

Lecture 12: Diodes

• Announcements:

- HW#4 online and due Friday via Gradescope
- Lab#2 continues this week
 - ↳ Prelab is due at the beginning of lab
- Lab#3 next week
 - ↳ Materials for Lab#3 already online
- Midterm 1 ~2.5 weeks away, on Friday, Oct. 11
 - ↳ We have 7-9 p.m., 160 Kroeber Hall
- My Monday Office Hours will move to 5-6 p.m. on Oct. 14 and thereafter
- Projector overheated in our classroom; this is a recorded lecture

• Lecture Topics:

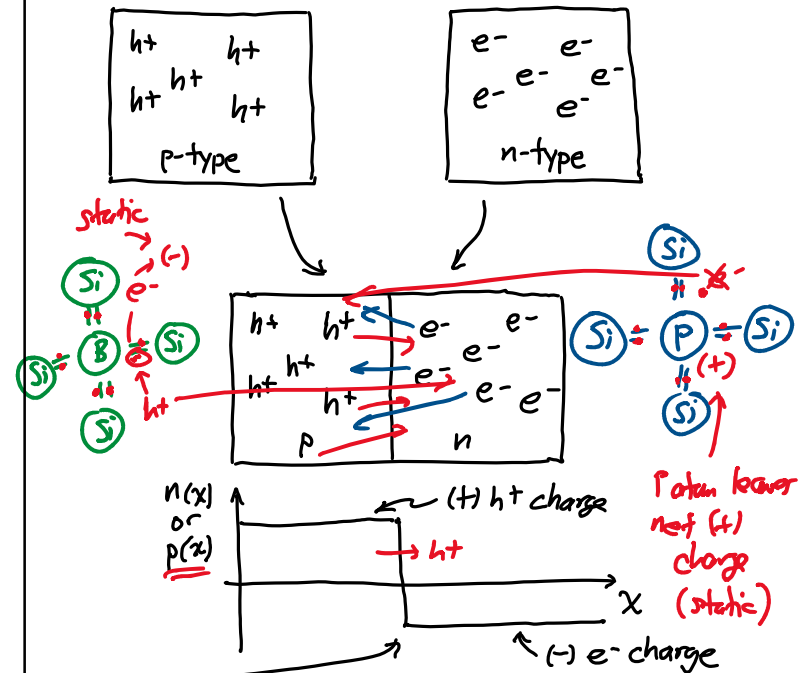
- ↳ Diode Operation
 - Zero Bias
 - Forward Bias
 - Reverse Bias
- ↳ Diode Fabrication
- ↳ MOSFET Overview

• Last Time:

- Finished currents in semiconductors
- Now, start diode operation ...

Diode

⇒ merely a pn-junction, i.e., a result of bringing p-type and n-type material into contact w/ one another



↳ huge gradient in free charge @ the interface
 ↳ corresponds to high energy state
 ↳ ∴ system tries to eq. uilibrate to a low energy state
 ↳ e-'s move to the left, h+'s move to the right

pn Junction

⇒ when they move they leave behind static charge regions (because there originally was a neutral region)

depletion region → region of static charge devoid of carriers

Eventually, an E field develops that opposes further movement of mobile charge (e^- & h^+)

(opposites attract; likes repel)

mobile charge static negative charge static positive charge mobile charge

The Diode Equation

$$i_D = I_S \left[\exp\left(\frac{qV_D}{nkT}\right) - 1 \right] = I_S \left[\exp\left(\frac{V_D}{nV_T}\right) - 1 \right]$$

$I_S \triangleq$ reverse saturation current [A]

$q = 1.602 \times 10^{-19} \text{ C}$

$k =$ Boltzmann constant $= 1.38 \times 10^{-23} \text{ J/K}$

$T =$ absolute temperature [K]

$V_T = \frac{kT}{q} = 25 \text{ mV}$

Reverse Bias Forward Bias

⇒ now, get some insight into where this equation comes from

Zero Bias $V_D = 0V \rightarrow i_D = 0A$

No current \rightarrow i_V characteristic not interesting.
However, there is capacitance:

free carriers \rightarrow mobile charge \rightarrow conductor!
immobile (static) charge \rightarrow insulator!

Capacitor

p-type: N_A n-type: N_D

$-Q_p = q N_A x_p A$
 $+Q_n = q N_D x_n A = Q_n$

W_{d0}

These must be equal:

$$Q_p = q N_A x_p A = Q_n = q N_D x_n A$$

$$q N_A x_p W_{d0} A = q N_D x_n W_{d0} A \rightarrow x_p = \frac{N_D}{N_A} x_n$$

$$x_n + x_p = W_{d0} = (x_n + \frac{N_D}{N_A} x_n) = W_{d0} \rightarrow \frac{N_A}{N_A + N_D} x_n + \frac{N_D}{N_A + N_D} x_n = W_{d0}$$

$$x_n = \frac{N_A}{N_A + N_D} W_{d0} \rightarrow Q_n = q N_D \left(\frac{N_A}{N_A + N_D} \right) W_{d0} A$$

$$x_p = \frac{N_D}{N_A + N_D} W_{d0} \rightarrow Q_p = q N_A \left(\frac{N_D}{N_A + N_D} \right) W_{d0} A$$

$$\Rightarrow Q_n = Q_p = q (N_A N_D) W_{d0} A$$

\Rightarrow to get W_{d0} , need:

