z^{-n} =$$

Zeros of GLP system

⑥

Type I, II: $h[n] = h[n-M]$

$$H(z) = \sum_{n=0}^M h[n] z^{-n} =$$

$$= \sum_{n=0}^M h[M-n] z^{-n} = z^{-M} \sum_{n=0}^M h[M-n] z^{M-n}$$

Zeros of GLP system

⑥

Type I, II: $h[n] = h[n-M]$

$$H(z) = \sum_{n=0}^M h[n] z^{-n} =$$

$$= \sum_{n=0}^M h[M-n] z^{-n} = z^{-M} \sum_{n=0}^M \underbrace{h[M-n]}_{\triangleq k} z^{\underbrace{M-n}_{\triangleq k}}$$

$$= z^{-M} \sum_{k=0}^M h[k] z^k$$

Zeros of GLP system

⑥

Type I, II: $h[n] = h[n-M]$

$$H(z) = \sum_{n=0}^M h[n] z^{-n} =$$

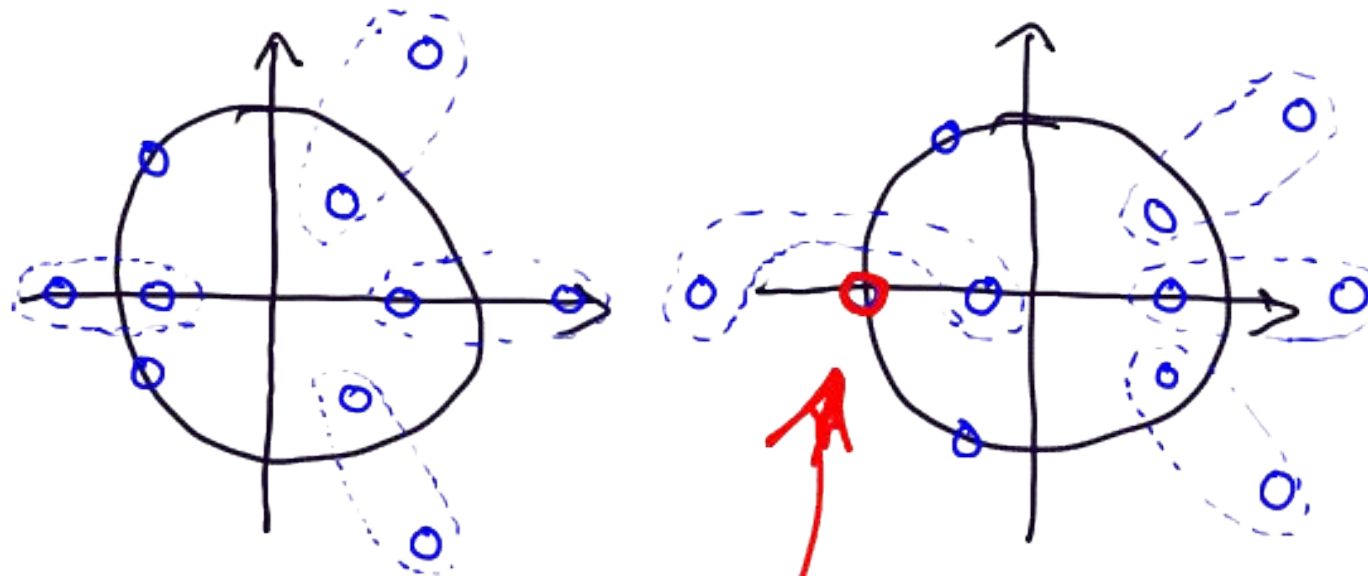
$$= \sum_{n=0}^M h[M-n] z^{-n} = z^{-M} \sum_{n=0}^M \underbrace{h[M-n]}_{\triangleq k} z^{\underbrace{M-n}_{\triangleq k}}$$

$$= z^{-M} \sum_{k=0}^M h[k] z^k$$

$$\Rightarrow \boxed{H(z) = z^{-M} H(z^{-1})}$$

$$H(z) = z^{-M} H(z^{-1}) \quad \text{Type I, II}$$

7



$$H(-1) = 0 \quad \text{Type II (Never high-pass)}$$

→ FOR GLP, IF $a = re^{j\theta}$ is a zero
 $\frac{1}{a^*}$ is also a zero

Zeros of GLP system

⑥

Type I, II: $h[n] = h[n-M]$

$$H(z) = \sum_{n=0}^M h[n] z^{-n} =$$

$$= \sum_{n=0}^M h[M-n] z^{-n} = z^{-M} \sum_{n=0}^M \underbrace{h[M-n]}_{\triangleq k} z^{\underbrace{M-n}_{\triangleq k}}$$

