

Lecture 23: Small-Signal CE Amplifier Analysis

• Announcements:

- HW#7 online and due Friday via Gradescope
- Lab#5 due Tuesday, Nov. 12, 5 p.m.
- Gave Z scores last time

• Lecture Topics:

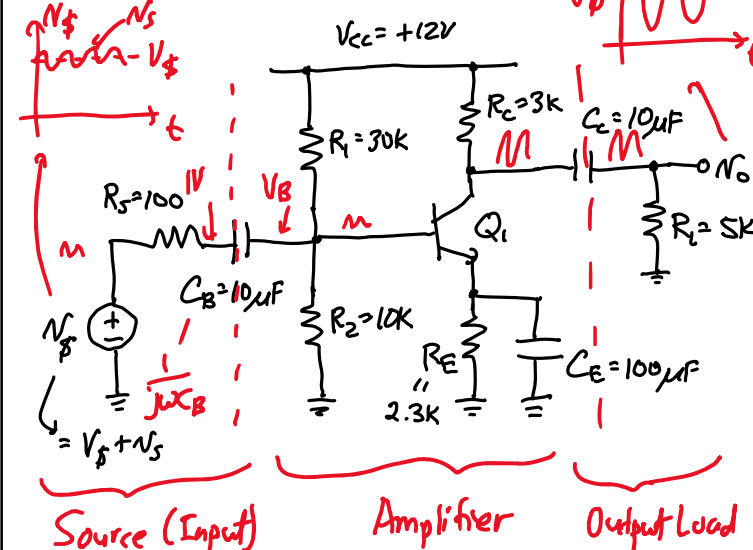
- ↳ Finish Common Emitter Amplifier
- ↳ Frequency Response
- ↳ High Frequency Model for BJT

• Last Time:

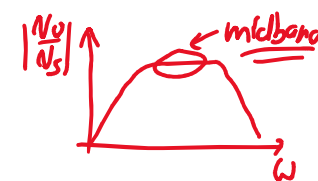
- Going through a Common Emitter Amplifier small-signal analysis example
- Now, continue with this ...

Procedure for Small-Signal Analysis

• (Common Emitter Example)



[Thevenin Equivalent]

