

CS 184: Foundations of Computer Graphics

Kinematics of Articulated Bodies

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Kinematics vs. dynamics

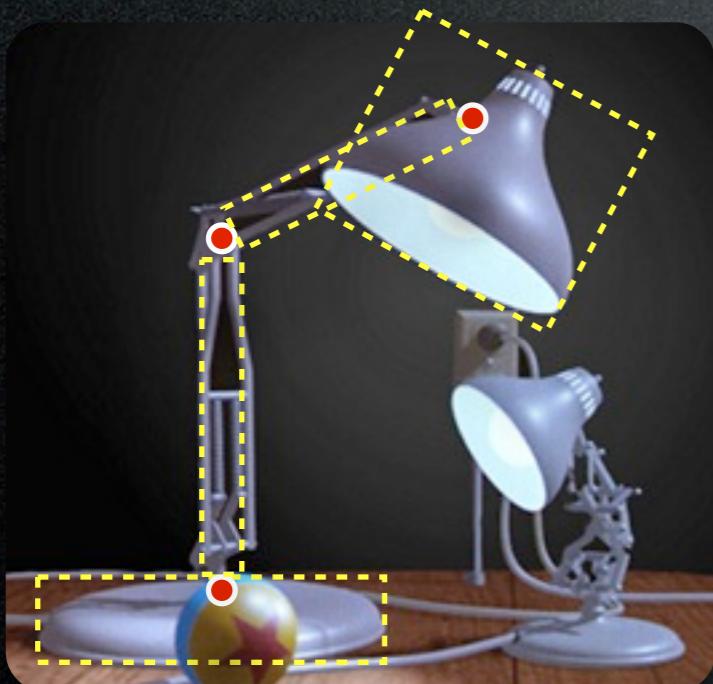
- Kinematics = motion but no forces
 - Keyframing, motion capture, etc.
- Dynamics = motion from forces
 - Simulation

If you want to know more about dynamics and simulation...

- Particles and rigid bodies:
 - Baraff and Witkin, “Physically Based Modeling”, 2001
- Deformable bodies:
 - James O’Brien’s CS 283 slides and readings on elastic simulation
- Fluids:
 - Bridson and Müller-Fischer, “Fluid Simulation for Computer Animation”, 2007

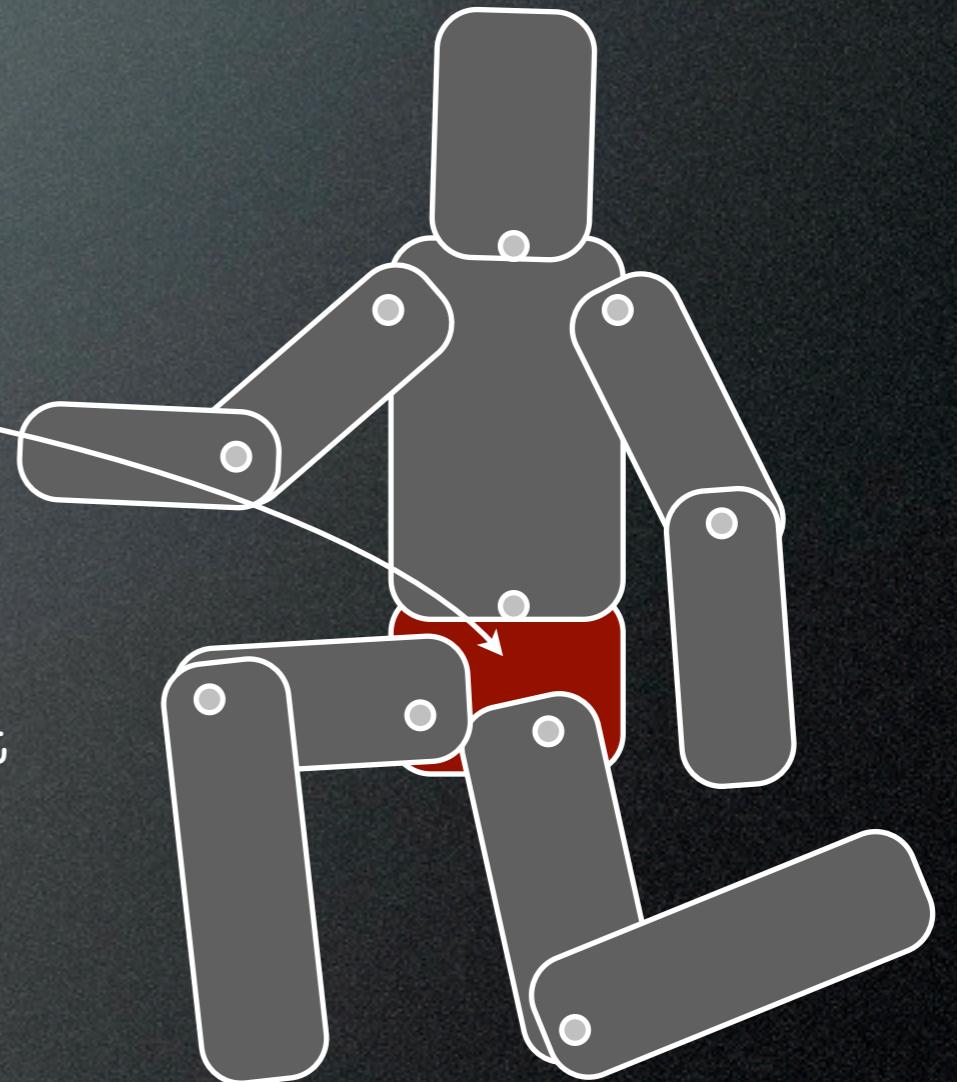
Articulated bodies

- Rigid bodies connected with joints
 - Topology (what's connected to what)
 - Geometric relations from joints
- Not necessarily what's displayed in the end



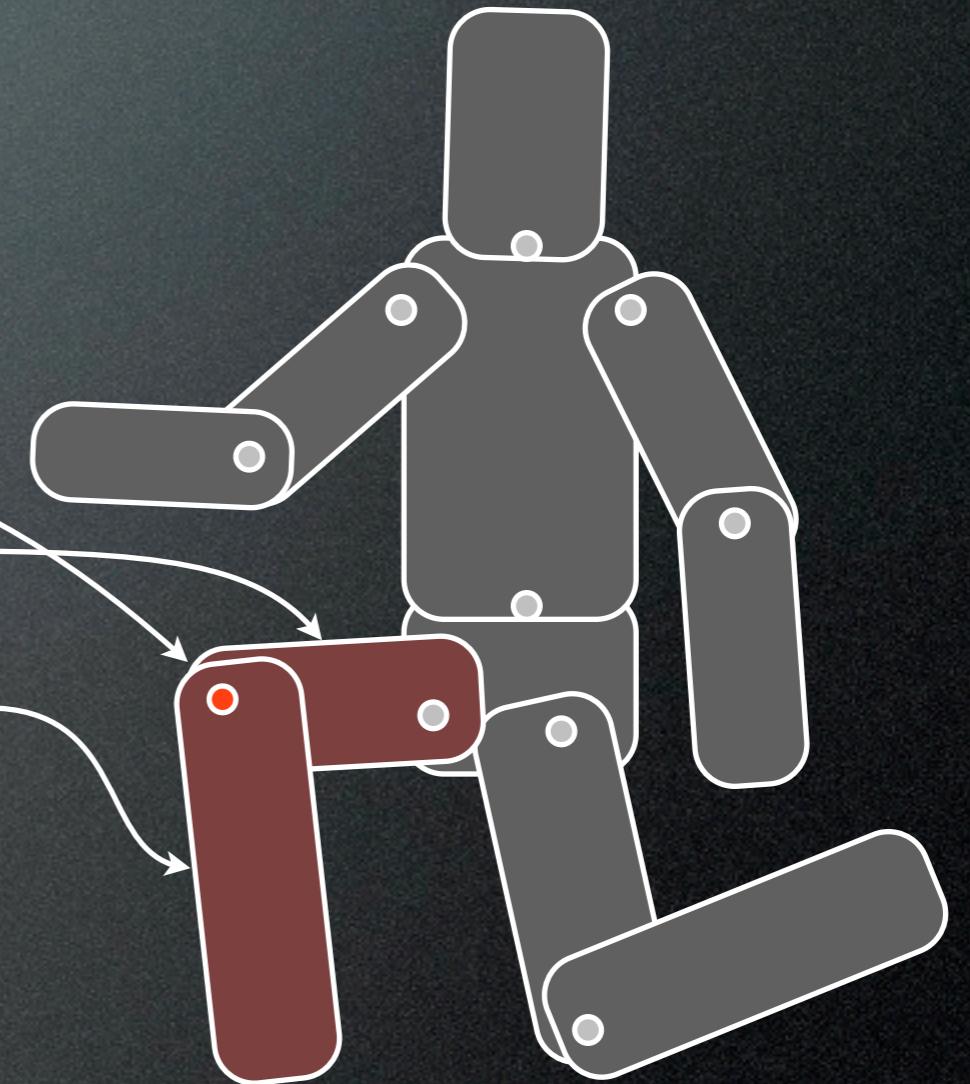
Articulated bodies

- Root body
 - Position and orientation set by “global” transformation
 - Other bodies move relative to root



