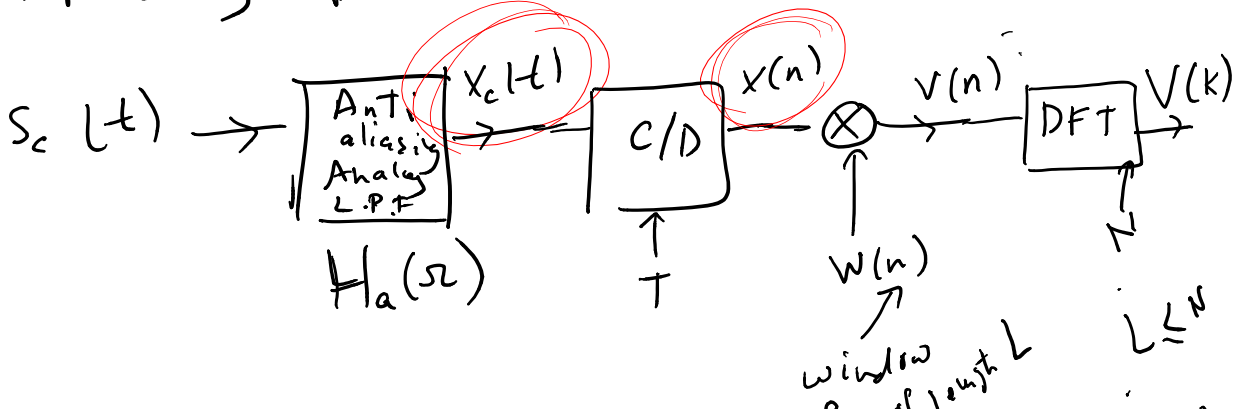


# Fourier Analysis of Signals using DFT

Applying DFT to continuous time signal.



$$X(\omega) = \text{DTFT} \{ x(n) \} = \frac{1}{T} \sum_{r=-\infty}^{+\infty} X_c \left( \frac{\omega}{T} + \frac{2\pi r}{T} \right)$$

$$v(n) = W(n) x(n)$$

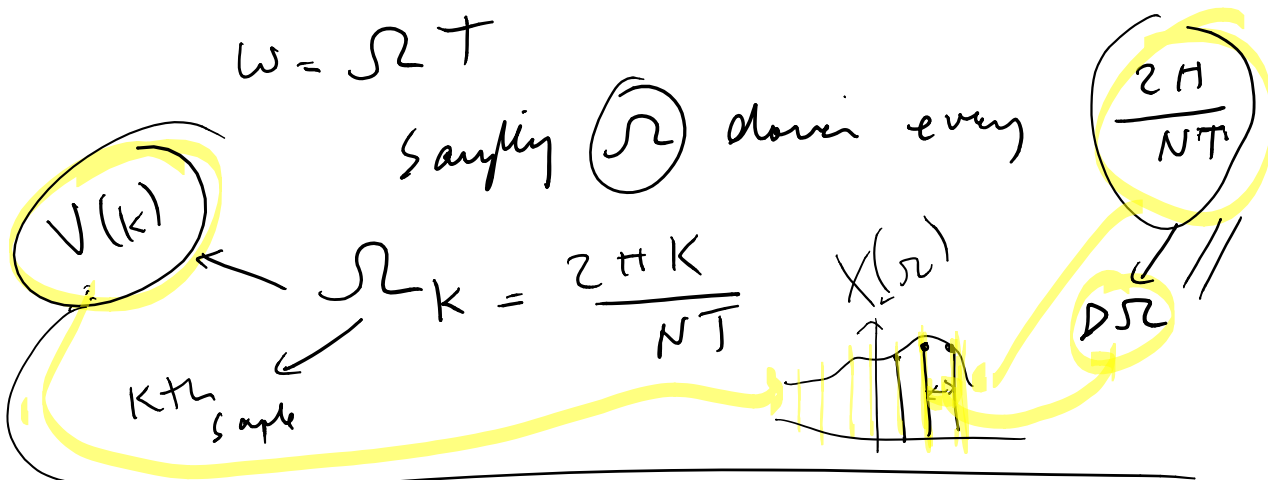
$$V(\omega) = W * X = \frac{1}{2\pi} \int_{-\pi}^{+\pi} X(\theta) W(\omega - \theta) d\omega$$