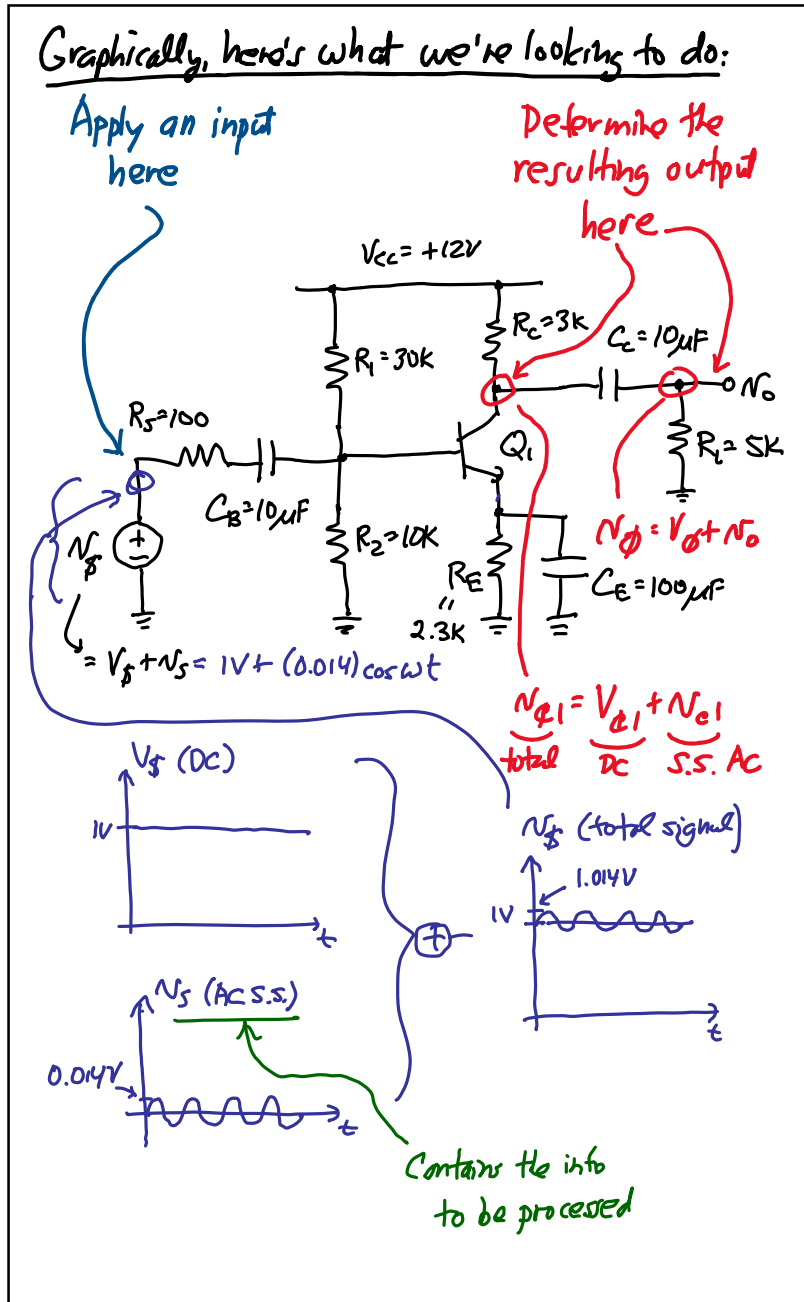


For Q:  $\beta = 100$ ,  $V_A = 100V$

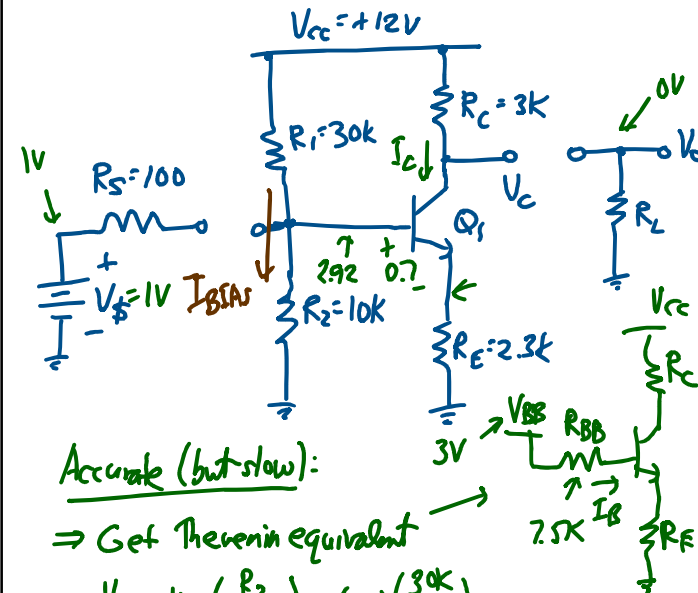
Find the voltage gain,  $\frac{V_o}{V_s}$ .

Draw the collector voltage waveform for

$$V_s = \underbrace{(0.014) \cos \omega t}_{\text{AC small-signal component}} + \underbrace{1V}_{\text{DC component}}$$



- Determine the DC operating point
  - i.e., find the relevant DC voltages at all nodes and DC currents through all branches
  - Draw the DC circuit
    - Eliminate independent AC small-signal sources
      - Short AC voltage sources
      - Open AC current sources
    - Open all capacitors (in particular, open the bypass/coupling capacitors)
    - Use DC transistor models
      - this might entail nonlinearity in some cases, but approximations can alleviate



Accurate (but slow):

⇒ Get Thevenin equivalent

$$V_{BB} = V_{CC} \left( \frac{R_2}{R_1 + R_2} \right) = (12) \left( \frac{30k}{40k} \right) = 3V$$

$$R_{BB} = R_1 || R_2 = (10k) || (30k) = 7.5k$$

$$I_C = \frac{V_{BB} - V_{BE}}{\frac{R_E}{\alpha} + \frac{R_{BB}}{\beta}} = \frac{3 - 0.7}{\frac{2.3k}{1} + \frac{25k}{100}} = 0.97mA \approx 1mA$$

$$I_B = \frac{I_C}{\beta} = 0.01mA$$

$$\therefore I_E \approx 0.97mA \approx 1mA$$

$$V_B = V_{BB} - I_B R_{BB} = 3 - (0.01mA)(7.5k) = 2.92V$$

$$\therefore V_E = 2.92 - 0.7 = 2.22V$$

$$V_C = V_{CC} - I_C R_C = 12 - (1mA)(3k) = 9V$$

Faster Way:

$$\text{Ignore } I_B \rightarrow V_B = V_{CC} \left( \frac{R_2}{R_1 + R_2} \right) = 3V$$

$$V_E = V_B - V_{BE(on)} = 3 - 0.7 = 2.3V$$

$$\therefore I_E = \frac{V_E}{R_E} = \frac{2.3}{2.3k} = 1mA = I_C$$

$$I_B = \frac{I_C}{\beta} = \frac{1mA}{100} = 0.01mA$$

$$V_C = V_{CC} - I_C R_C = 9V$$

$$I_{BIAS} = \frac{V_{CC}}{R_1 + R_2} = \frac{12}{40k} = 0.3mA > 10I_B \checkmark$$

For a stable bias pt.