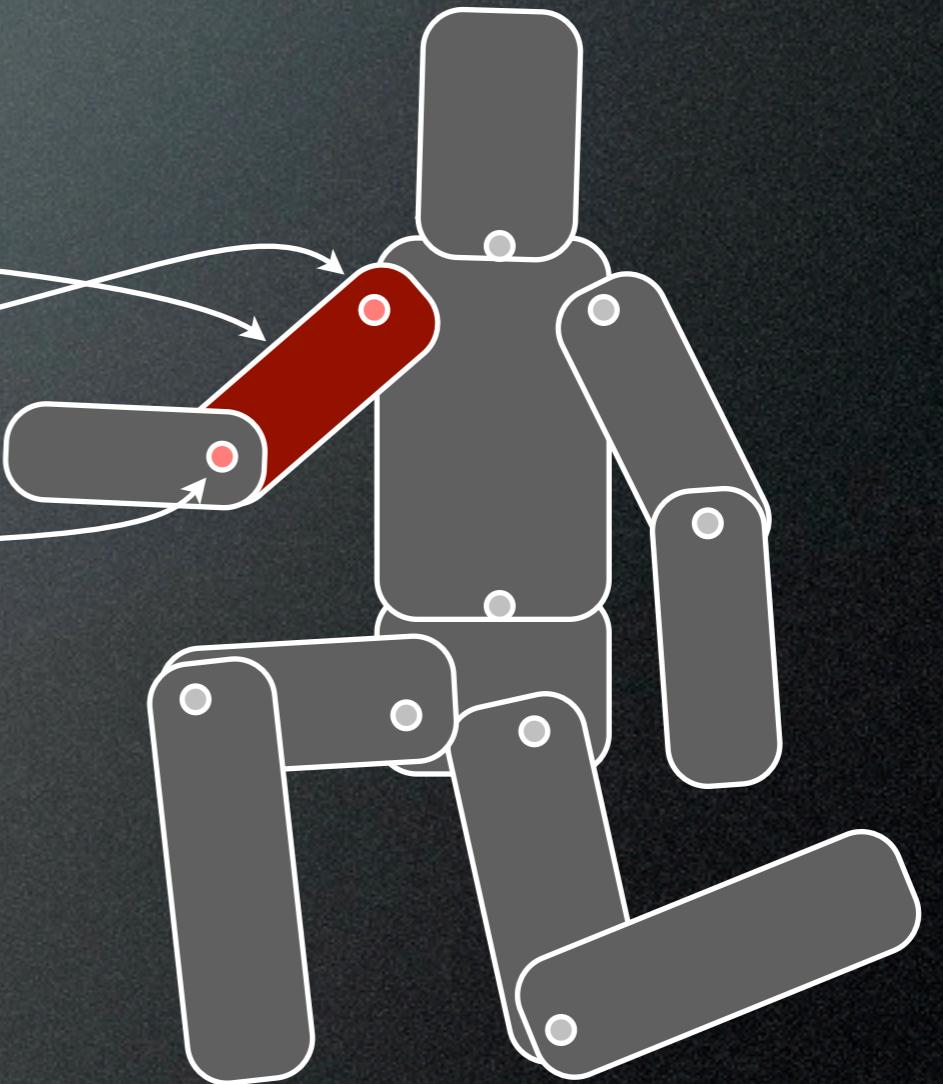
Articulated bodies

- A joint
 - Inboard body (towards root)
 - Outboard body (away from root)



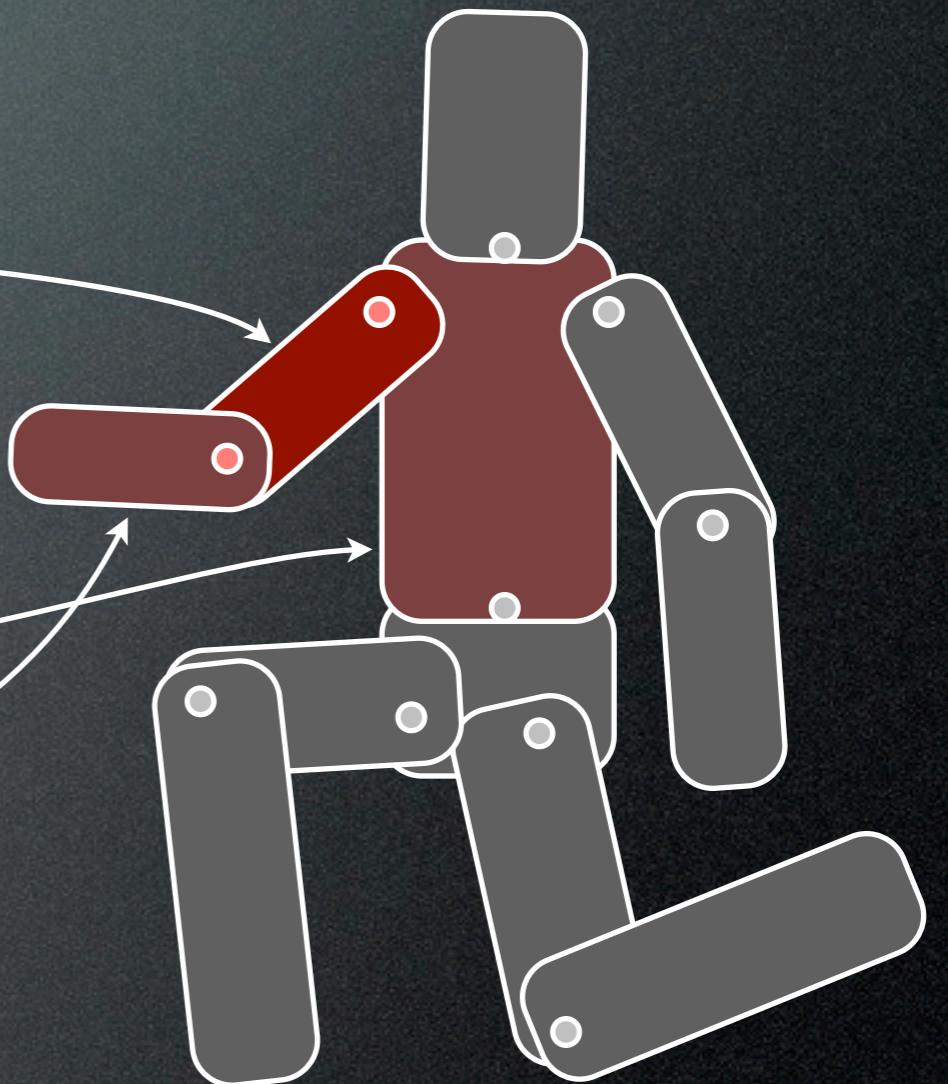
Articulated bodies

- A body —
- Inboard joint —
- Outboard joint(s) —
- Parent
- Child(ren)



Articulated bodies

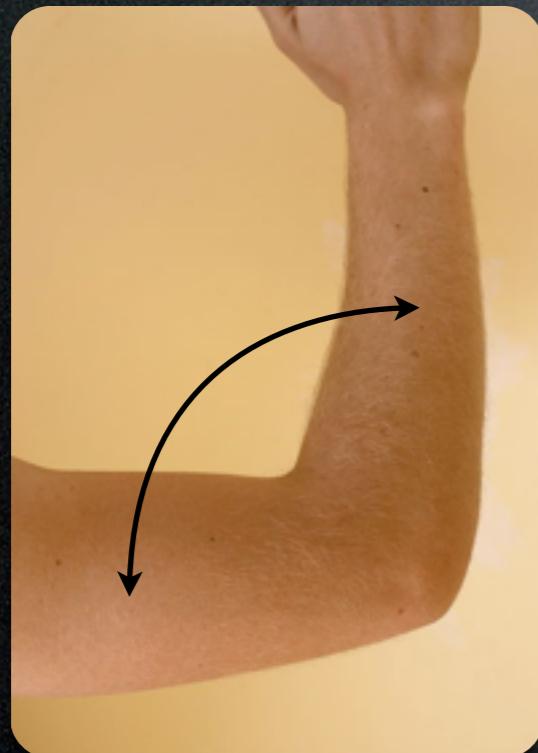
- A body —
 - Inboard joint
 - Outboard joint(s)
- Parent —
- Child(ren) —