$$V(k) = \sum_{n=0}^{N-1} v(n) e^{-j2\pi n k / N}$$

$$V(k) = \left[ V(\omega) \right]_{\omega = \frac{2\pi k}{N}} \quad \text{Sampling } \omega \text{ every } \left( \frac{2\pi}{N} \right)$$

$$\omega = \Omega T$$

Sampling  $\Omega$  down every



$KTH_{\text{sample}}$

EX  $X_c(t)$  bandlimited  $X_c(\Omega) = 0$   
for  $|\Omega| > 2\pi \cdot 2500$

- Assume ideal anti-aliasing
- sample rate Nyquist  $\Rightarrow \frac{1}{T} = 5000$  sample/sec
- Want DFT sample of  $V(k)$  to represent  $X_c(\Omega)$  at 10 Hz every  $2\pi \cdot 10$  rad/s

$$\Delta\Omega = \frac{2\pi}{NT} = 2\pi \cdot 10 = \frac{2\pi}{NT} \Rightarrow$$

$$T = \frac{1}{5000}$$

$$2\pi \cdot 10 = \frac{2\pi}{N \cdot \frac{1}{5000}} \Rightarrow$$

$$N = 500 \Rightarrow N' = 512$$

### DFT Analysis of Sinusoidal Signals

$$S_c(t) = A_0 \cos(\Omega_0 t + \theta_0) + A_1 \cos(\Omega_1 t + \theta_1)$$

Identify samples

$$X(n) = A_0 \cos(\omega_0 n + \theta_0) + A_1 \cos(\omega_1 n + \theta_1)$$

$$\omega_0 = \Omega_0 T \quad \omega_1 = \Omega_1 T$$

$$V(n) = X(n) W(n)$$

$$v(n) = x(n) w(n)$$

$$v(n) = A_0 w(n) \cos(\omega_0 n + \theta_0) + A_1 w(n) \cos(\omega_1 n + \theta_1)$$

$$= \frac{A_0}{2} w(n) e^{j\theta_0} e^{j\omega_0 n} + \frac{A_0}{2} w(n) e^{-j\theta_0} e^{-j\omega_0 n}$$

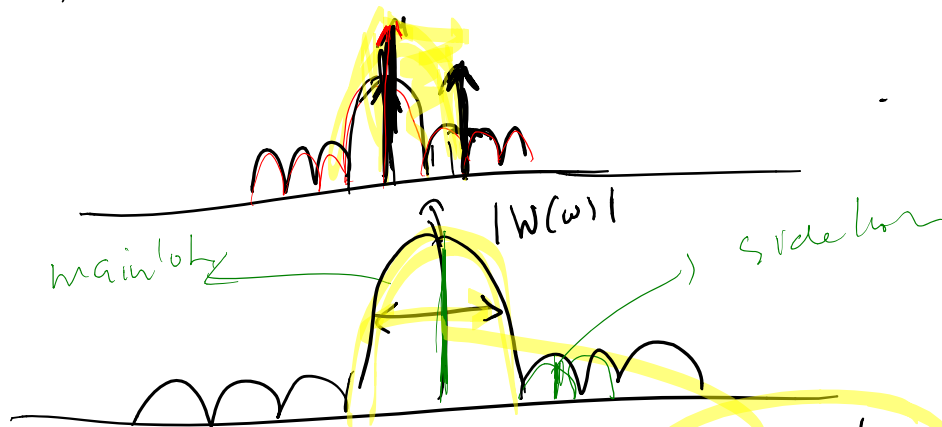
$$+ \frac{A_1}{2} w(n) e^{j\theta_1} e^{j\omega_1 n} + \frac{A_1}{2} w(n) e^{-j\theta_1} e^{-j\omega_1 n}$$

$$V(\omega) = \frac{A_0}{2} e^{j\theta_0} W(\omega - \omega_0) + \frac{A_0}{2} e^{-j\theta_0} W(\omega + \omega_0)$$

$$+ \frac{A_1}{2} e^{j\theta_1} W(\omega - \omega_1) + \frac{A_1}{2} e^{-j\theta_1} W(\omega + \omega_1)$$

ex  $\frac{1}{T} = 16 \text{ kHz}$   $w(n)$  has length  $L = 64$   
 $A_0 = 1$   $A_1 = 0.75$   $\theta_0 = \theta_1 = 0$