② Determine the elements in the small-signal transistor model(s)

↳ If more than one transistor, might need to determine SS element values for several of them

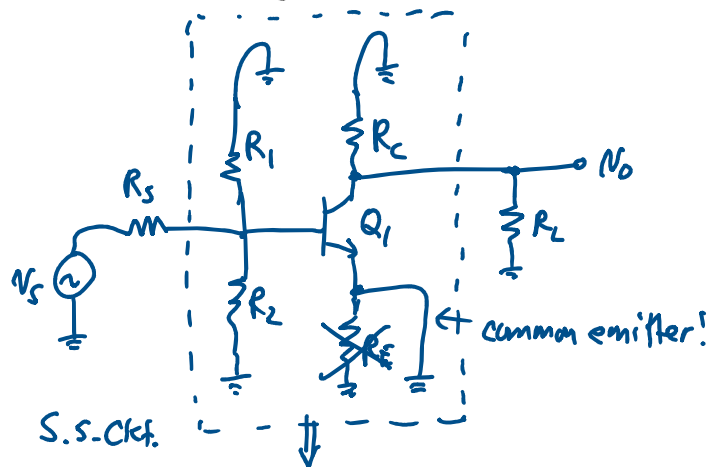
$$g_m = \frac{I_E}{V_T} = \frac{1mA}{25mV} = 0.04 \text{ S} \quad r_o = \frac{V_A}{I_E} = \frac{100}{1mA} = 100k\Omega$$

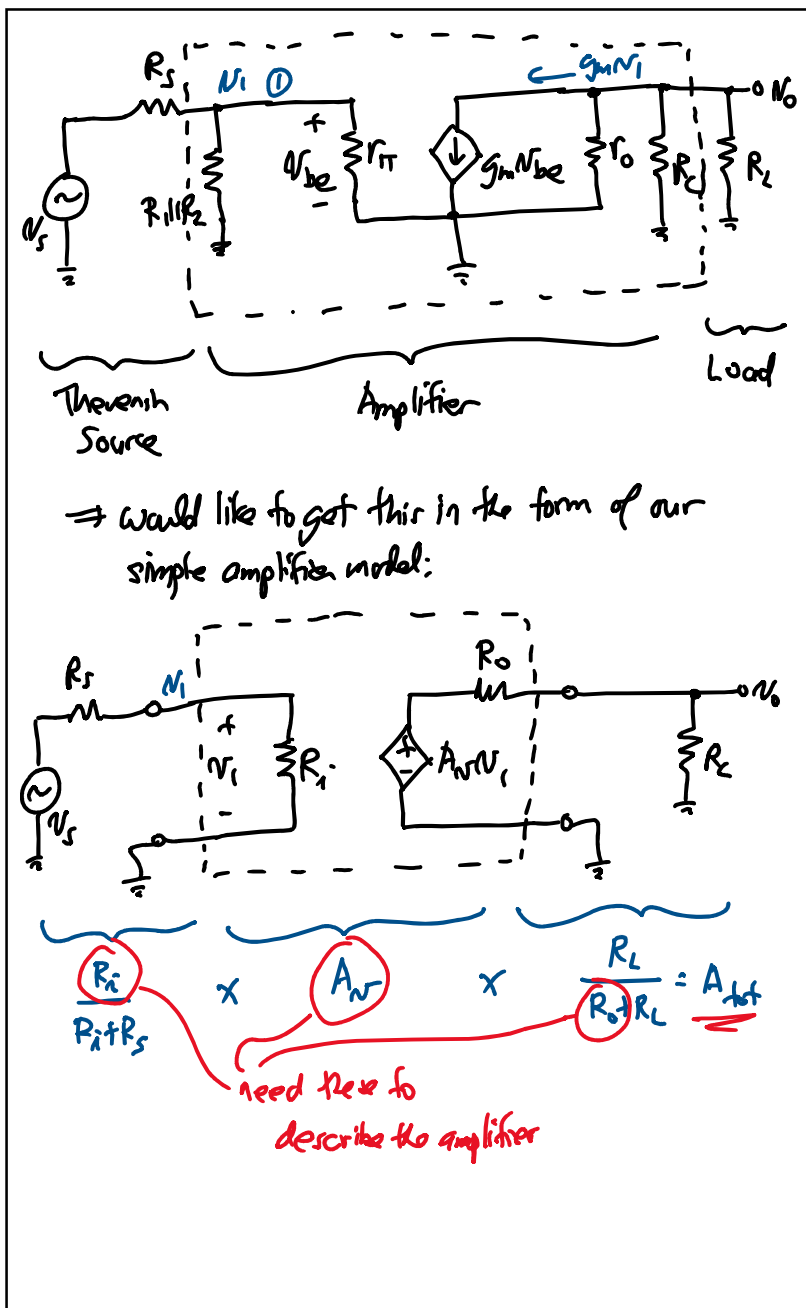
$$r_{\pi} = \frac{\beta}{g_m} = \frac{100}{0.04} = 2.5k\Omega \quad r_e = \frac{\alpha}{g_m} \approx \frac{1}{g_m} = 25\Omega$$