Articulated bodies

- Interior joints are typically not 6 DOF

Pin joint:
rotation about one axis



Ball:
arbitrary rotation



Prism joint:
translation along one axis

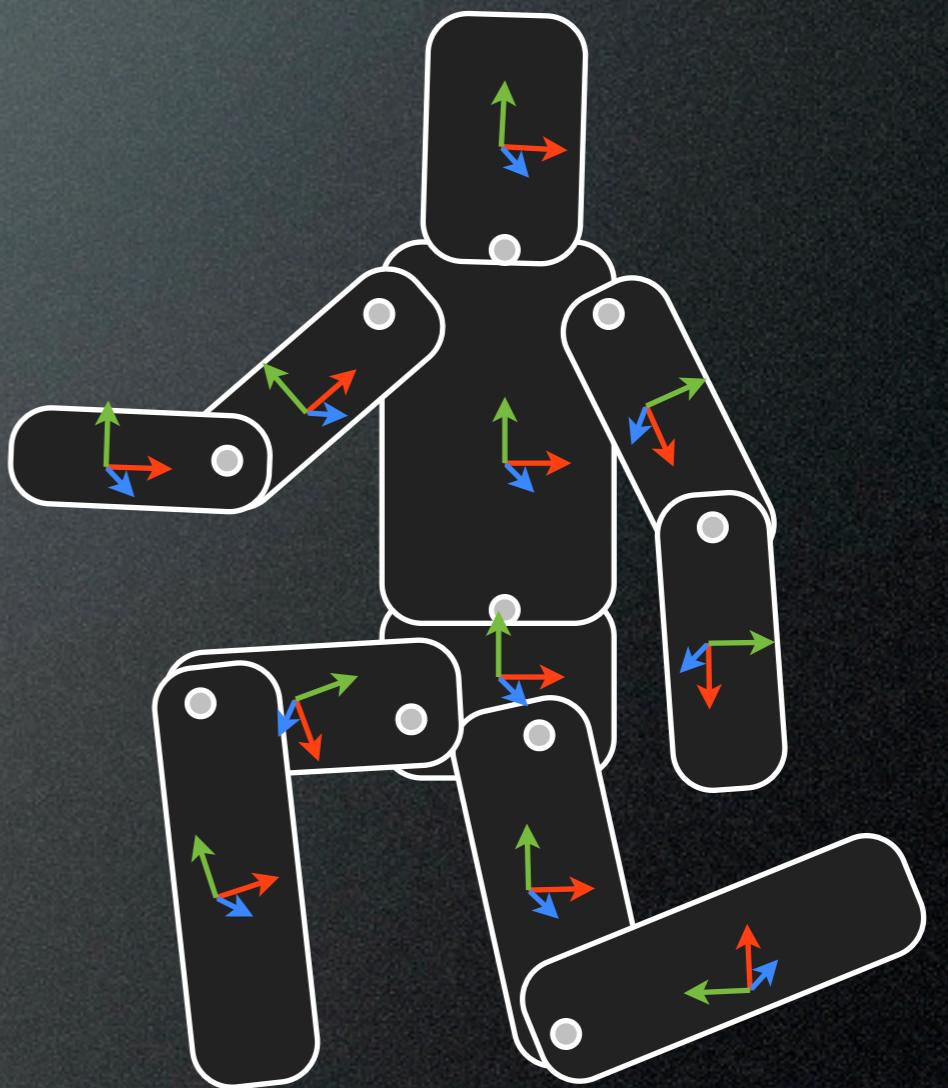


Forward and inverse kinematics

- Forward kinematics:
 - Given all the joint parameters, where are the bodies?
- Inverse kinematics:
 - Given where I want some body to be, what joint parameters do I need to set?

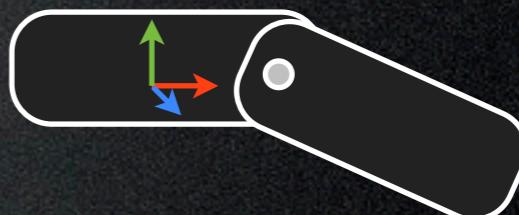
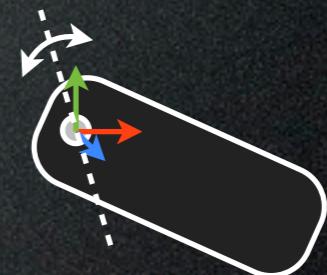
Forward kinematics

- Each body gets its own local coordinate system
 - Position of a vertex is fixed relative to local coordinate system
 - What is its position relative to world coordinates?



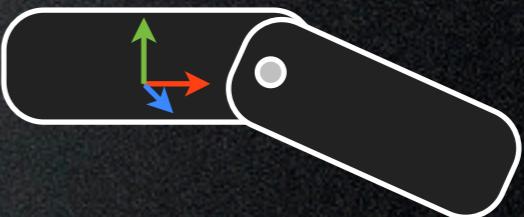
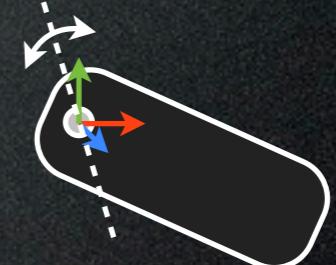
Forward kinematics

- Pin joints
 - Translate inboard joint to origin
 - Apply rotation about axis
 - Translate origin to location of outboard joint on parent body



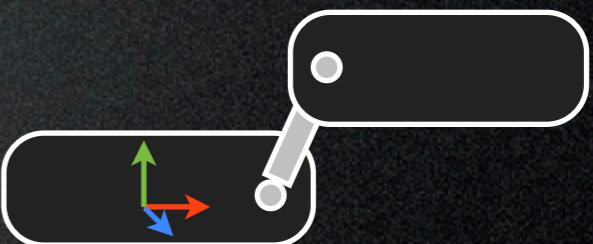
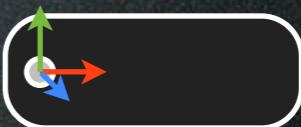
Forward kinematics

- Ball joints
 - Translate inboard joint to origin
 - Apply rotation about arbitrary axis
 - Translate origin to location of outboard joint on parent body



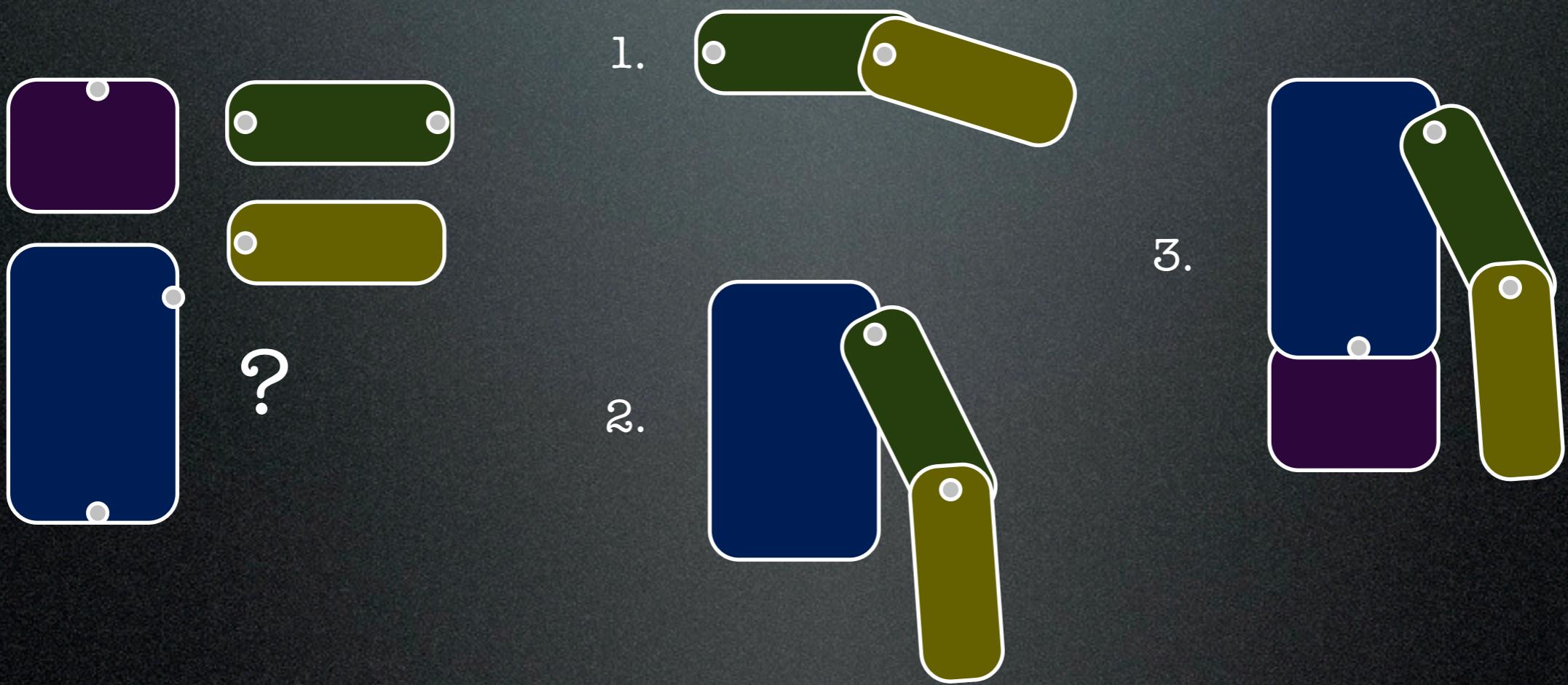
Forward kinematics

- Prism joints
 - Translate inboard joint to origin
 - Translate along axis
 - Translate origin to location of outboard joint on parent body