## Properties of Windows



Resolution: Width of the main lobe

Leakage: relative amplitude of main lobe to side lobe

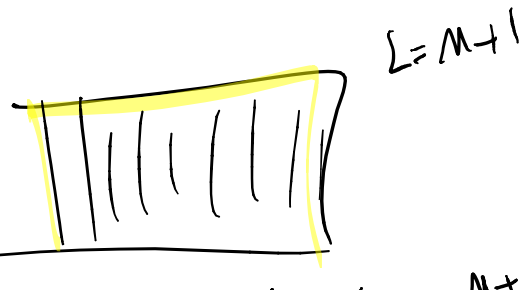
Rectangular  $w(n) = \begin{cases} 1 & 0 \leq n \leq M \\ 0 & \text{elsewhere} \end{cases}$

Rectangular

$$w(n) = \begin{cases} 1 & 0 \leq n \leq M \\ 0 & \text{elsewhere} \end{cases}$$

$$0 \leq n \leq M$$

elsewhere



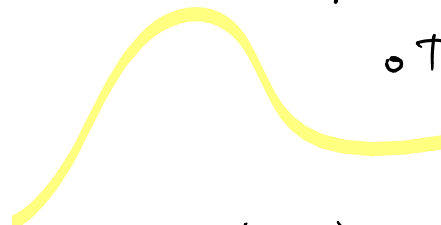
Bartlett

$$w(n) = \begin{cases} \frac{2n}{M} & 0 \leq n \leq M/2 \\ 2 - \frac{2n}{M} & M/2 \leq n \leq M \end{cases}$$



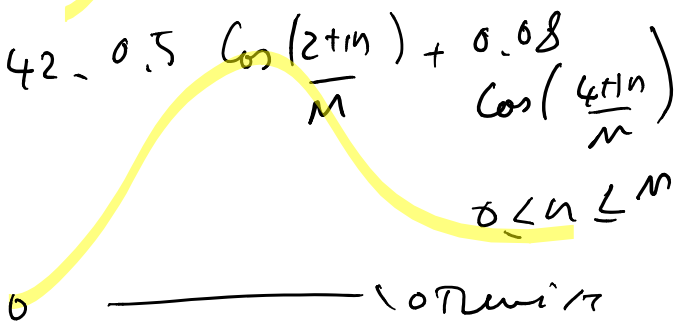
Hanning Window

$$w(n) = \begin{cases} 0.54 - 0.46 \cos\left(\frac{2\pi n}{M}\right) & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$



Blackman Window

$$w(n) = \begin{cases} 0.42 - 0.5 \cos\left(\frac{2\pi n}{M}\right) + 0.08 \cos\left(\frac{4\pi n}{M}\right) & 0 \leq n \leq M \\ 0 & \text{otherwise} \end{cases}$$



Kaiser Window

$$w(n) = \frac{I_0 \left[ \beta \sqrt{1 - \left[ \frac{n-d}{L} \right]^2} \right]}{I_0(\beta)}$$

$0 \leq n \leq M$

$$I_0(\beta)$$

otherwise

$$\alpha = \frac{M}{2}$$

$M+1 = L = \text{length of wire}$

$I_0(\cdot)$  is zeroth order modified Bessel fn of first kind.

$$I_0(x) = 1 + \frac{x^2}{2^2 (1!)^2} + \frac{x^4}{2^4 (2!)^2} + \frac{x^6}{2^6 (3!)^2} + \dots$$

$I_n(x)$  nth order modified Bessel fn of 1st kind  
soln to

$$x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} - (x^2 + n^2) y = 0$$

$\beta$  → affects shape of main lobe  
Trade off between main lobe width  
against side lobe ampl. and using  $\beta$ .