③ Obtain the small-signal circuit

↳ Eliminate independent DC sources

- Short DC voltage sources
- Open DC current sources
- Short large coupling capacitors ( $C's > 10nF$ )
- Use small-signal transistor models





- ④ Use standard circuit analysis (i.e., KCL or KVL with superposition) to determine the parameters of interest
- Usually, the parameters of interest include
    - ↗ Gain,  $A_v$
    - ↗ Input Resistance,  $R_i$
    - ↗ Output Resistance,  $R_o$
    - ↗ Low Frequency Cut-off,  $\omega_b$
    - ↗ High Frequency Cut-off,  $\omega_h$
  - Determine all of these during small-signal analysis
  - The total gain of the simplified amplifier circuit takes the form

$$\frac{V_o}{V_s} = \frac{R_i}{R_i + R_s} A_N \frac{R_L}{R_L + R_o}$$

For ideal want:  $R_i = \infty$   $R_o = 0$   
 ( $R_i \gg R_s$ ) ( $R_o \ll R_L$ )

Amplifier Gain -

$$A_N = \frac{V_o}{V_i} \Big|_{R_i = \infty} \quad (i_b = 0)$$

$$V_o = -(g_m V_i)(r_o \parallel R_c) \Rightarrow A_N = \frac{V_o}{V_i} \Big|_{R_i = \infty} = -g_m(r_o \parallel R_c) = A_N$$

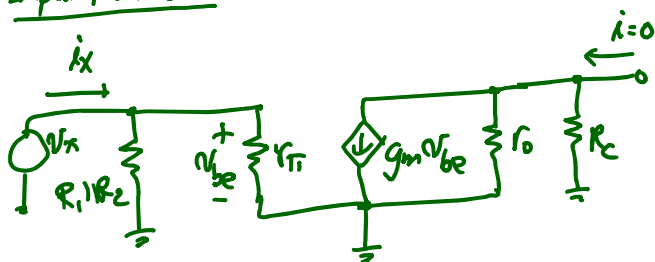
$$A_N \approx -g_m R_c = -120$$

$r_o \gg R_c$

⇒ Max gain occurs when  $R_c = \infty$ :

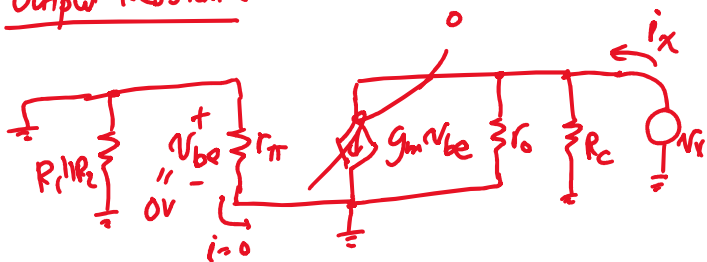
$$\text{Max Gain} = -g_m r_o = -\frac{I_C}{V_T} \frac{V_A}{I_C} = -\frac{V_A}{V_T} = \text{Max Gain}$$