Forward kinematics

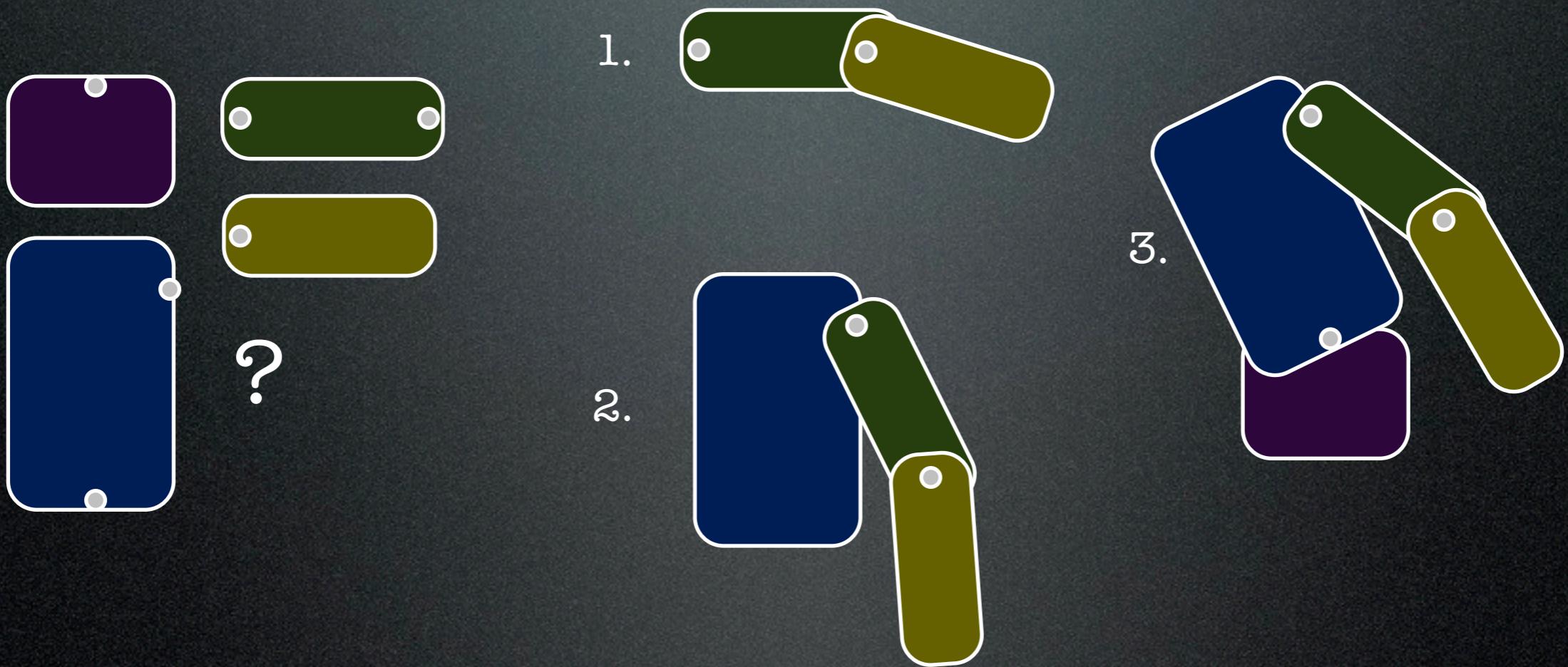
- Composite transformations up the hierarchy



- $\mathbf{M}_{\text{world} \leftarrow \text{forearm}} = \mathbf{M}_{\text{world} \leftarrow \text{hip}} \cdot \mathbf{M}_{\text{hip} \leftarrow \text{torso}} \cdot \mathbf{M}_{\text{torso} \leftarrow \text{upperarm}} \cdot \mathbf{M}_{\text{upperarm} \leftarrow \text{forearm}}$

Forward kinematics

- Composite transformations up the hierarchy



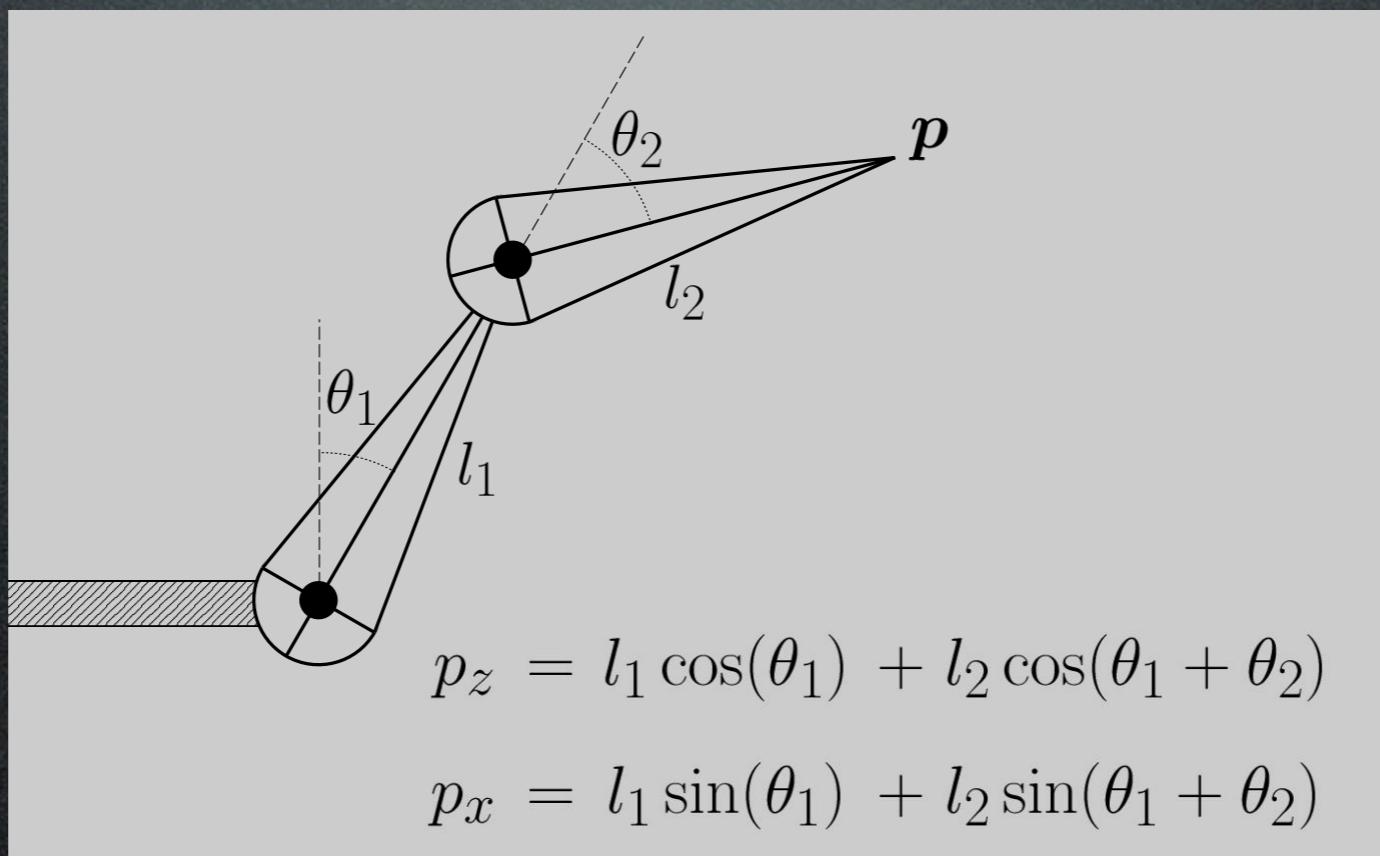
Inverse kinematics

- Given
 - Root transformation
 - Initial configuration
 - Desired location of end point
- Find
 - Internal parameter settings



Inverse kinematics

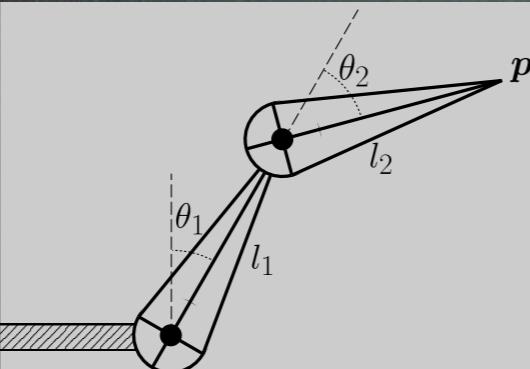
- A simple two segment arm in 2D



James O'Brien

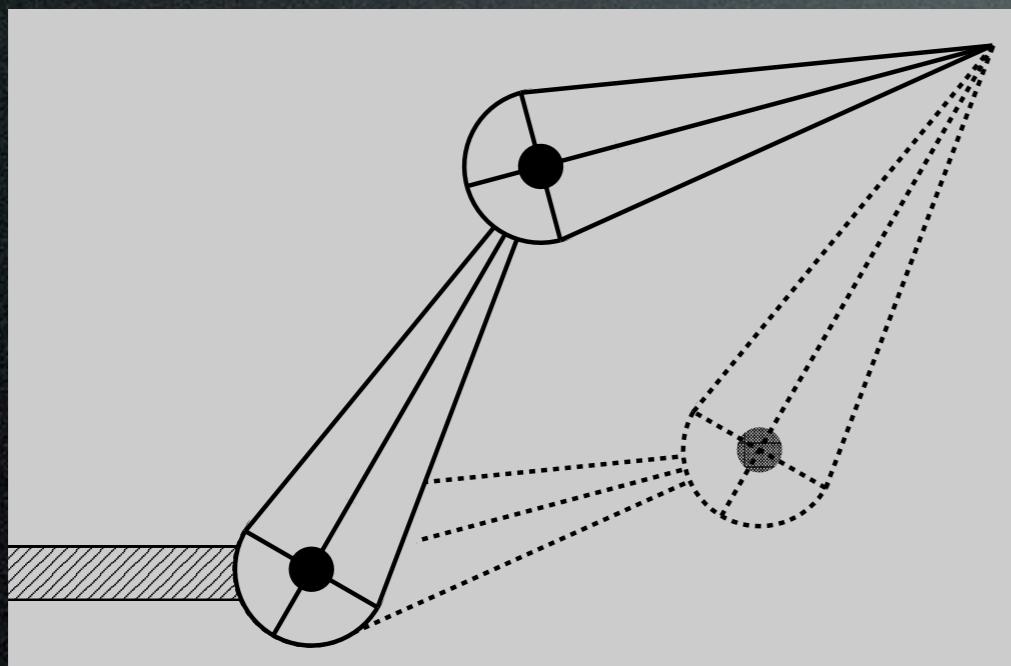
Direct IK

- Just solve for the parameters! What's the problem?