$A_{sl}$  = ratio in dB of amplitude of main lobe to the amplitude of side lobe

$$A_{sl} < 13.26$$

$$\beta = 0.76609 (A_{sl} - 13.26)^{0.4} + 0.07834 (A_{sl} - 13.26)$$

∴  $A_{sl} < A_{sl} < 60$

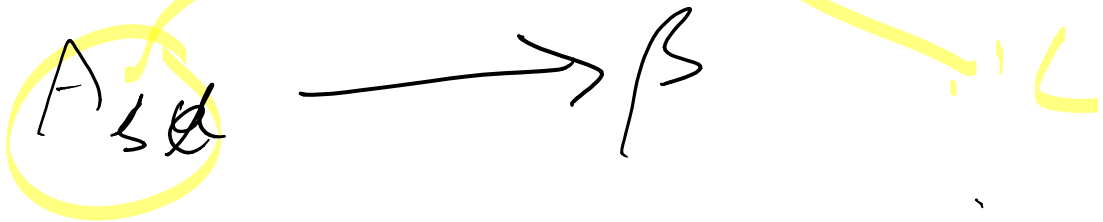
(1751 - 13.26)

$$13.26 < A_{SI} < 60$$

$$0.2439(A_{SI} + 6.3) \quad 60dB < A_{SI} < 120$$

$\Delta m l$  = main lobe width

$$L \approx \frac{24 \pi (A_{SI} + 12)}{155 \Delta m l} + 1$$



Time dependent Fourier Transform  
Short Term Fourier Transform STFT

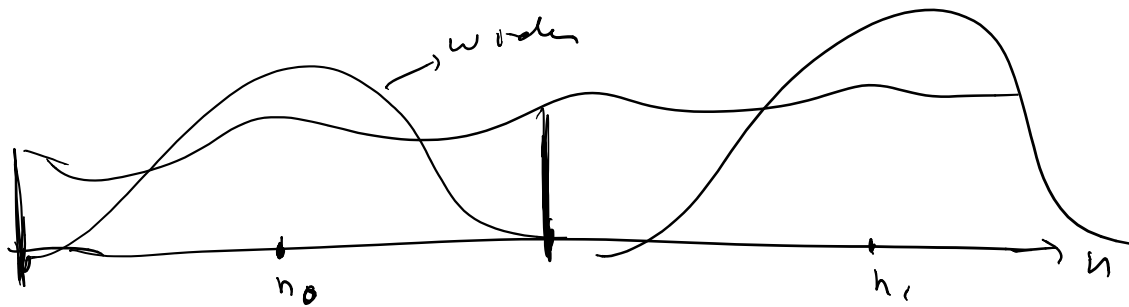
long window  $\rightarrow$  can resolve two close frequencies  
But no good in detecting point of change.

Freq. Content  
Real life signals vary over time  $\Rightarrow$  Non-stationary.

$X(n, \omega)$  S.T.F.T  $-j\omega m$

$$X(n, \omega) = \sum_{m=-\infty}^{+\infty} x(n+m) w(m) e^{-j\omega m}$$

$$\frac{1}{N} \sum_{m=0}^{N-1} x(n-m) e^{-j2\pi k m / N}$$



Ex  $x_c(t) = \cos(\theta(t)) = \cos(A \cdot t^2)$  linear chirp signal

Instantaneous freq =  $\Omega_i(t) = \frac{d}{dt}(\theta(t)) = 2A \cdot t$

$$x(n) = x_c(nT) = \cos(A \cdot T^2 n^2) = \cos(\alpha_0 n^2)$$

$$\alpha_0 = A \cdot T^2$$

Inst. freq  $\omega_i(n) = 2 \alpha_0 n$  linearly

Sampling in Time and in Freq:  $j \frac{2\pi k m}{N}$

$$X(n, k) = \sum_{m=0}^{L-1} x(n+m) w(m) e^{-j \frac{2\pi k m}{N}} \quad 0 \leq k < N$$

$$= x(n) * h_k(n)$$

$$h_k(n) = w(-n) e^{j \frac{2\pi k n}{N}} \quad \left. \begin{matrix} \downarrow \\ k=0, \dots, N-1 \end{matrix} \right\}$$

$$H_k(\omega) = W\left(\frac{2\pi k}{N} - \omega\right)$$

$$\left[ h_{k-1} \right] \quad \left[ \tilde{x}(n, N-1) \right]$$