Input Resistance -



$$R_i = \frac{V_x}{i_x} = r_{\pi} \parallel R_1 \parallel R_2 = 1875 \Omega$$

Output Resistance -



$$R_o = \frac{V_x}{i_x} = r_o \parallel R_c \approx R_c = 3k\Omega$$

↑  
[ $r_o \gg R_c$ ]

For the total ckt:

$$\begin{aligned} \text{Gain} &= \frac{N_o}{N_s} = \frac{R_i}{R_i + R_s} A_v \frac{R_L}{R_L + R_o} \\ &= \frac{r_{\pi} \parallel R_1 \parallel R_2}{r_{\pi} \parallel R_1 \parallel R_2 + R_s} (-g_m R_c) \left( \frac{R_L}{R_L + R_o} \right) \\ &= -\frac{r_{\pi} \parallel R_1 \parallel R_2}{r_{\pi} \parallel R_1 \parallel R_2 + R_s} g_m (R_c \parallel R_L) \\ &= -\frac{1875}{1875 + 100} (0.04) (3k \parallel 15k) \\ &= -71.2 = \frac{N_o}{N_s} \quad (\text{midband gain}) \end{aligned}$$

⇒ just for kicks...

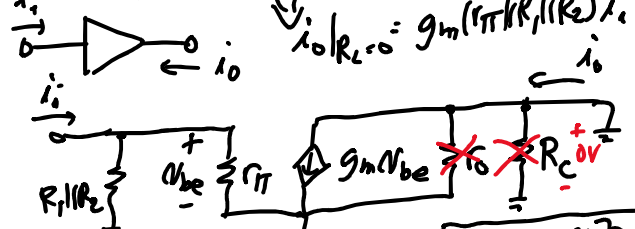
for the ckt. in the box

Short Ckt. Current Gain for the C.E. amp -

$$A_{is} = \frac{i_o}{i_i} \Big|_{R_L=0}$$

( $\alpha v_{be} = 0$ )

$i_o \Big|_{R_L=0} = g_m v_{be}$   
 $v_{be} = i_i (r_{\pi} \parallel R_1 \parallel R_2)$   
 $i_o \Big|_{R_L=0} = g_m (r_{\pi} \parallel R_1 \parallel R_2) i_i$