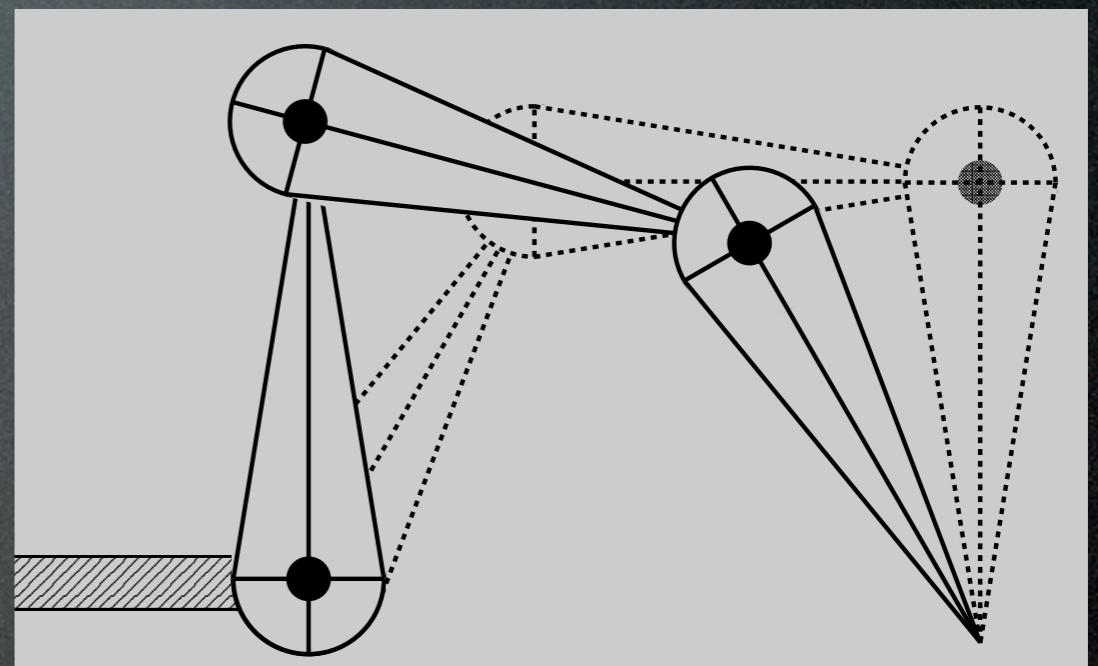

$$\theta_2 = \cos^{-1} \left(\frac{p_z^2 + p_x^2 - l_1^2 - l_2^2}{2l_1l_2} \right)$$
$$\theta_1 = \frac{-p_zl_2\sin(\theta_2) + p_x(l_1 + l_2\cos(\theta_2))}{p_xl_2\sin(\theta_2) + p_z(l_1 + l_2\cos(\theta_2))}$$

Why is this hard?

Multiple disconnected solutions

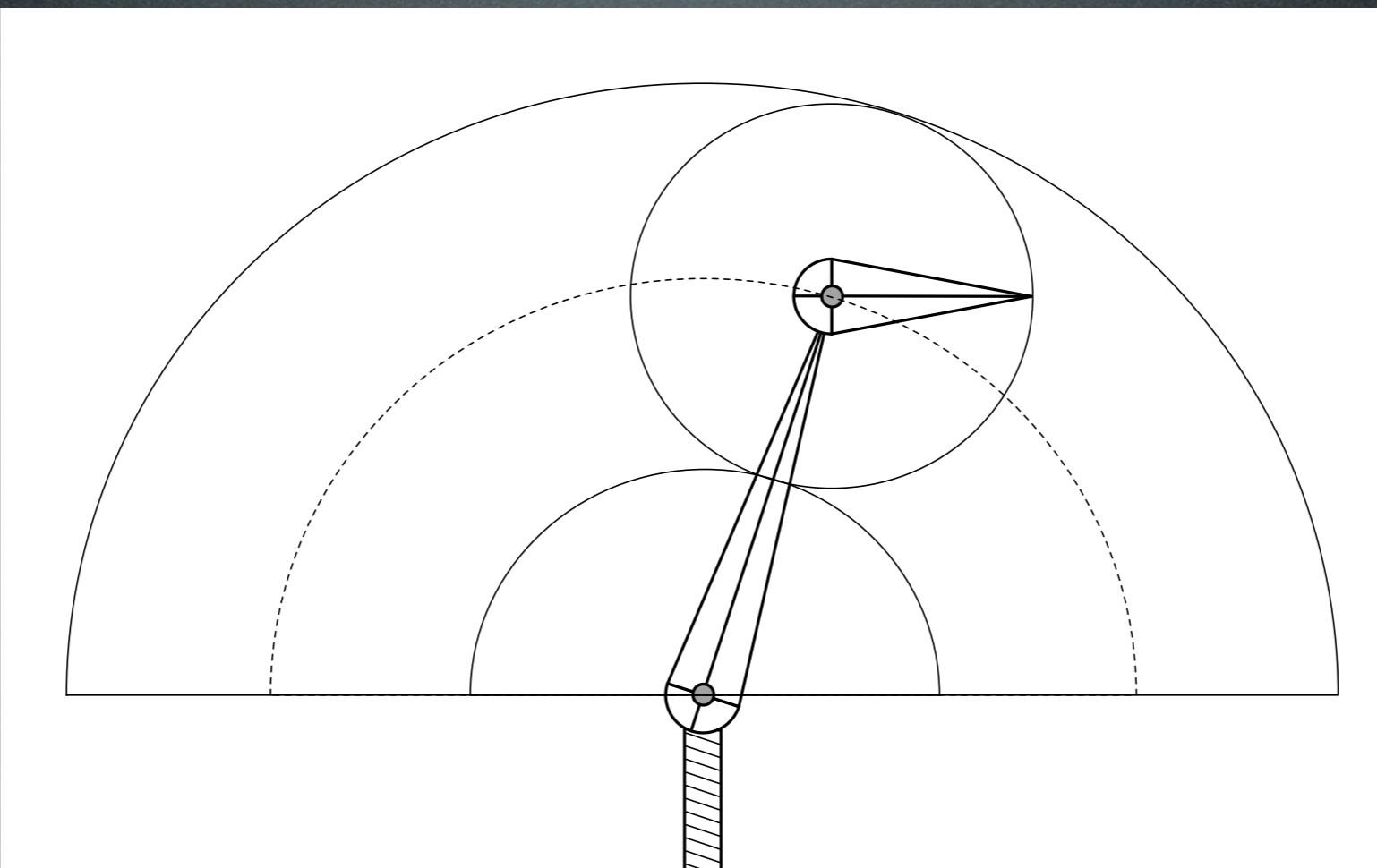


Multiple **connected** solutions



Why is this hard?