$$= z^{-M} \sum_{k=0}^M h[k] z^k$$

$$\Rightarrow \boxed{H(z) = z^{-M} H(z^{-1})}$$

for type II: $\overset{\text{odd}}{\text{pro}}$

$$H(-1) = (-1)^M H(-1) = -H(-1) \Rightarrow \boxed{H(-1) = 0}$$

similarly, can show for ⑧
type III, IV

$$H(z) = -z^{-M} H(z^{-1})$$

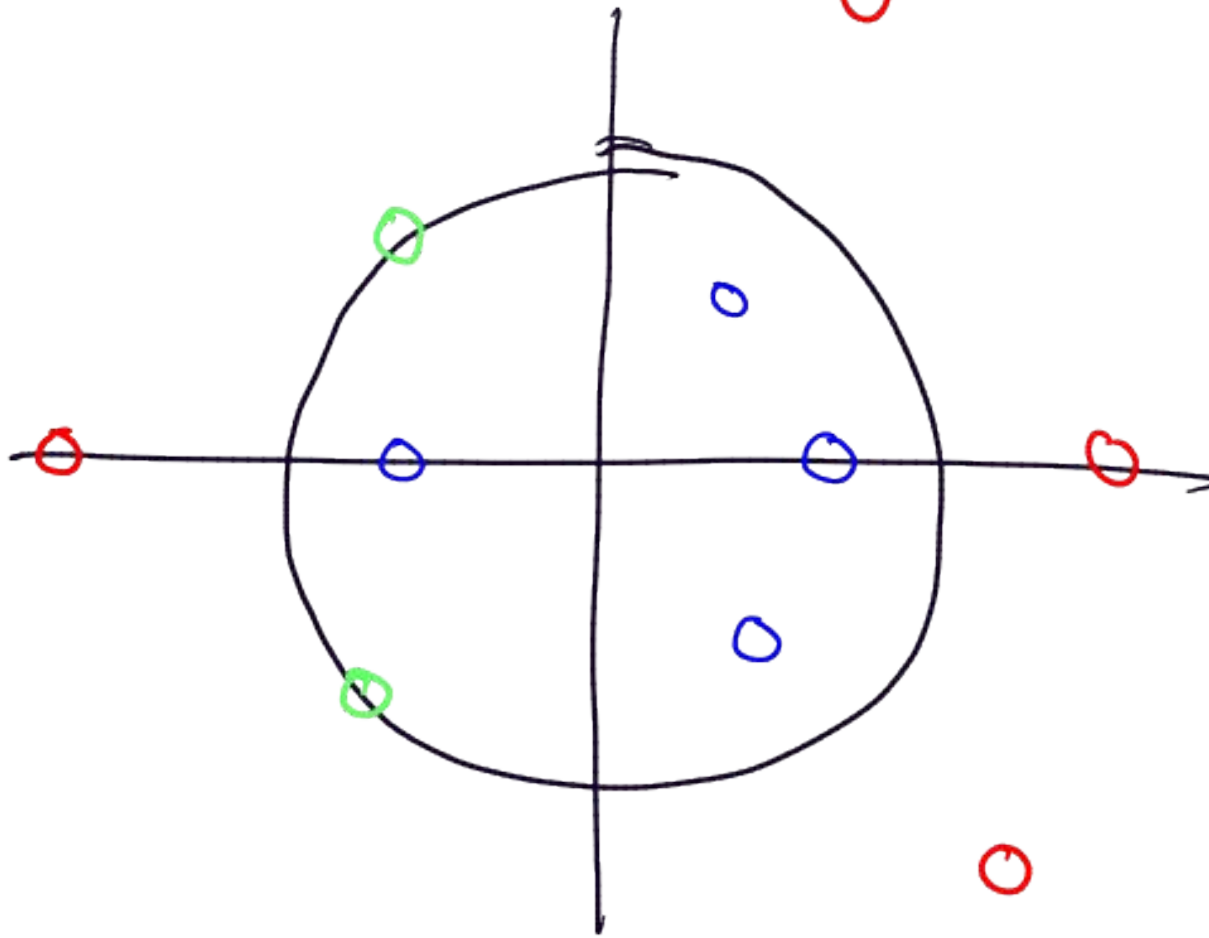
$$H(1) = 0 \rightarrow \text{Never low pass}$$

for type III

$$H(-1) = 0 \quad \text{only band pass}$$

Relation of FIR GLP to min-phase systems

⑨



$$H(z) = H_{\min}(z) H_{\max}(z) H_{uc}(z)$$

↑
minimum
phase

↑
maximum
phase