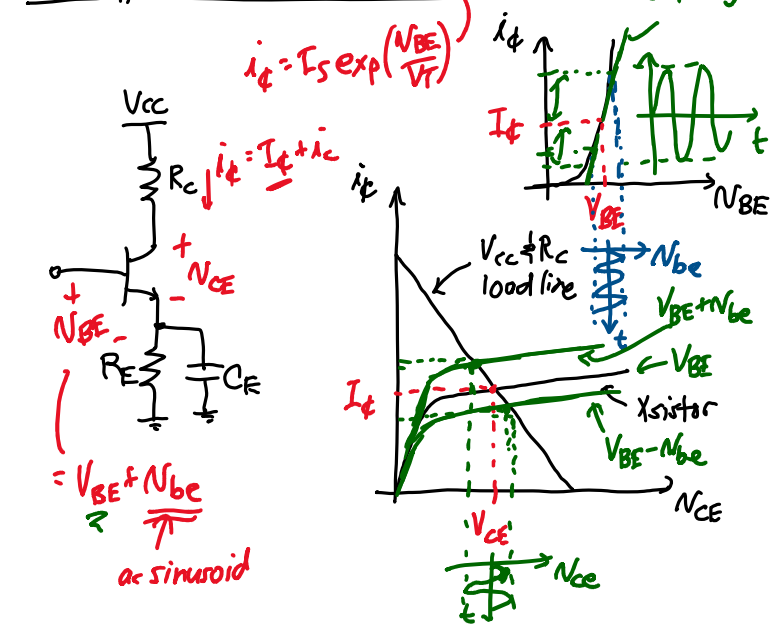
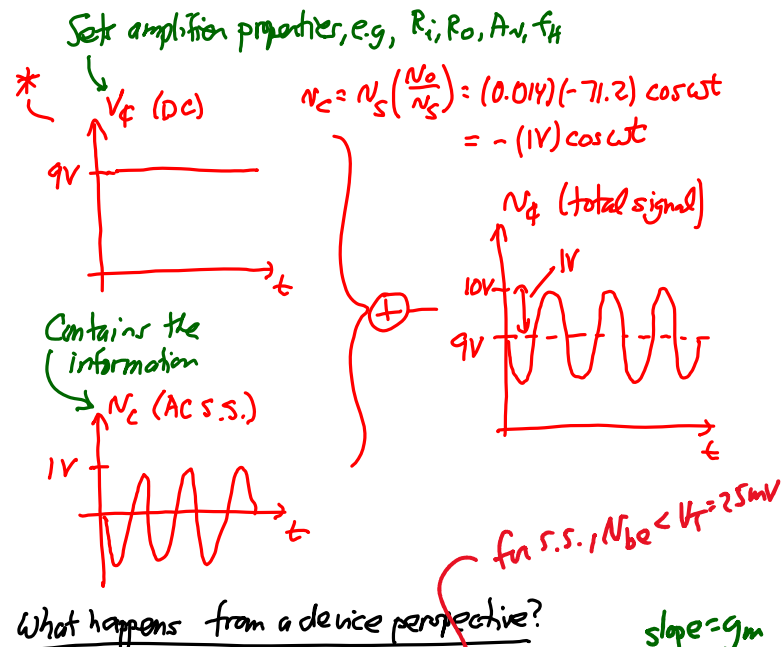
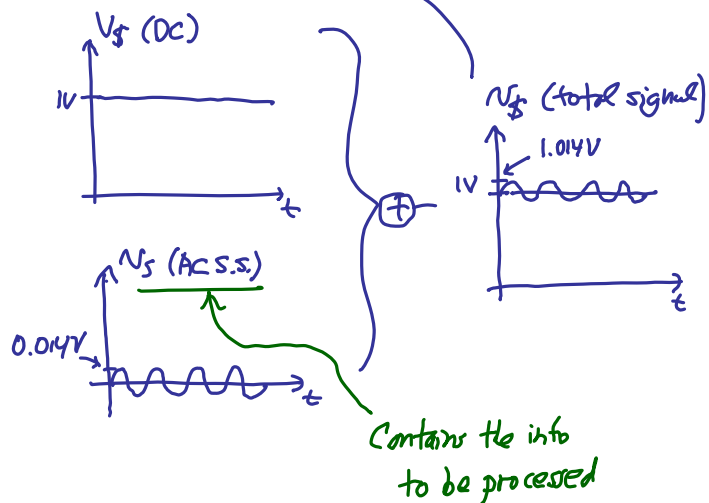
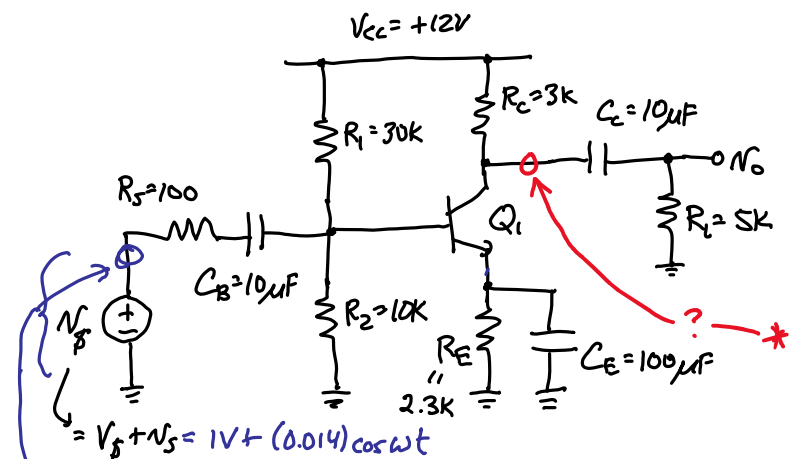


$$A_{is} = g_m (r_{\pi} \parallel R_1 \parallel R_2) = g_m R_i$$

[ $R_1 = R_2 = \infty$ ]  
 $A_{is} = g_m r_{\pi} = \beta$

⑤ Use the gain and resistances determined above to obtain the small-signal voltages and currents at each node/branch of the circuit

- To obtain the actual node & branch signals, superpose the DC and small-signal AC solutions



An Inking of Inspection Analysis

⇒ for fast s.s. ckt analysis:

$R_i = r_{\pi} \parallel R_1 \parallel R_2$

$i_c = g_m v_{be}$

$v_{be}$

$r_{\pi}$

$N_o$

$R_c$

$R_L$

$R_s$

$R_1$

$R_2$

$N_s$

$\frac{N_o}{N_s} = \frac{N_D}{N_s} \cdot \frac{N_o}{N_D} = \frac{r_{\pi} \parallel R_1 \parallel R_2}{r_{\pi} \parallel R_1 \parallel R_2} (-g_m (r_o \parallel R_c \parallel R_L))$

...but more later...