Solutions don't always exist

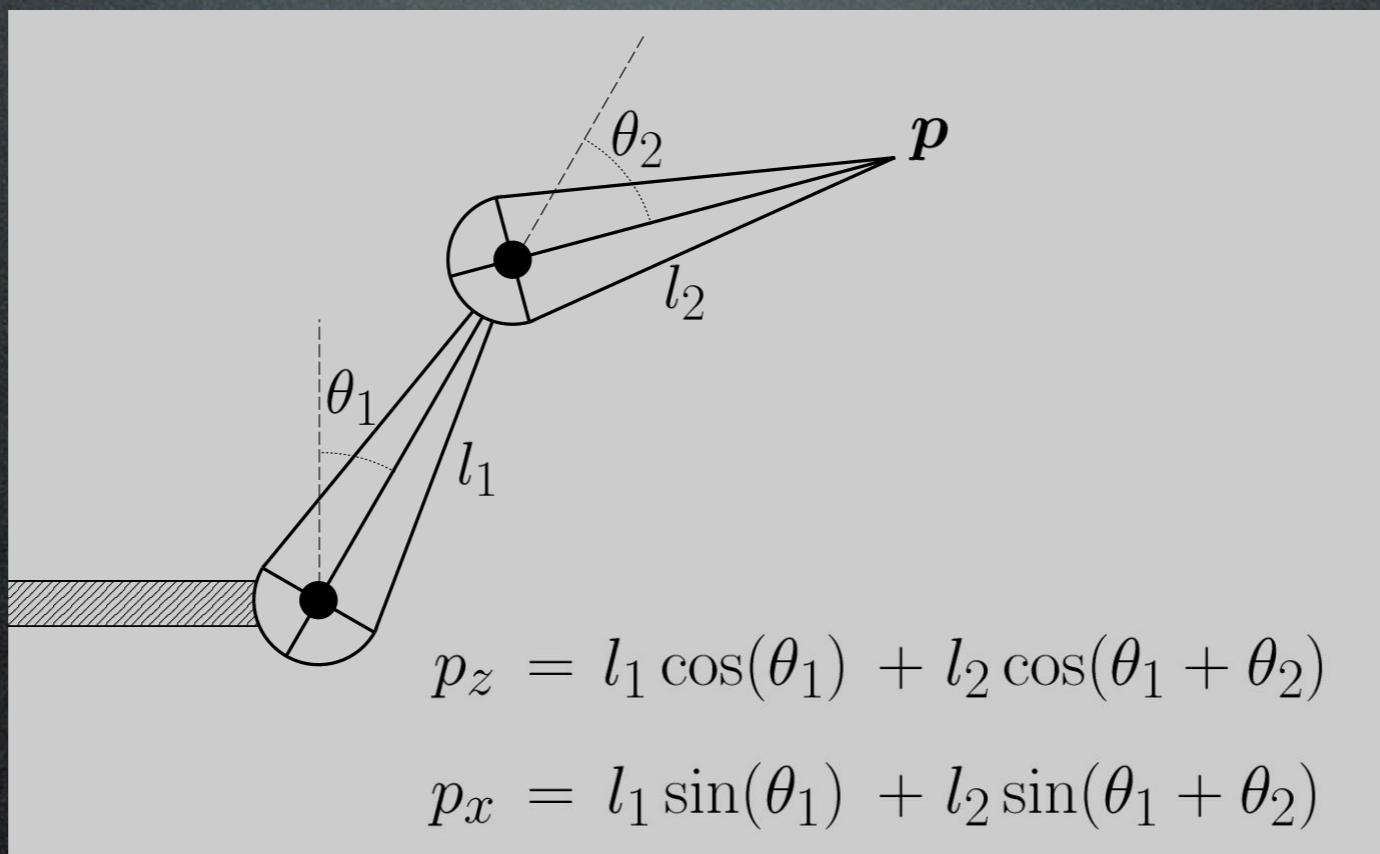


Numerical IK

- Start in some initial configuration
- Define an error metric (e.g. $\mathbf{p}_{\text{goal}} - \mathbf{p}_{\text{current}}$)
- Compute Jacobian of error w.r.t joint angles θ
- Apply Newton's method (or other procedure)
- Iterate...

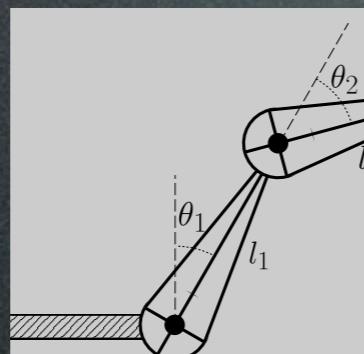
Inverse kinematics

- Recall the simple two segment arm:

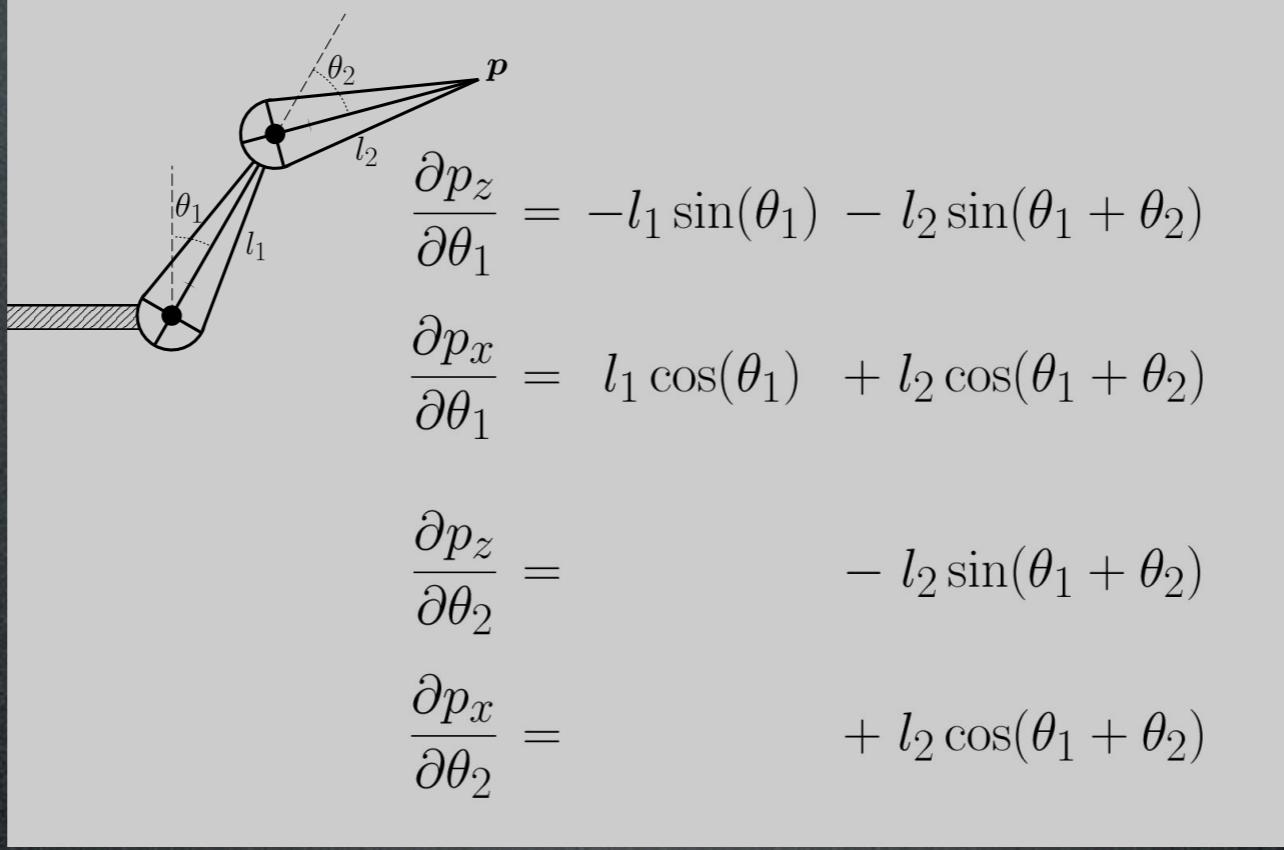


Numerical IK

- We can write the derivatives


$$\frac{\partial p_z}{\partial \theta_1} = -l_1 \sin(\theta_1) - l_2 \sin(\theta_1 + \theta_2)$$
$$\frac{\partial p_x}{\partial \theta_1} = l_1 \cos(\theta_1) + l_2 \cos(\theta_1 + \theta_2)$$
$$\frac{\partial p_z}{\partial \theta_2} = -l_2 \sin(\theta_1 + \theta_2)$$
$$\frac{\partial p_x}{\partial \theta_2} = +l_2 \cos(\theta_1 + \theta_2)$$

Numerical IK



A diagram of a two-link robotic arm. The first link is fixed to a horizontal surface. The second link is pivoted at its left end. The joint angles are labeled θ_1 and θ_2 . The segments are labeled l_1 and l_2 . The tip of the second link is labeled p .

$$\frac{\partial p_z}{\partial \theta_1} = -l_1 \sin(\theta_1) - l_2 \sin(\theta_1 + \theta_2)$$
$$\frac{\partial p_x}{\partial \theta_1} = l_1 \cos(\theta_1) + l_2 \cos(\theta_1 + \theta_2)$$
$$\frac{\partial p_z}{\partial \theta_2} = -l_2 \sin(\theta_1 + \theta_2)$$
$$\frac{\partial p_x}{\partial \theta_2} = +l_2 \cos(\theta_1 + \theta_2)$$

- If we change the angles by a small amount $d\theta_1$ and $d\theta_2$, this tells us how p_x and p_z change.

The Jacobian

- Matrix of partial derivatives $J_{ij} = \frac{\partial p_i}{\partial \theta_j}$
- For a two segment arm in 2D,

$$\mathbf{J} = \begin{bmatrix} \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} \\ \frac{\partial p_z}{\partial \theta_1} & \frac{\partial p_z}{\partial \theta_2} \end{bmatrix}$$

The Jacobian

- A small change in θ leads to a small change in \mathbf{p}

$$\begin{aligned} dp_x &= \frac{\partial p_x}{\partial \theta_1} d\theta_1 + \frac{\partial p_x}{\partial \theta_2} d\theta_2 \\ dp_z &= \frac{\partial p_z}{\partial \theta_1} d\theta_1 + \frac{\partial p_z}{\partial \theta_2} d\theta_2 \end{aligned} \quad d\mathbf{p} = \begin{bmatrix} \frac{\partial p_x}{\partial \theta_1} & \frac{\partial p_x}{\partial \theta_2} \\ \frac{\partial p_z}{\partial \theta_1} & \frac{\partial p_z}{\partial \theta_2} \end{bmatrix} \cdot \begin{bmatrix} d\theta_1 \\ d\theta_2 \end{bmatrix} = \mathbf{J} \cdot d\theta$$