Voltage Dropped Across the Depletion Region:

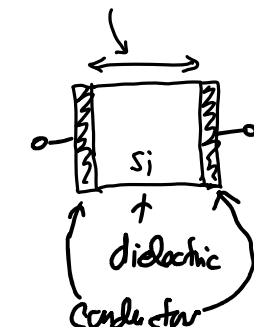
Separate oppositely charged regions \rightarrow Electric field across the depletion region
 \rightarrow Voltage Drop = $-\int E(x) dx$

As you will see in EE 130: The voltage dropped from $x = -x_p$ to $x = x_n$ is:

$$\phi_j \triangleq \text{built-in potential} = V_T \ln \left(\frac{N_A N_D}{n_i^2} \right) \left[= - \int_{-x_p}^{x_n} E(x) dx \right]$$

The depletion layer width:

$$W_{d0} = f(\phi_j) = x_n + x_p = \sqrt{\frac{2 \epsilon_s}{q} \left(\frac{1}{N_A} + \frac{1}{N_D} \right) \phi_j}$$



\Rightarrow this is a capacitor:

$$C_j = \frac{\epsilon_s A}{W_{d0}} \text{ for } V_D = 0$$

ϵ_s = permittivity of silicon = 11.7

A = cross-sectional area of diode

Reverse Bias $V_D < 0 \rightarrow i_D = -I_S$

Current negligible \rightarrow but again, there is capacitance and it is now a function of the reverse bias voltage

Again, the depletion region width is proportional to the potential dropped across the region. But now, the total potential drop = $V_R + \phi_j$ and

$$W_d = x_n + x_p = \sqrt{\frac{2\epsilon_s}{q} \left(\frac{1}{N_A} + \frac{1}{N_D} \right) (\phi_j + V_R)} = W_{d0} \sqrt{1 + \frac{V_R}{\phi_j}}$$

$$Q_n = q N_D x_n A = q \left(\frac{N_A N_D}{N_A + N_D} \right) W_d A \Rightarrow Q_n = f(V_R)$$

$f(V_R)$ Thus, this is a nonlinear capacitor!

$$C_j = \frac{dQ_n}{dV_R} = \frac{C_{j0}}{\sqrt{1 + \frac{V_R}{\phi_j}}} ; C_{j0} = \frac{\epsilon_s A}{W_{d0}}$$

$[V_R = -V_D] \Rightarrow C_j = \frac{C_{j0}}{\sqrt{1 - \frac{V_D}{\phi_j}}}$

Forward Bias Case $V_D > 0$.

\Rightarrow most interested in case where $V_D \geq V_{D0}$.

(minority carriers) e^- conc. on the p-side \uparrow diode turn-on voltage

h^+ are majority carriers \rightarrow the p-side \rightarrow minority carriers

h^+ conc. \rightarrow majority carriers e^- 's are majority carriers

$n_p(-W_p) = \frac{n_i^2}{N_A}$ $p_n(W_n) = \frac{n_i^2}{N_D}$

$+ V_D$

Injected e^- 's on the p-side: $n_p(-x_p) = \frac{n_i^2}{N_A} \exp\left(\frac{V_D}{V_T}\right)$

Injected h^+ on the n-type side: $p_n(x_n) = \frac{n_i^2}{N_D} \exp\left(\frac{V_D}{V_T}\right)$

To get currents, take the slopes of the minority carrier distributions:

On the n-side $\rightarrow h^+$ diffusion current:

$$J_p^{diff} = -qD_p \frac{\partial p}{\partial x} = -qD_p \left[\frac{p_n(W_n) - p_n(x_n)}{W_n - x_n} \right]$$

$$\Rightarrow J_p^{diff} = qD_p \frac{n_i^2}{N_D} \frac{1}{(W_n - x_n)} \left[\exp\left(\frac{V_D}{V_T}\right) - 1 \right]$$

contributes to the saturation current, I_S

On p-side $\rightarrow e^-$ diffusion current:

$$J_n^{diff} = qD_n \frac{\partial n}{\partial x} = qD_n \left[\frac{n_p(-x_p) - n_p(-W_p)}{-x_p + W_p} \right]$$

$$\Rightarrow J_n^{diff} = qD_n \frac{n_i^2}{N_A} \frac{1}{(-x_p + W_p)} \left[\exp\left(\frac{V_D}{V_T}\right) - 1 \right]$$

... and for total current density:

$$J_{tot} = J_p^{diff} + J_n^{diff} = I_S \left[\exp\left(\frac{V_D}{V_T}\right) - 1 \right]$$

$$\text{where } I_S = qn_i \left[\frac{D_p}{N_D} \frac{1}{(W_n - x_n)} + \frac{D_n}{N_A} \frac{1}{(W_p - x_p)} \right]$$

Actual Diode