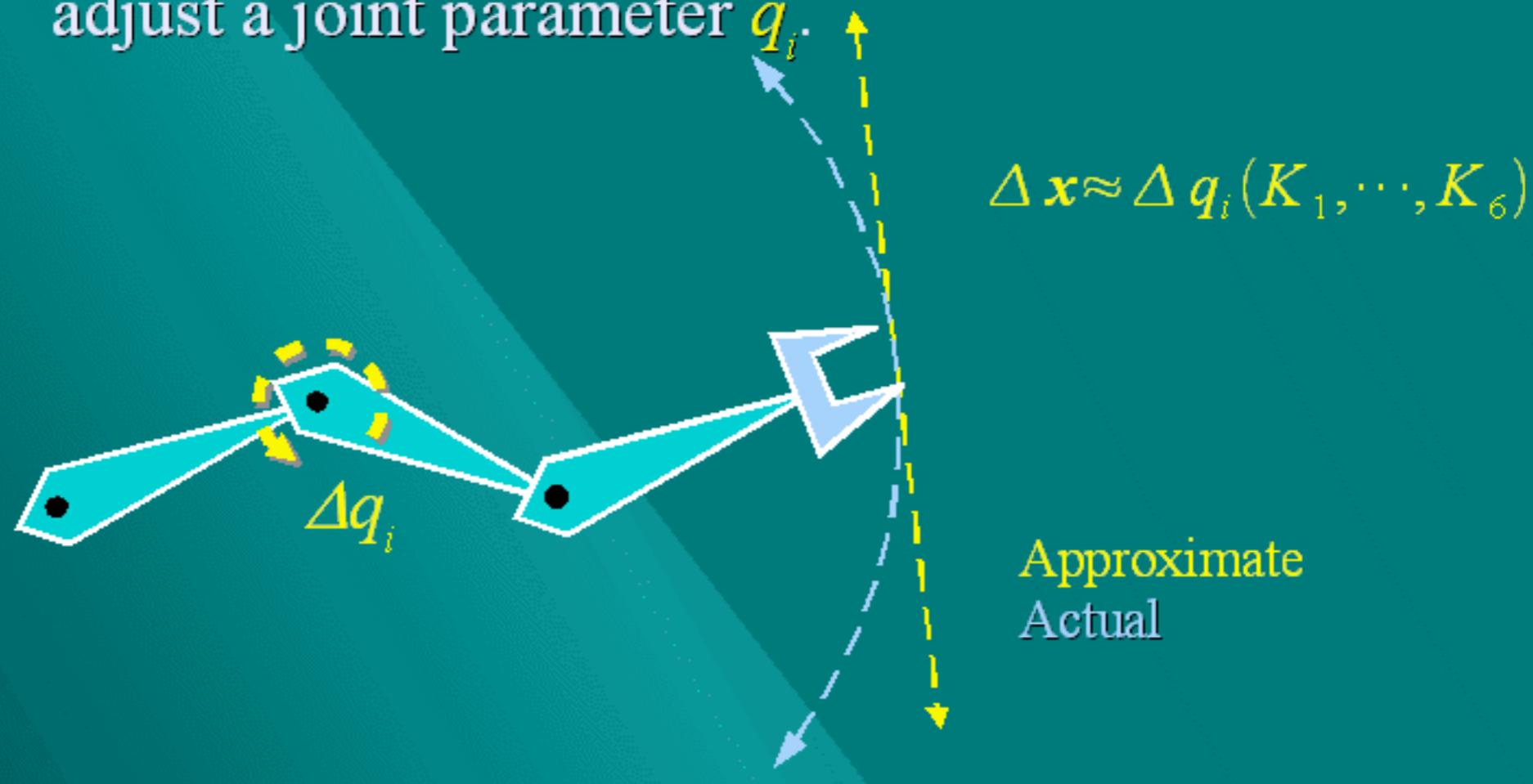
- So... if we want to change \mathbf{p} , this tells us how to change θ ?

$$d\mathbf{p} = \mathbf{J} \cdot d\theta$$

$$d\theta = \mathbf{J}^{-1} \cdot d\mathbf{p}?$$

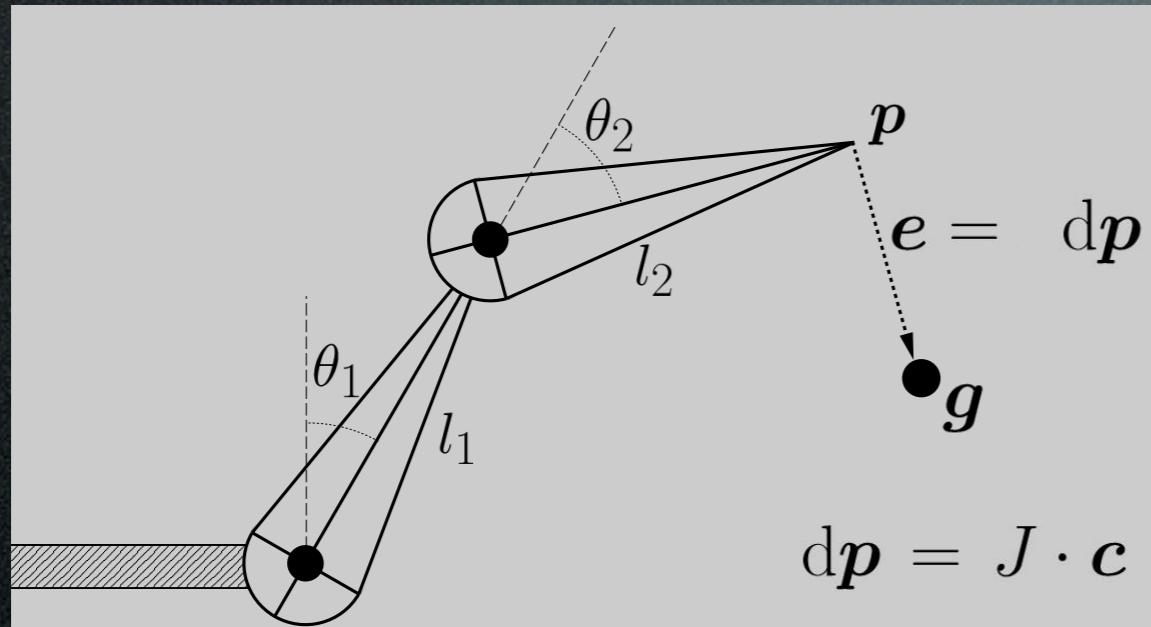
The Jacobian

- Put another way, J tells us approximately how much x will change in world space when we adjust a joint parameter q_i



Bill Baxter

Back to inverse kinematics



$$dp = J \cdot c = J \cdot d\theta$$

- We want \mathbf{p} to change by $d\mathbf{p}$
- Can we simply change $\boldsymbol{\theta}$ by $d\boldsymbol{\theta} = \mathbf{J}^{-1} d\mathbf{p}$?
- ...Is \mathbf{J} invertible?

Inverse kinematics

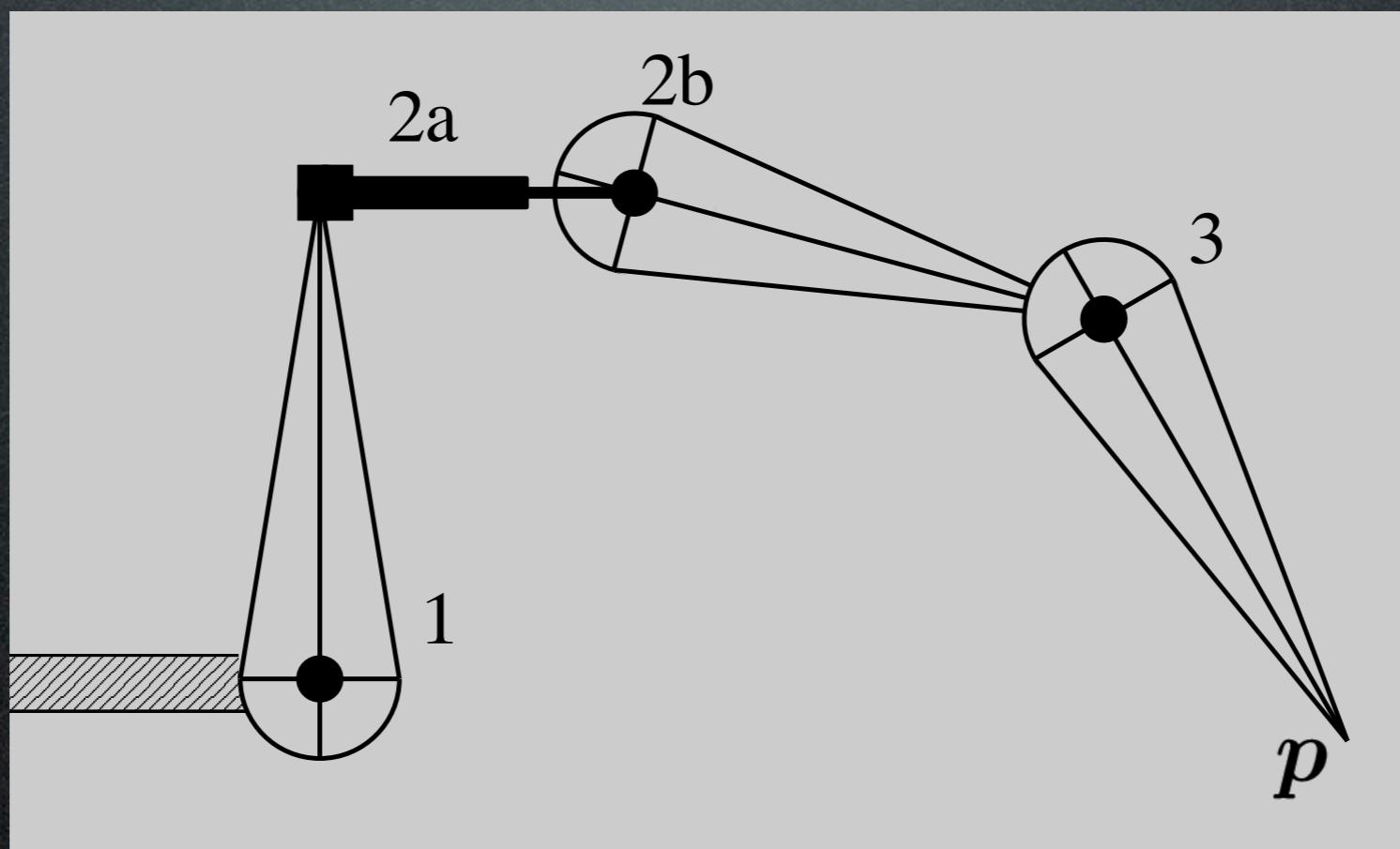
- Problems:
 - Jacobian may (will!) not be invertible → use pseudo-inverse, or use more robust numerical method
 - Jacobian is not constant → take small steps
- Nonlinear optimization, but (mostly) well-behaved

More complex systems

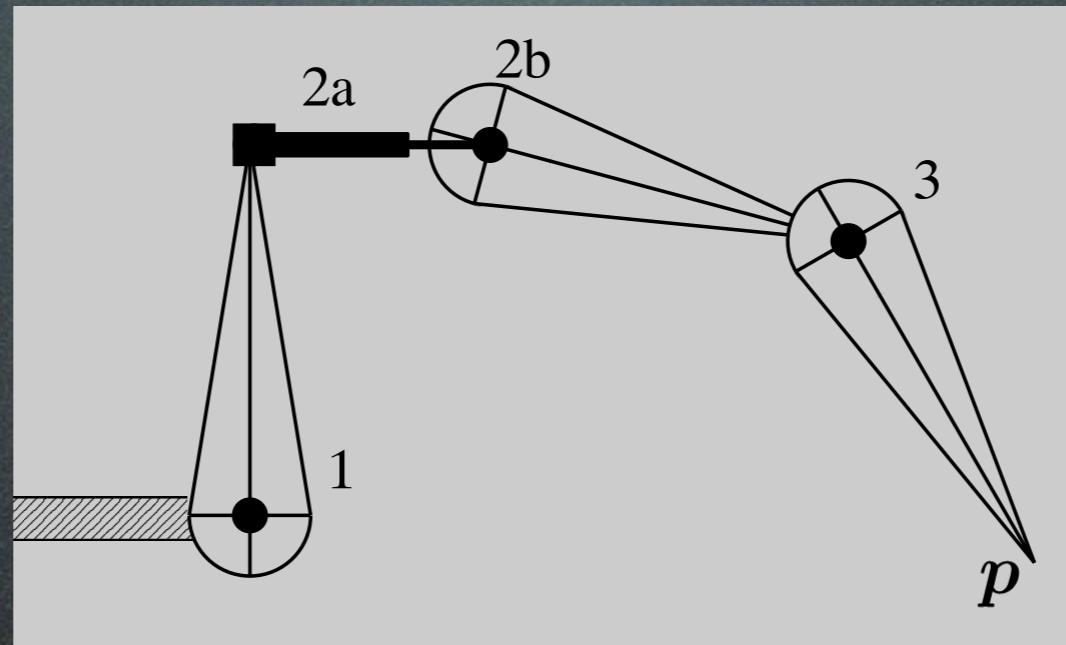
- More complex joints (prism and ball)
- More links
- Other goals (e.g. center of mass)
- Hard constraints (joint limits, collisions)
- Multiple criteria and multiple chains

Multiple links

- We need a generic way of building the Jacobian



Multiple links



- Can't just stack the Jacobians together!

$$\tilde{\mathbf{J}} = [\mathbf{J}_1 \ \mathbf{J}_{2a} \ \mathbf{J}_{2b} \ \mathbf{J}_3]$$

$$\mathbf{q} = \begin{bmatrix} \theta_1 \\ d_{2a} \\ \theta_{2b} \\ \theta_3 \end{bmatrix}$$

$$d\mathbf{p} \neq \tilde{\mathbf{J}} \cdot d\mathbf{q}$$

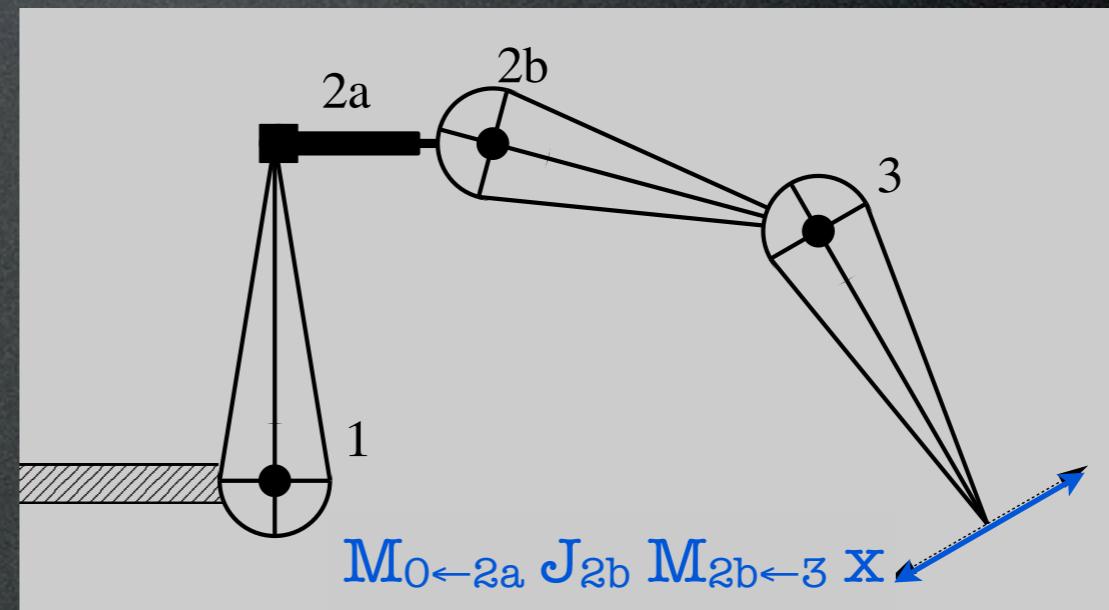
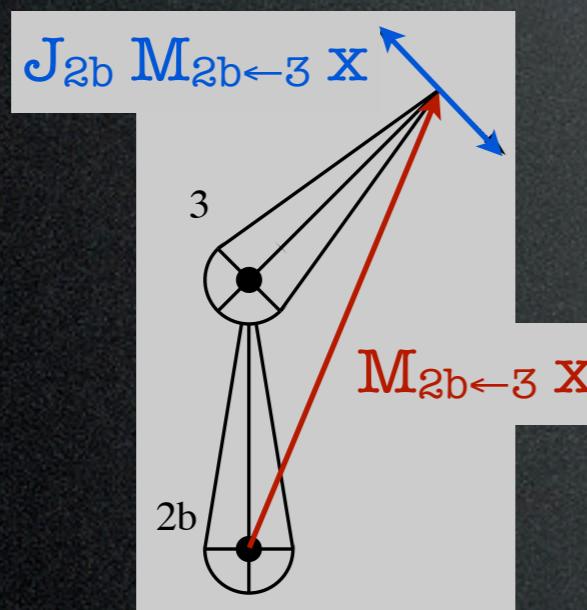
Remember forward kinematics

- World position of point is given by composition of transformations

$$\mathbf{p} = \mathbf{M}_{0 \leftarrow 1} \cdot \mathbf{M}_{1 \leftarrow 2a} \cdot \mathbf{M}_{2a \leftarrow 2b} \cdot \mathbf{M}_{2b \leftarrow 3} \cdot \mathbf{x}$$

- If joint 2b moves, only $\mathbf{M}_{2a \leftarrow 2b}$ changes

$$\begin{aligned}\frac{\partial \mathbf{p}}{\partial \theta_{2b}} &= \mathbf{M}_{0 \leftarrow 1} \cdot \mathbf{M}_{1 \leftarrow 2a} \cdot \frac{\partial}{\partial \theta_{2b}} \mathbf{M}_{2a \leftarrow 2b} \cdot \mathbf{M}_{2b \leftarrow 3} \cdot \mathbf{x} \\ &= \mathbf{M}_{0 \leftarrow 1} \cdot \mathbf{M}_{1 \leftarrow 2a} \cdot \mathbf{J}_{2b}(\theta_{2b}) \cdot \mathbf{M}_{2b \leftarrow 3} \cdot \mathbf{x}\end{aligned}$$



Multiple links

- Compute each joint's Jacobian locally (between outboard and inboard bodies)

$$\mathbf{J} = \begin{bmatrix} \cdot \mathbf{J}_1(\theta_1) \cdot \mathbf{M}_{1 \leftarrow 3} \mathbf{x}, \\ \mathbf{M}_{0 \leftarrow 1} \cdot \mathbf{J}_{2a}(d_{2a}) \cdot \mathbf{M}_{2a \leftarrow 3} \mathbf{x}, \\ \mathbf{M}_{0 \leftarrow 2a} \cdot \mathbf{J}_{2b}(\theta_{2b}) \cdot \mathbf{M}_{2b \leftarrow 3} \mathbf{x}, \\ \mathbf{M}_{0 \leftarrow 2b} \cdot \mathbf{J}_3(\theta_3) \cdot \mathbf{x} \end{bmatrix} \quad \mathbf{q} = \begin{bmatrix} \theta_1 \\ d_{2a} \\ \theta_{2b} \\ \theta_3 \end{bmatrix}$$

(each entry here is a column of the matrix)

$$dp = J \cdot dq$$